

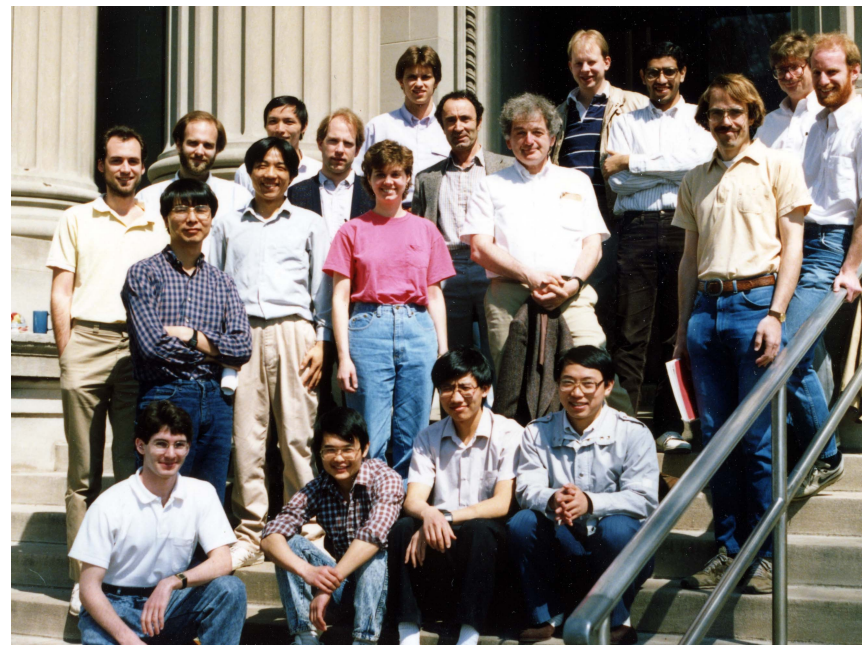
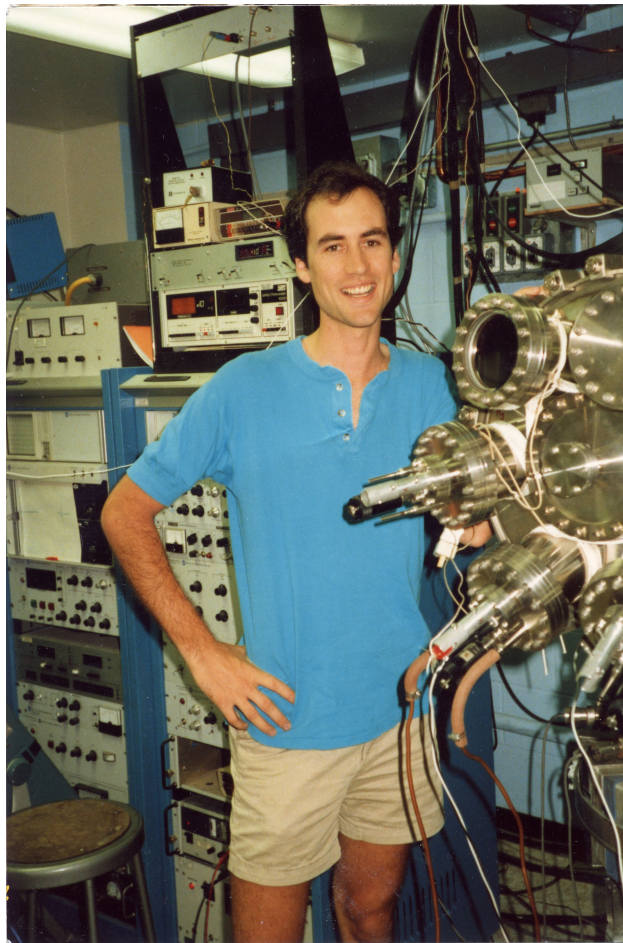
The Series Josephson Junction Array: from collective modes to quantum phase transitions - with applications.

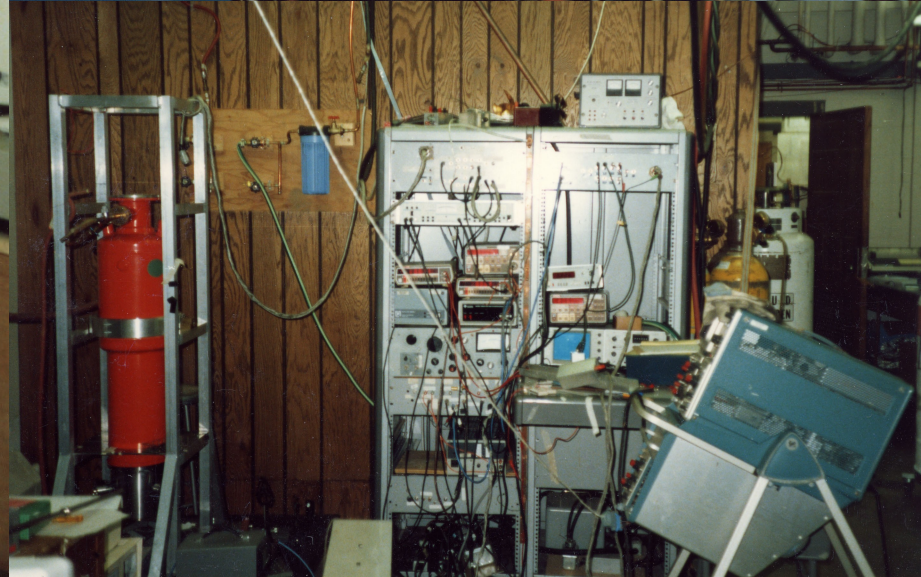
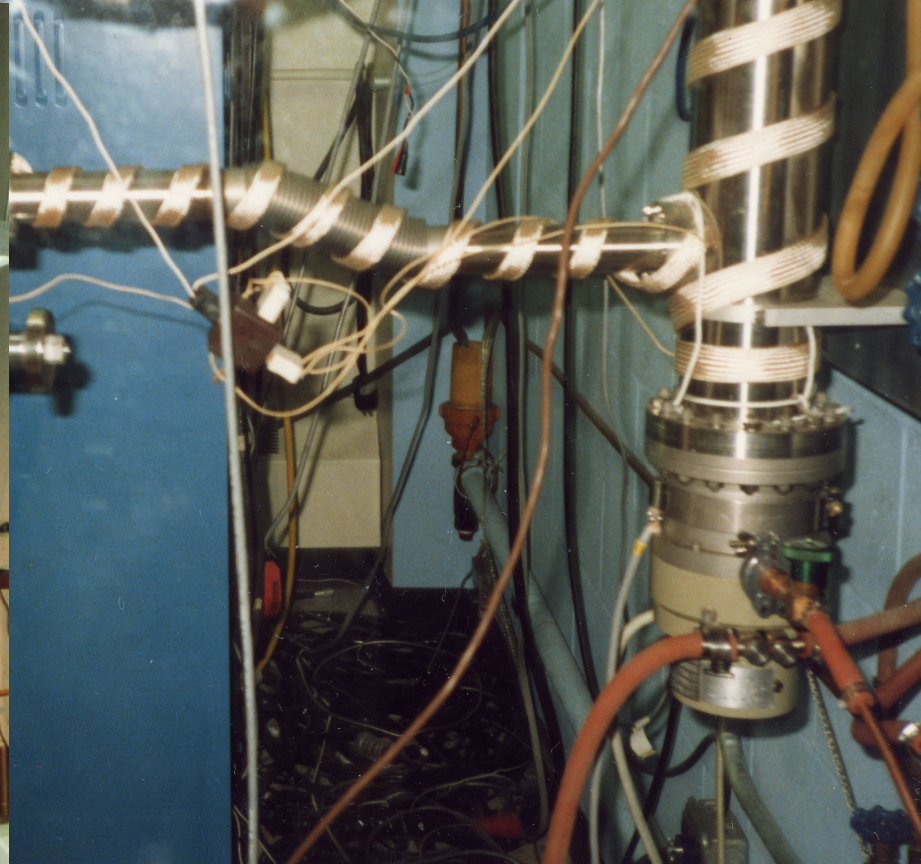
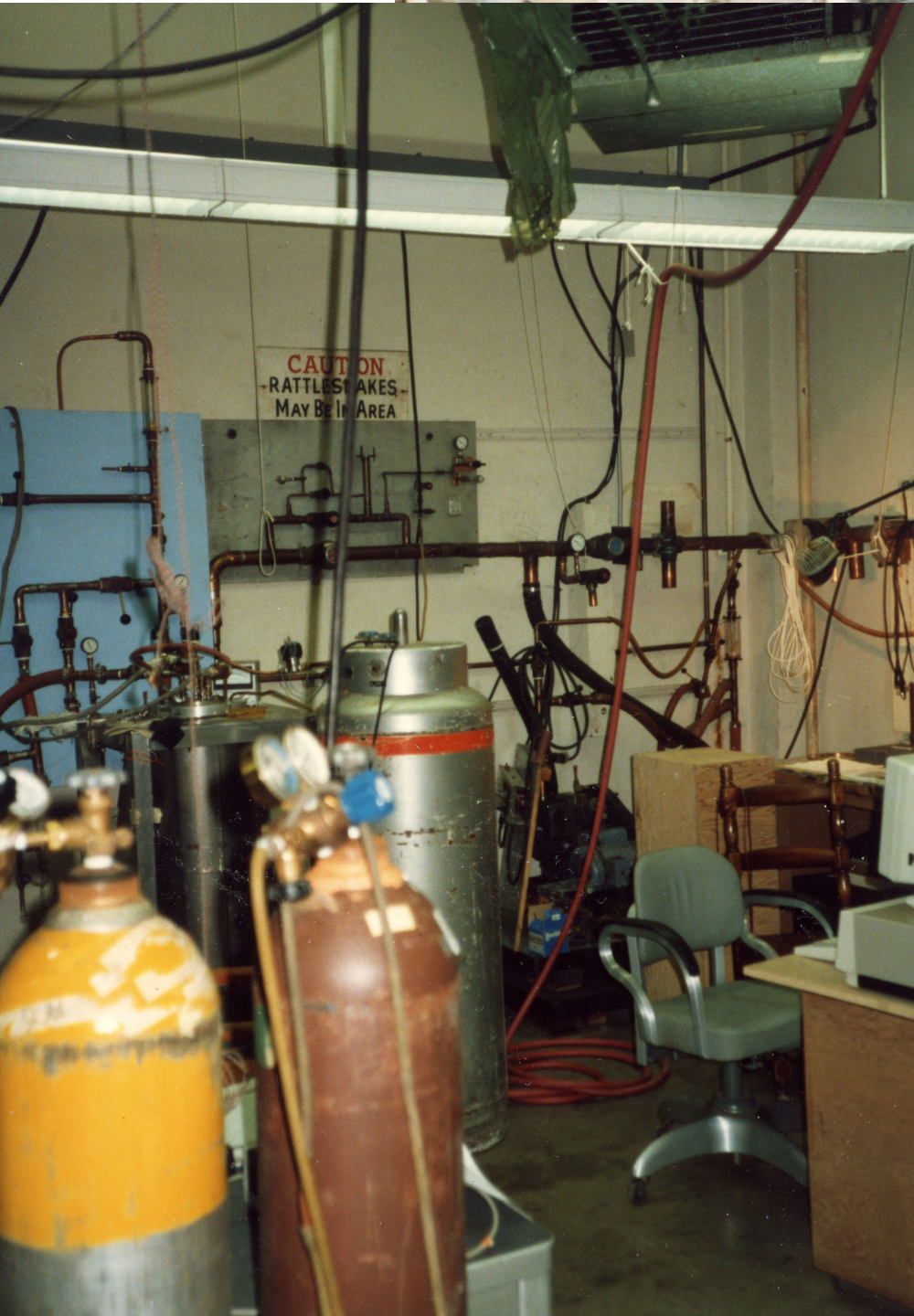
David B. Haviland



Nanostructure Physics
Royal Institute of Technology (KTH)
Stockholm, Sweden

Memories of working in Allen Goldman's Lab







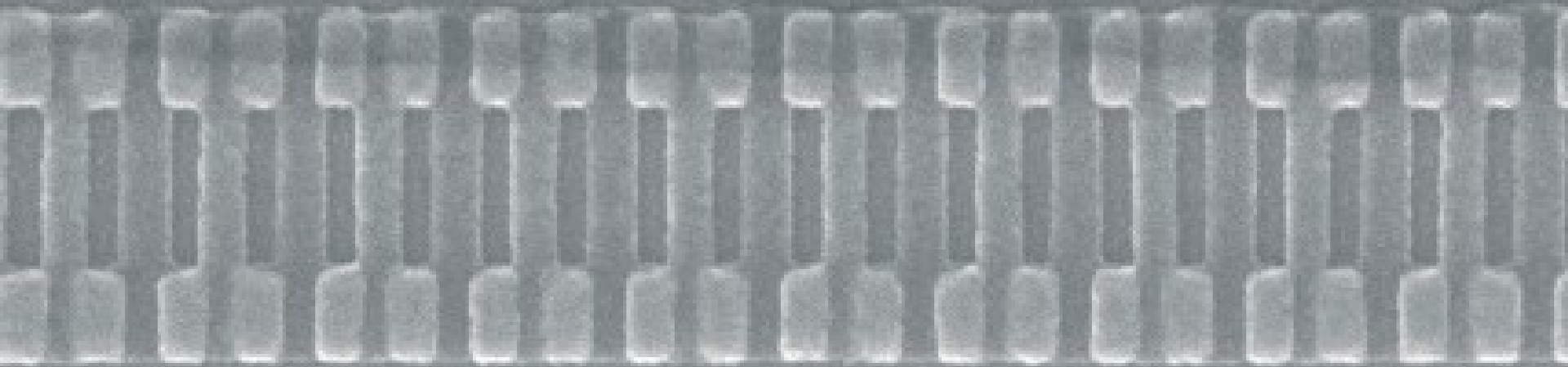




Conference on Josephson Junction Arrays Jackson Hole, 1994



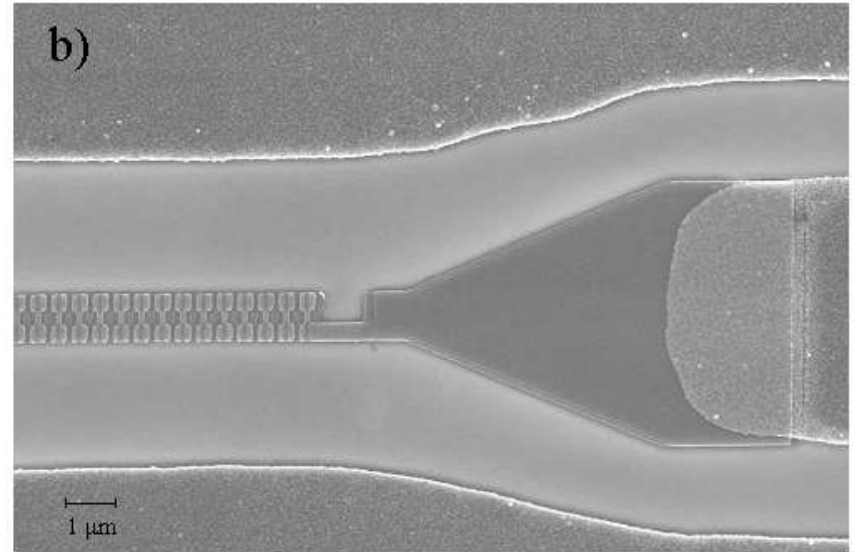
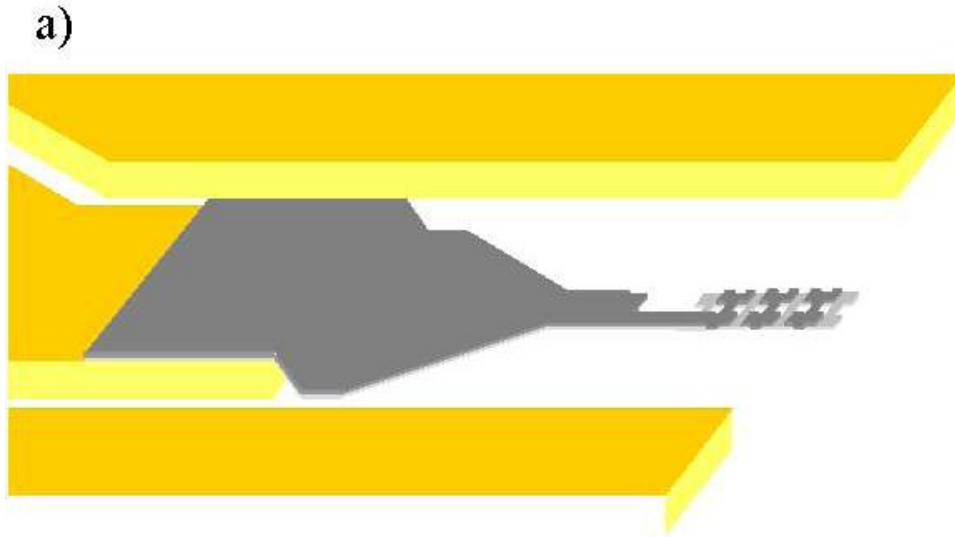
1D Array of small capacitance SQUIDs



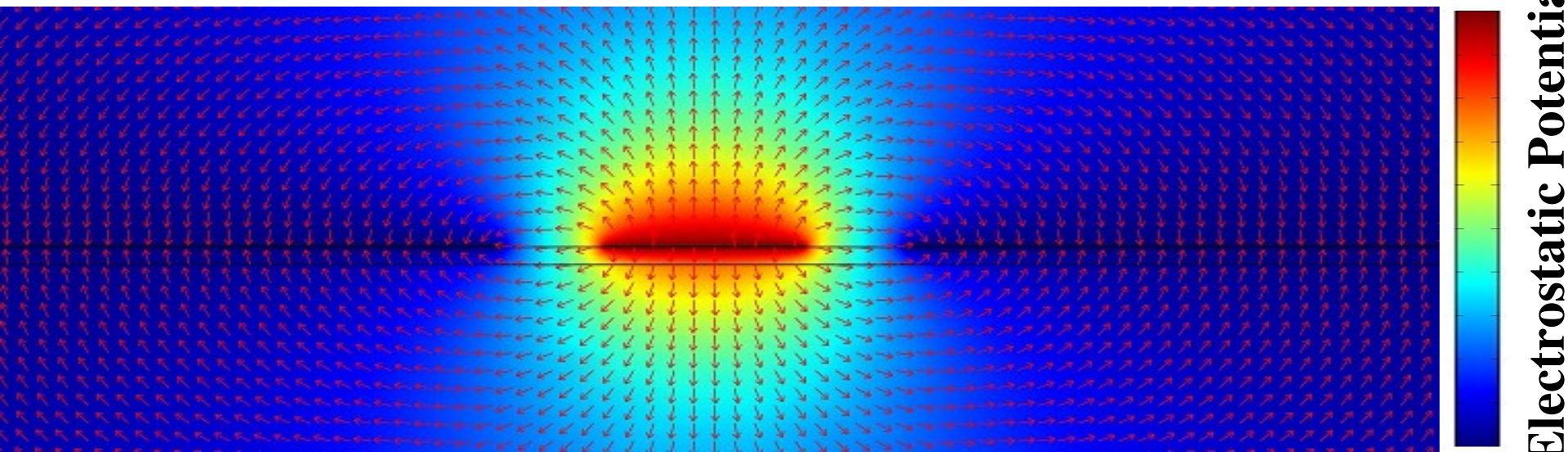
$1\mu m$



Array as a Transmission Line



Coplanar Wave Guide (CPW) - really a transmission line



Three Limits Examined

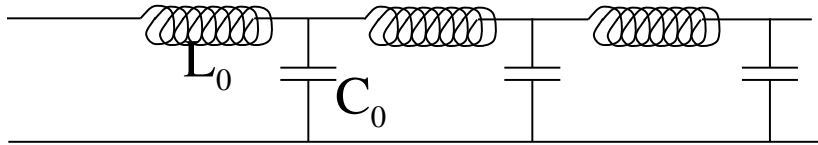
1. Classical, Linear Electrodynamics

2. Classical, Nonlinear Electrodynamics

3. Quantum Electrodynamics

Circuit model of a Transmission Line

Discrete, lumped element model of TEM transmission line



$$Z_L = \sqrt{\frac{L_0}{C_0}} \approx \frac{Z_0}{2\pi} = 60 \, \Omega$$

**Another Natural Impedance for Superconductors:
Quantum Resistance $R_Q = \Phi_0 / 2e = h/4e^2 = 6.45 \, \text{k}\Omega$**

Fact of Nature: $Z_0 \ll R_Q$

$$\frac{Z_L}{R_Q} = \frac{2e^2}{\pi h c \epsilon_0} = \frac{4}{\pi} \alpha$$

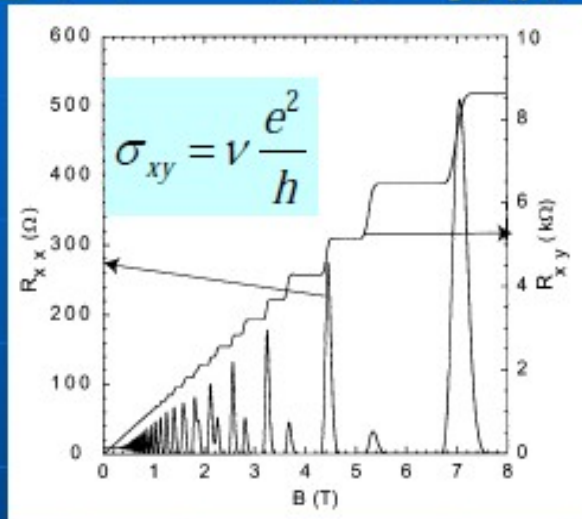
Fine structure constant $\alpha = \frac{1}{137.035999679(94)}$ $\alpha_{\text{CGS}} = \frac{e^2}{\hbar c}$

量子コンダクタンス

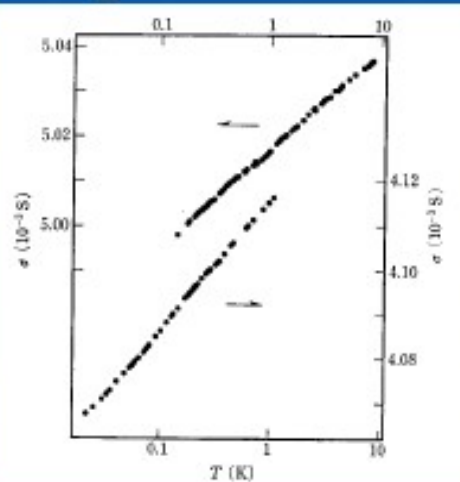
$$\frac{e^2}{h} = \frac{1}{25.813 \text{ k}\Omega}$$

量子ホール効果⇒抵抗の国際標準

超伝導絶縁体転移



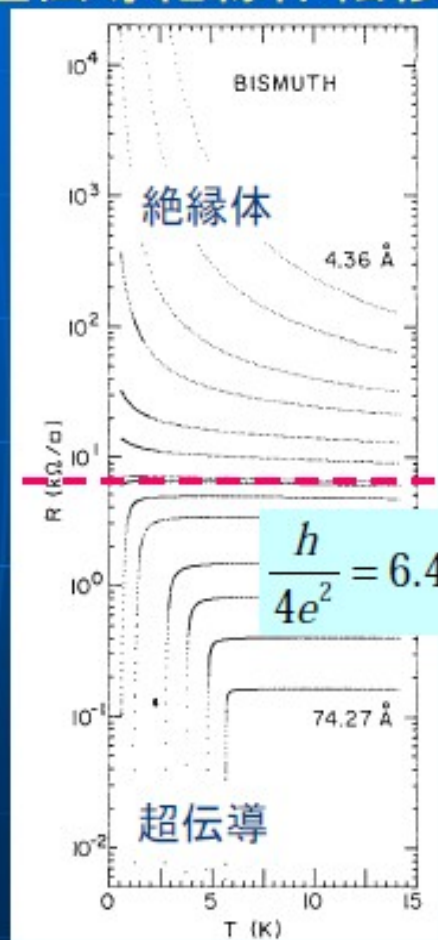
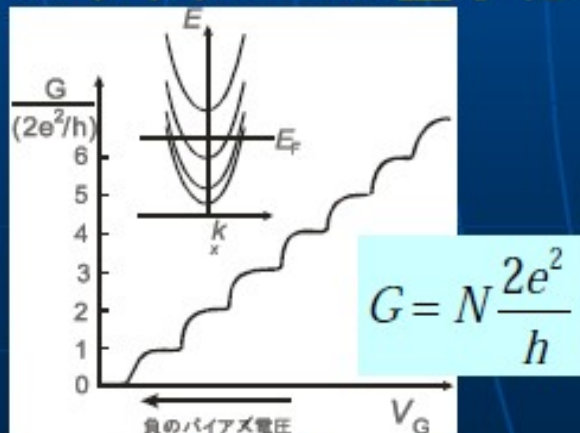
電子局在



$$\sigma_{2D} = \frac{ne^2\tau}{m} - \frac{Pe^2}{\pi h} \ln \frac{T}{T_0}$$

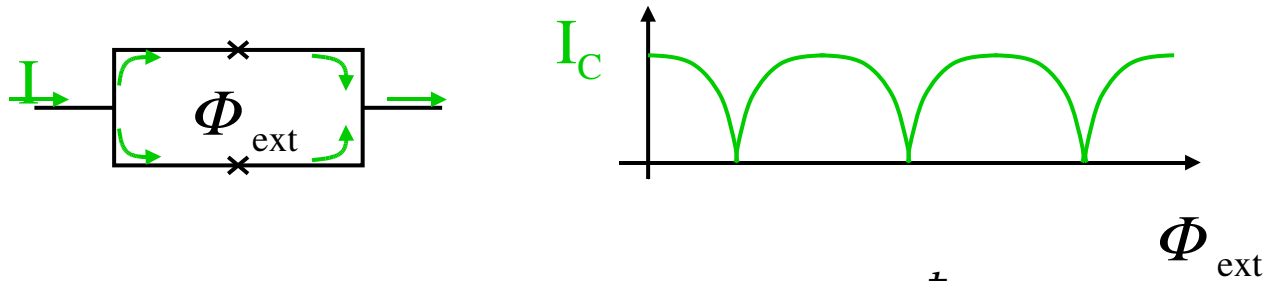
古典伝導度+量子補正

コンダクタンスの量子化

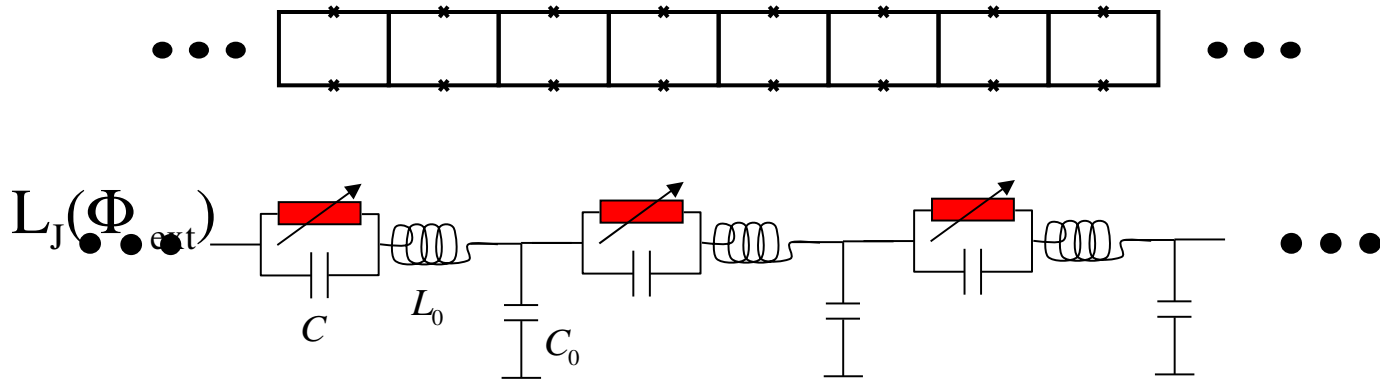


物質によらない普遍的物理

1D SQUID array as tunable Josephson transmission line



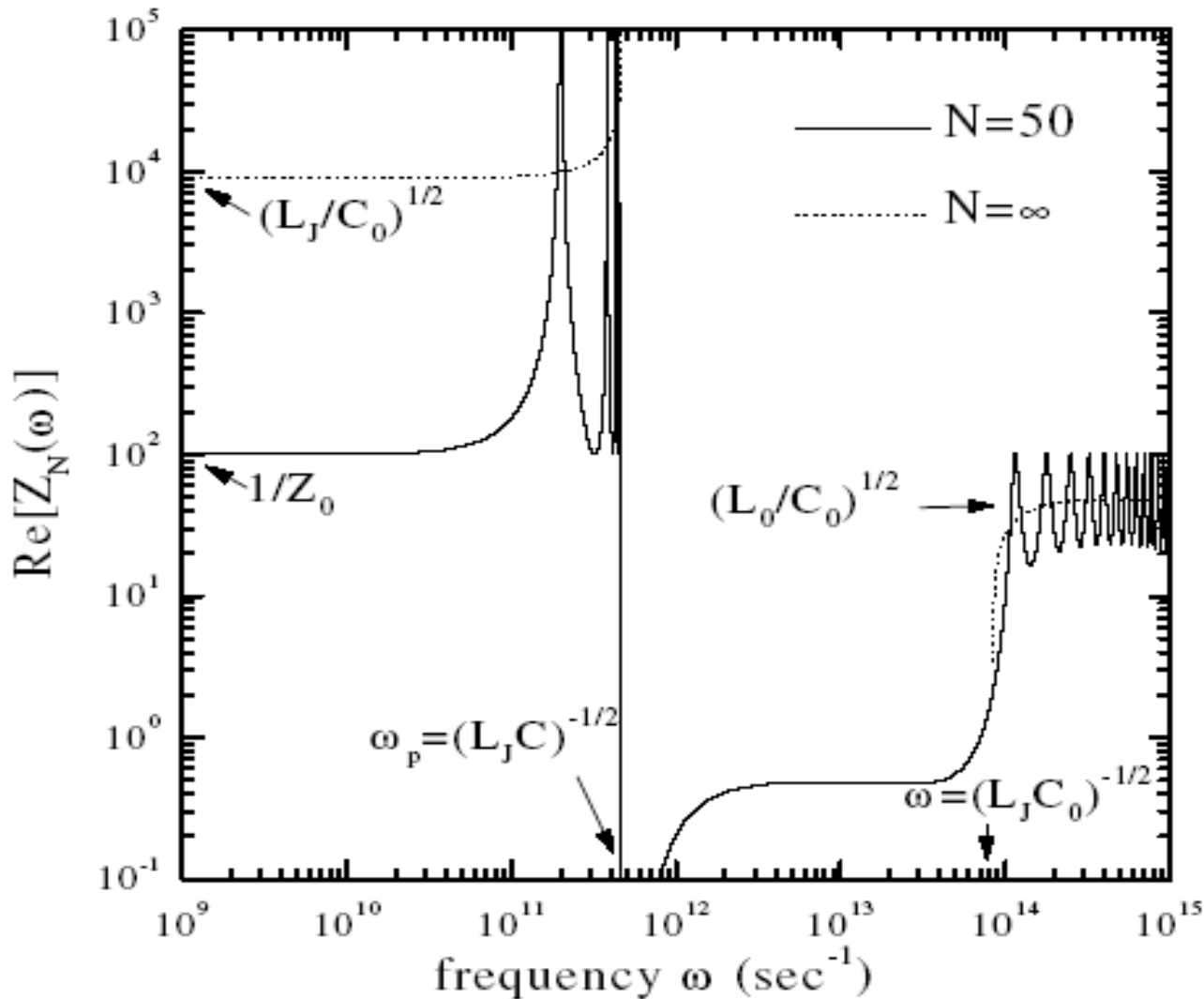
Tunable Josephson Inductance $L_J = \frac{\hbar}{2eI_C(\Phi_{\text{ext}})}$



Transmission Line Impedance:

$$N \rightarrow \infty, \quad \omega \ll \omega_p = \frac{1}{L_J C} \quad \Rightarrow \quad Z_A = \sqrt{\frac{L_J + L_0}{C_0}} \simeq R_Q \sqrt{\frac{4E_C}{E_J}} \sqrt{\frac{C}{C_0}}$$

Linear model - impedance



$$C = 3.5 \text{ fF}$$

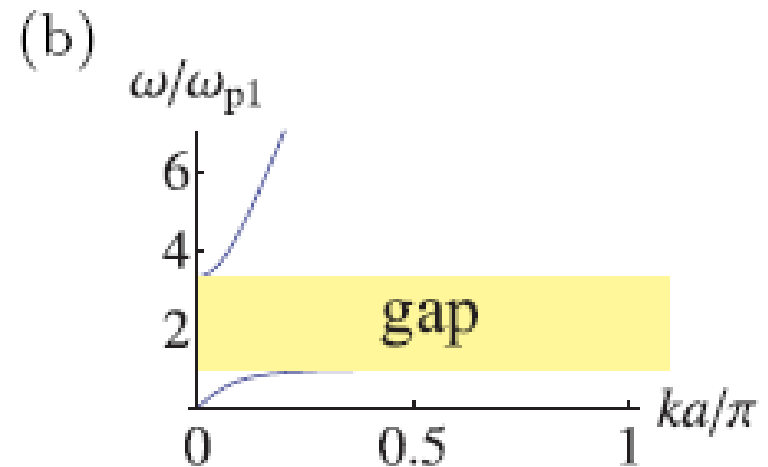
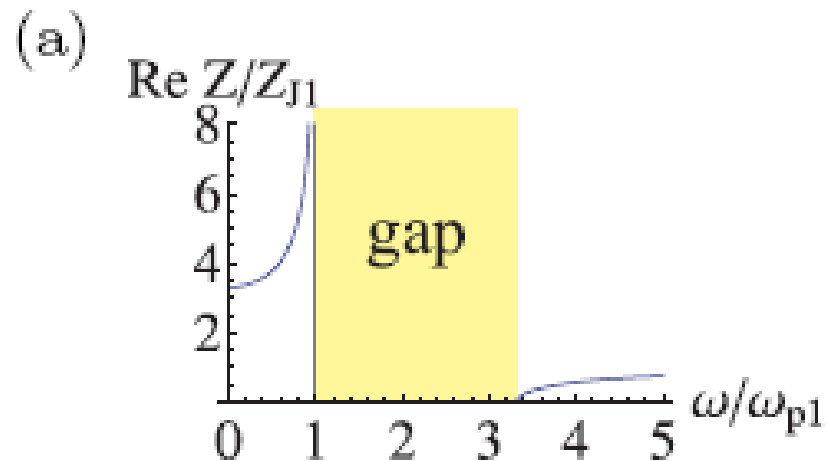
$$C_0 = 0.016 \text{ fF}$$

$$L_J = 1.1 \text{ nH}$$

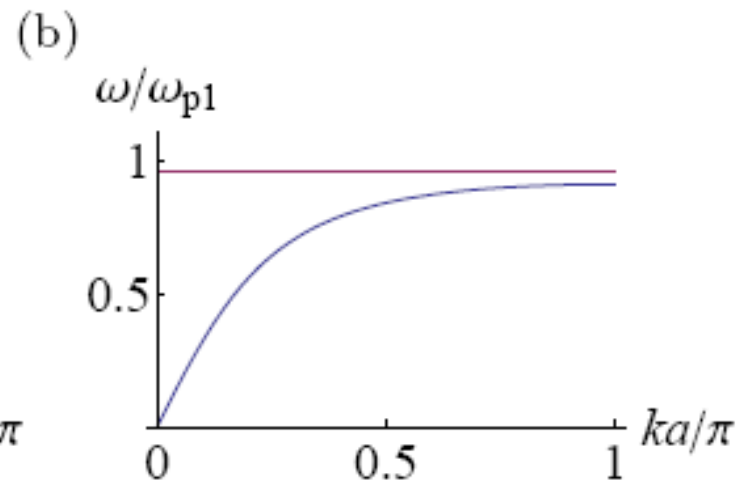
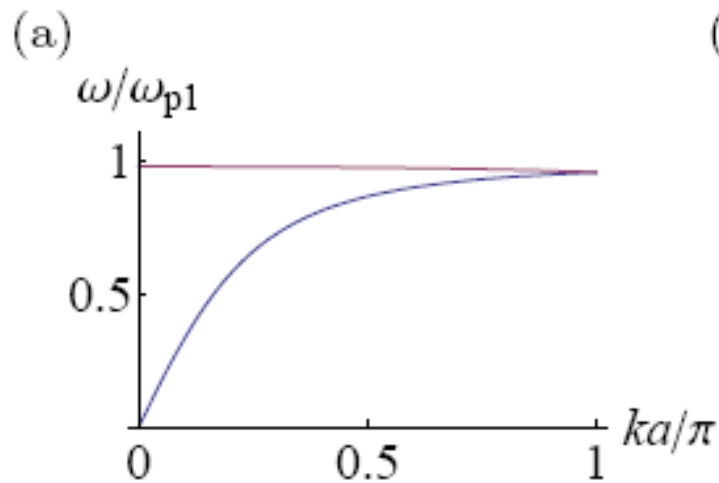
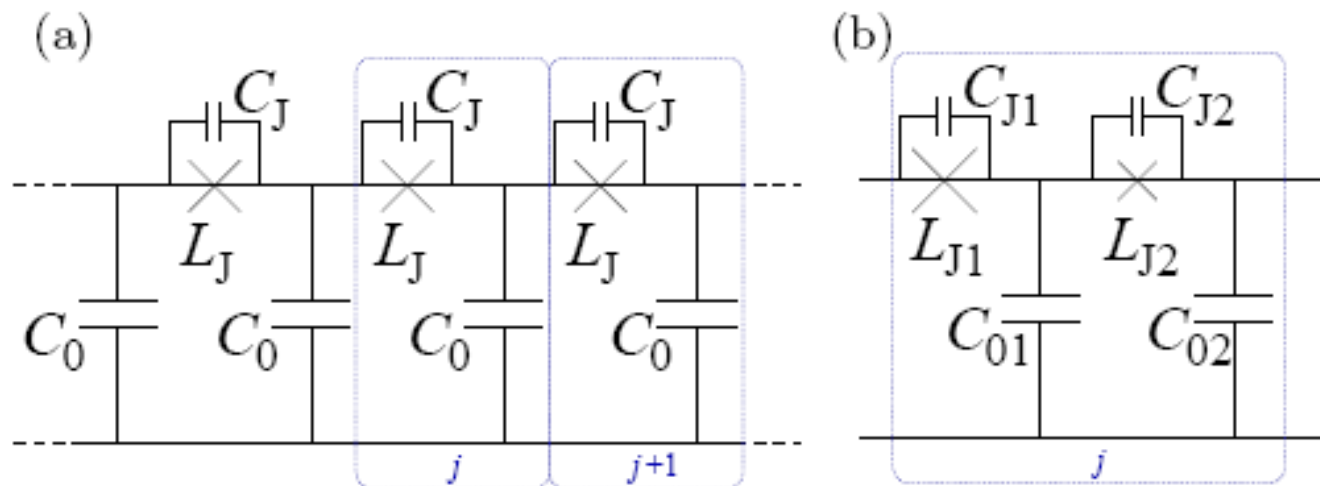
$$Z_0 = \sqrt{\frac{L_0}{C_0}} = 50 \Omega$$

**Circuit model of a
“photonic band
gap”**

Impedance, dispersion relation, Density of modes

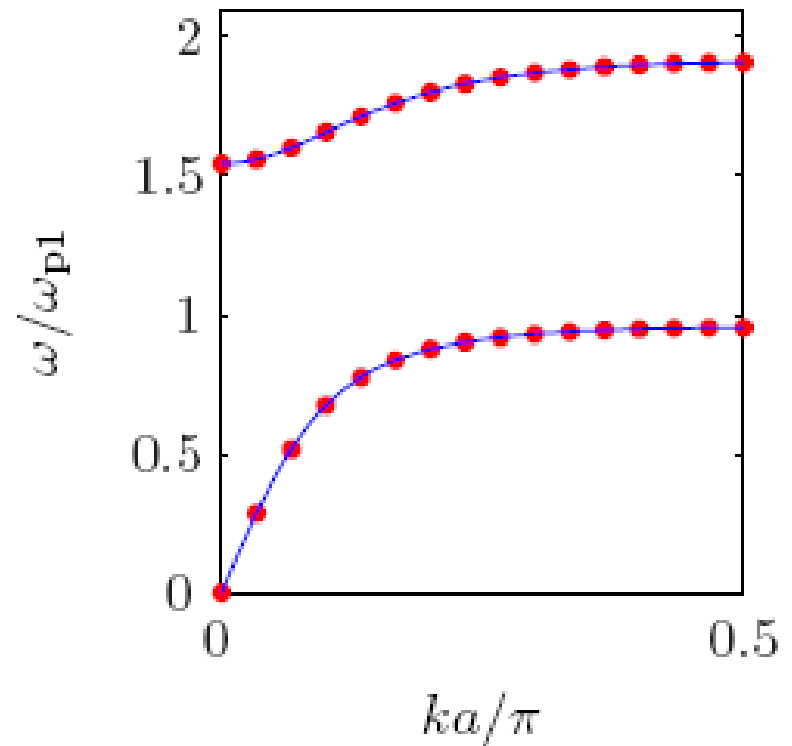
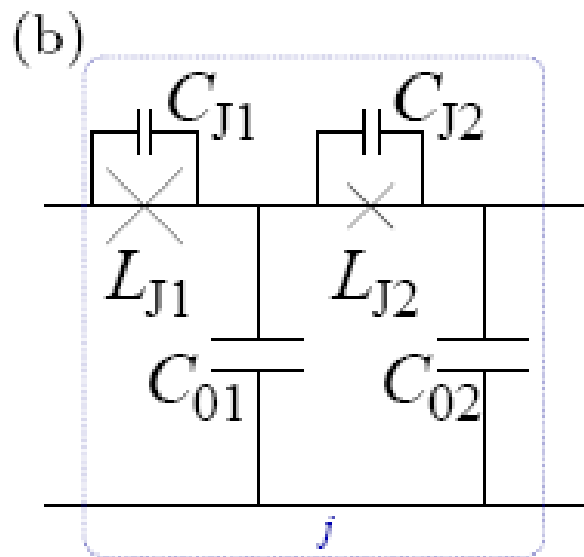


Lattice with a basis



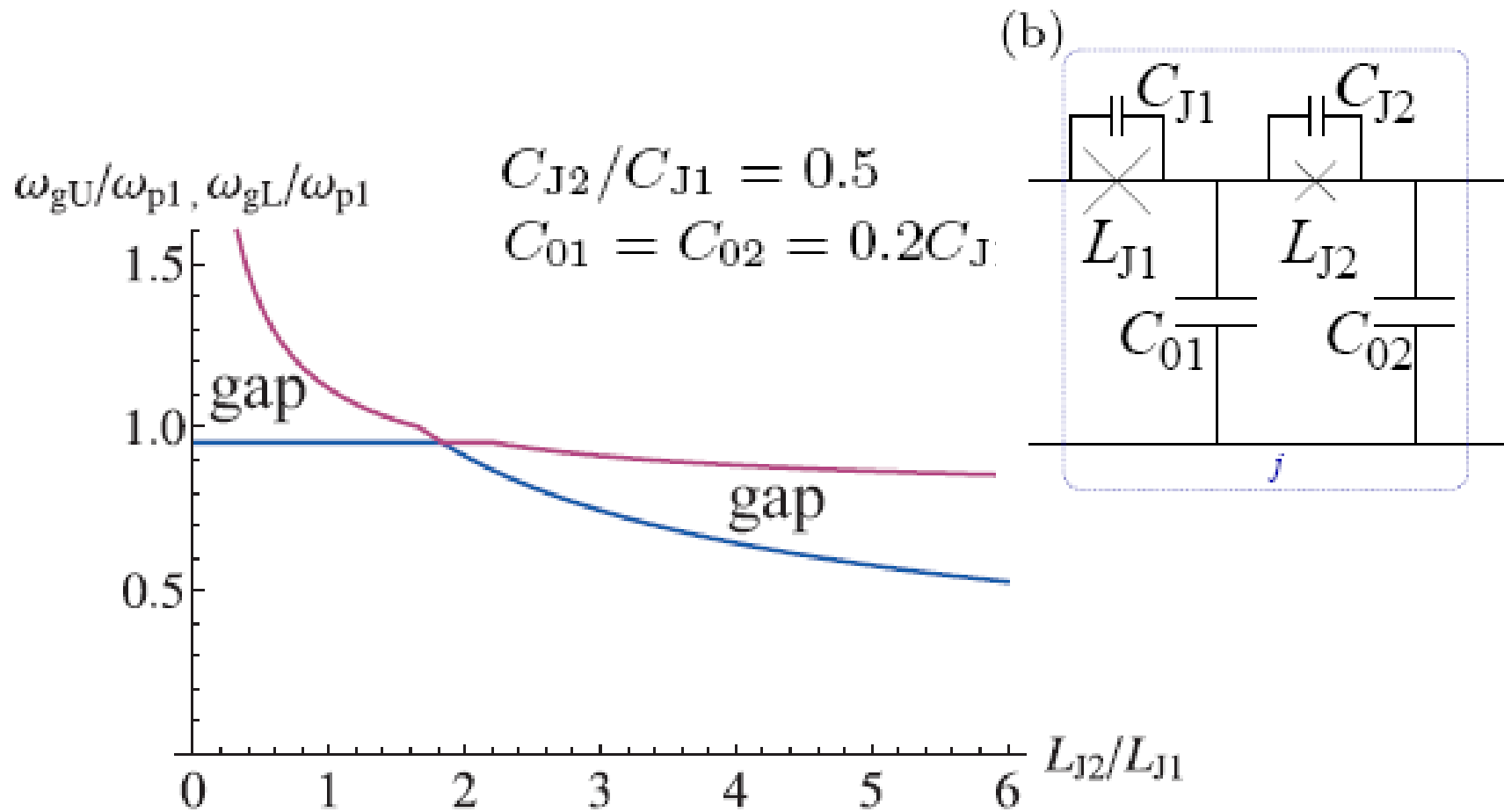
Gap when different plasma frequencies

When Junction Capacitance $>$ Capacitance to ground, $C_J > C_0$ we need $\omega_{p1} \neq \omega_{p2}$ in order to get gap.



$$L_{J2} = 0.25L_{J1} \text{ and } C_{01} = C_{02} = 0.2C_1 = 0.2C_2$$

Gap engineering by changing Plasma frequency



Transmission simulation, with disorder

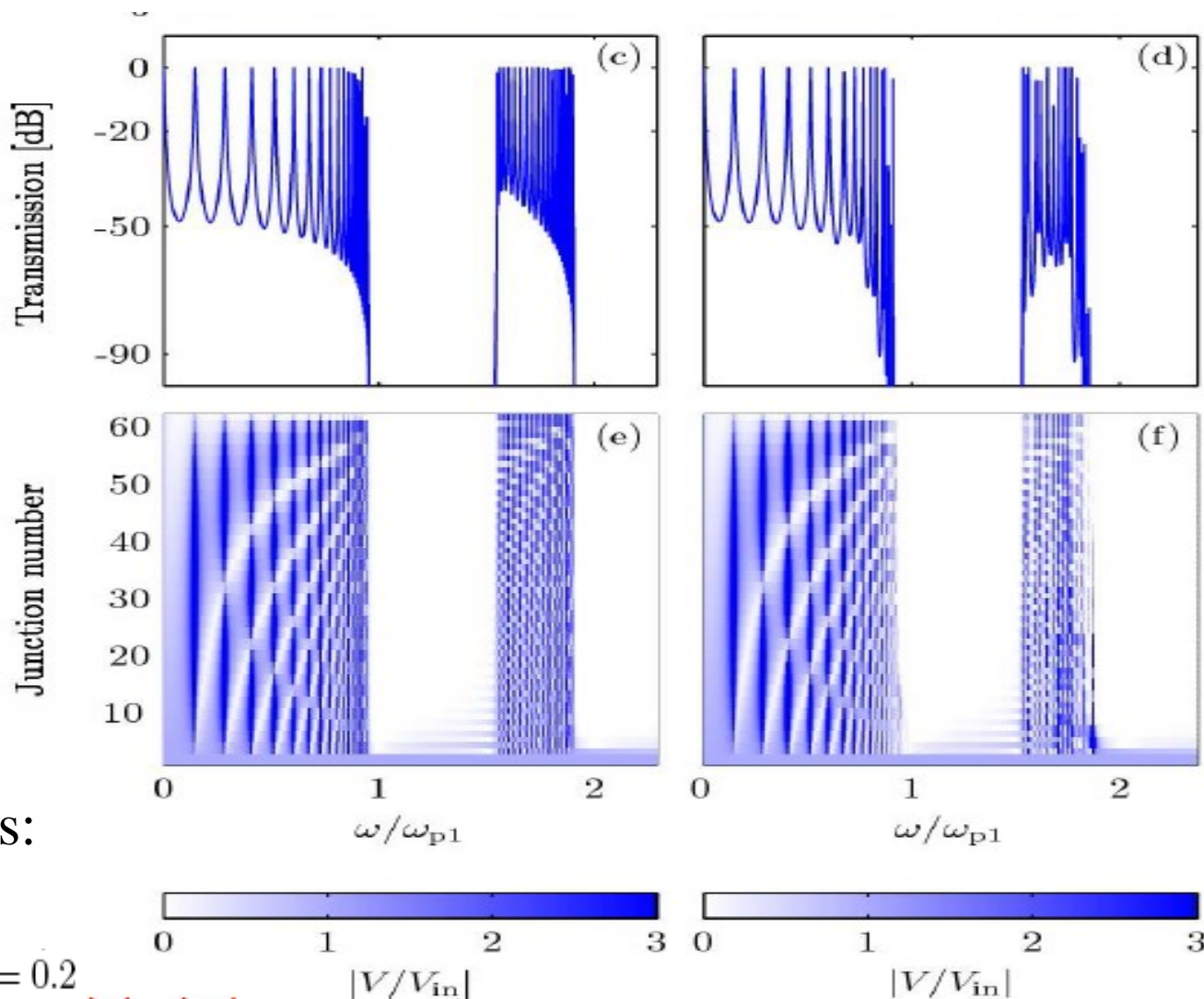
Transmission line impedance: $Z_A(0) = \frac{\sqrt{C_{01}C_{02}}}{C_{01} + C_{02}} \cdot \sqrt{\frac{L_{J1}}{C_{01}} + \frac{L_{J2}}{C_{01}} + \frac{L_{J1}}{C_{02}} + \frac{L_{J2}}{C_{02}}}$.

- Impedance mismatch gives standing waves

- resonator without capacitor at ends

- Note: voltage node (current anti-node) in middle ($Z_A > Z_0$).

- Gap is a robust feature, nearly unaffected parameter spread (5% SD)



Simulation parameters:

$$L_{J2} = 0.25L_{J1}$$

$$C_{01} = C_{02} = 0.2C_1 = 0.2C_2$$

$$Z_{in} = Z_{out}, \text{ and } Z_{in}/Z_A(0) = 0.2$$

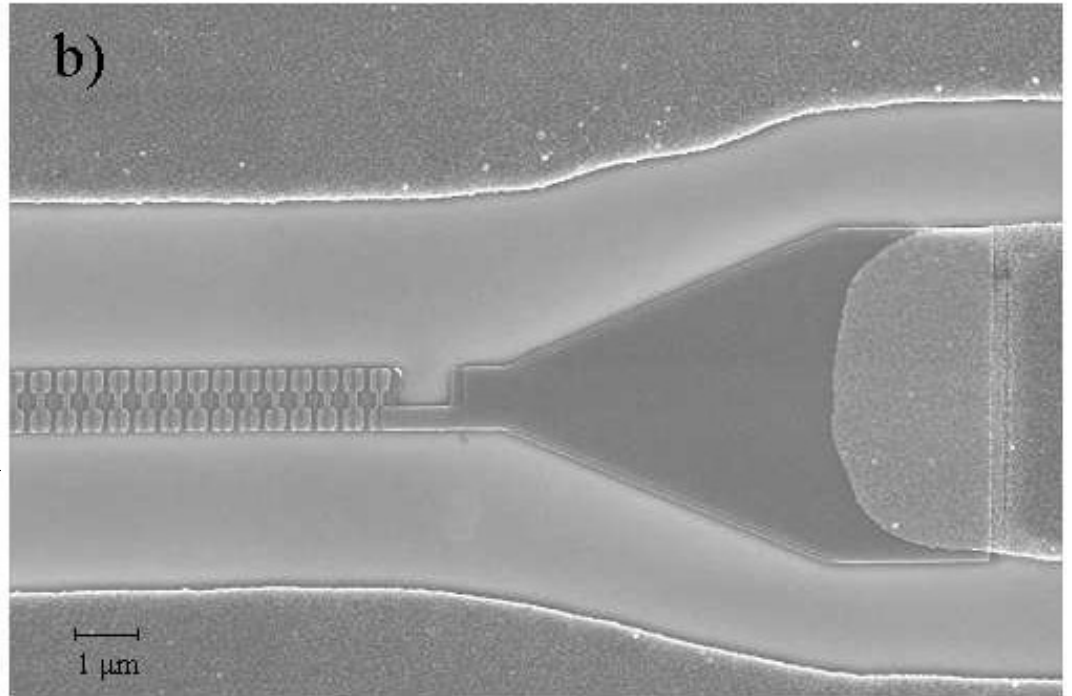
$$C_0 < C_J \quad \text{or} \quad C_0 > C_J$$

CPW geometry:

naturally $C_0 \ll C_J$

$\omega_{p1} \neq \omega_{p2}$ necessary for gap

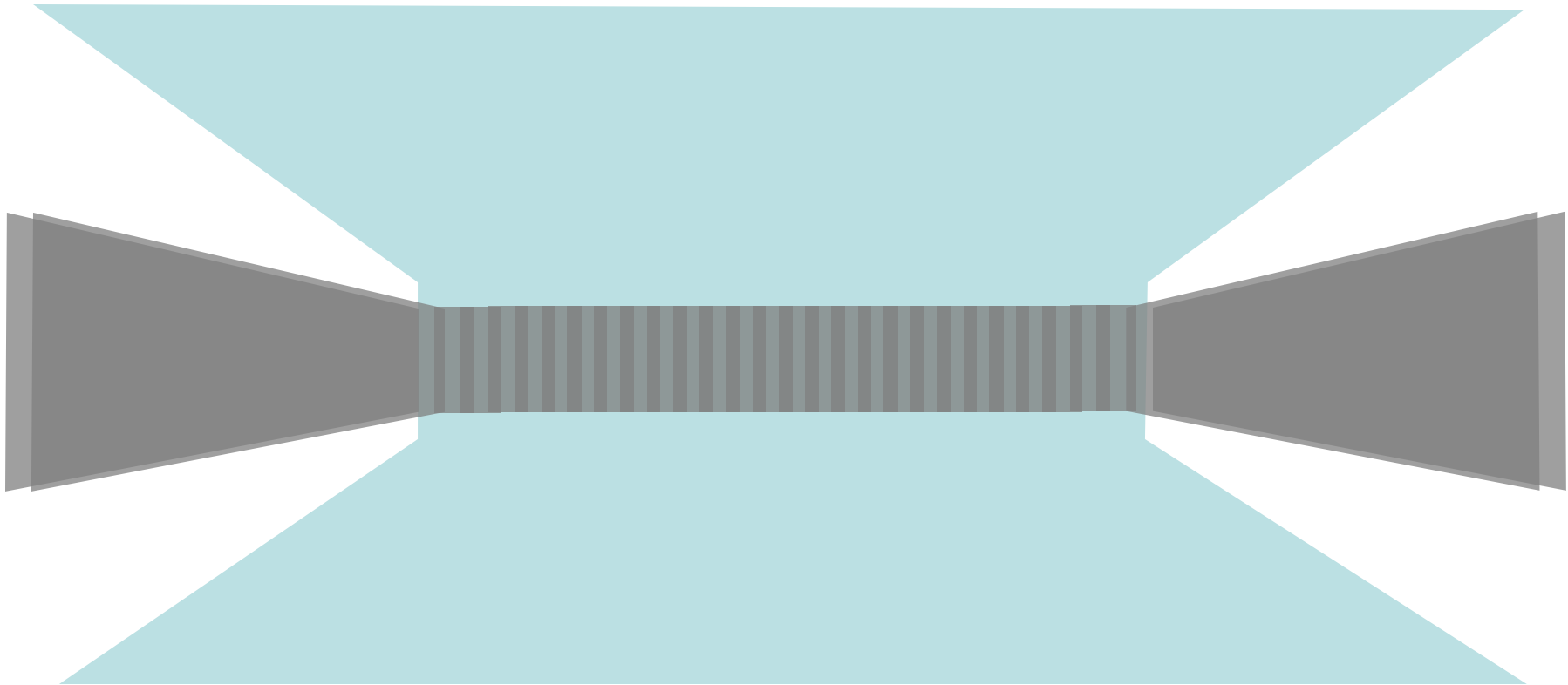
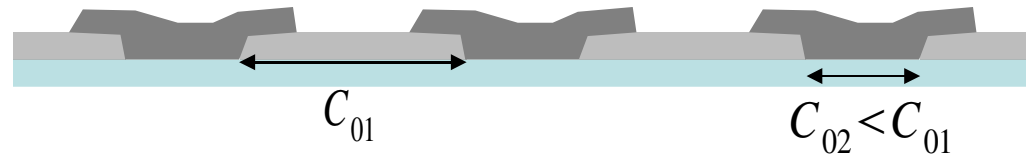
Not easy to realize for Al shadow evaporation junctions.



For $C_J < C_0$ we can have gap with $\omega_{p1} = \omega_{p2}$, if $C_{01} \neq C_{02}$.

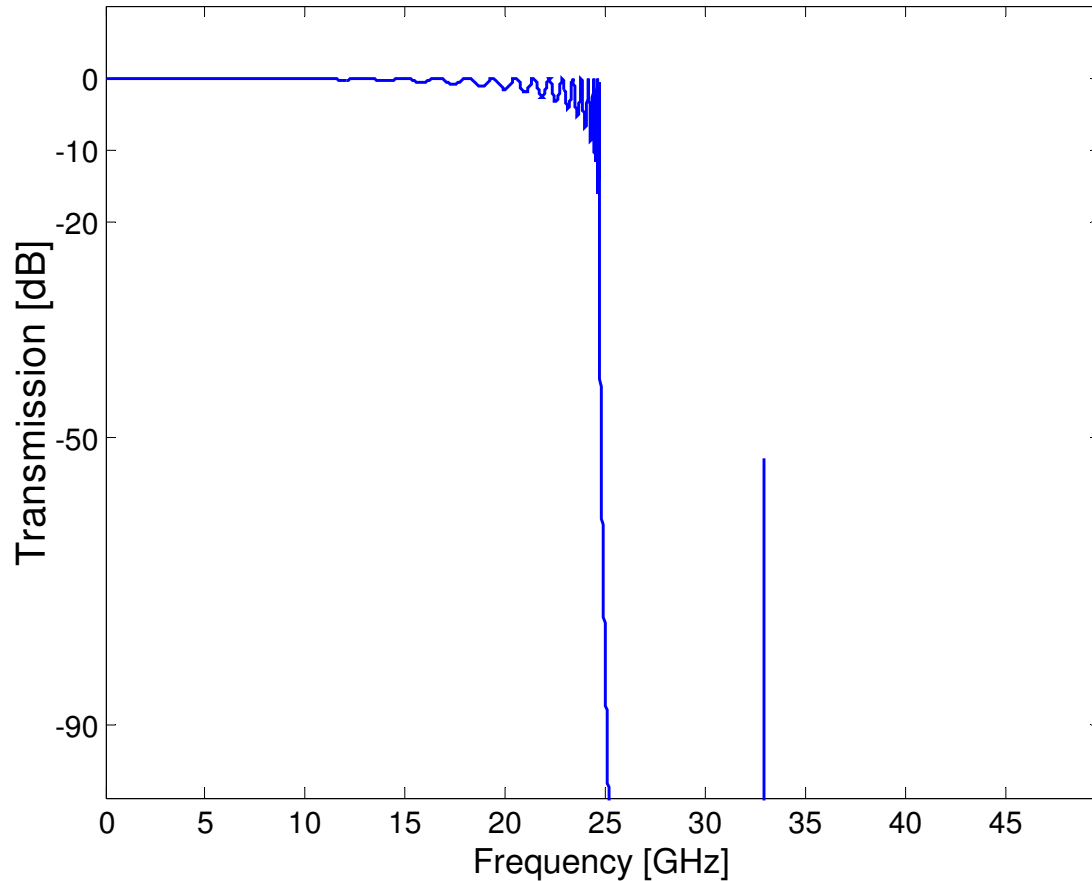
Stripline geometry to get large C_0 .

side view:



-  Layer 1 ground plane w/ heavy oxidation
-  Layer 2,3 Array, shadow evaporation

Simulation for Stripline geometry



Aluminum junctions on
Heavily oxidized Al ground
plane (insulating to gnd plane)

Heavy junction oxidation -
 $\omega_p = 33\text{GHz}$

$$Z_{\text{in}} = Z_{\text{out}} = 60 \Omega$$

$N=20$ unit cells

Shadow Mask dimensions:

$$L=8\mu\text{ m}$$

$$w=2\mu\text{ m}$$

$$D=0.2\mu\text{ m}$$

$$s=0.8\mu\text{ m}$$

$$\rightarrow Z_A = 61.4 \Omega$$

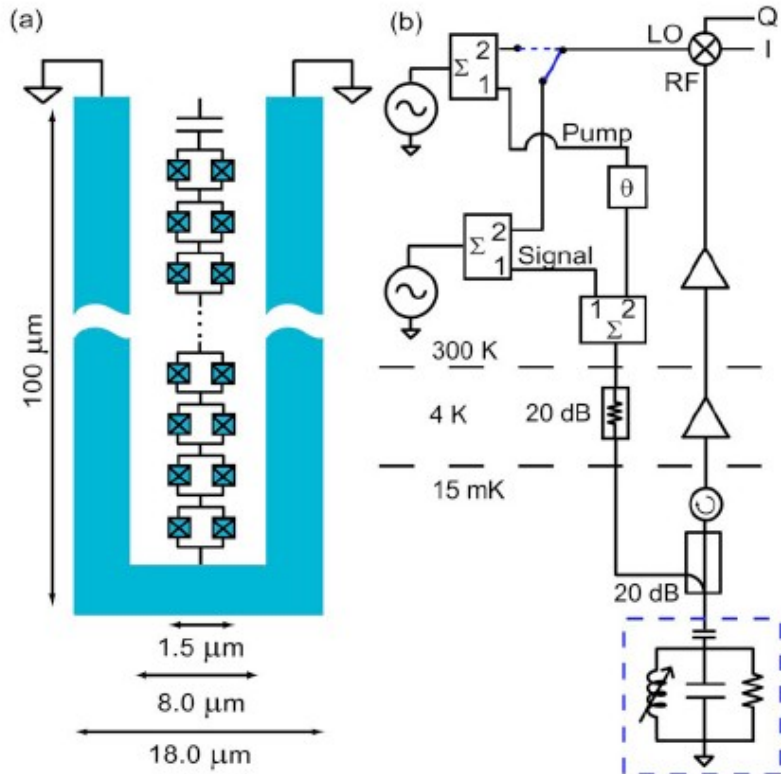


Classical Nonlinear Electrodynamics

APPLIED PHYSICS LETTERS 91, 083509 (2007)

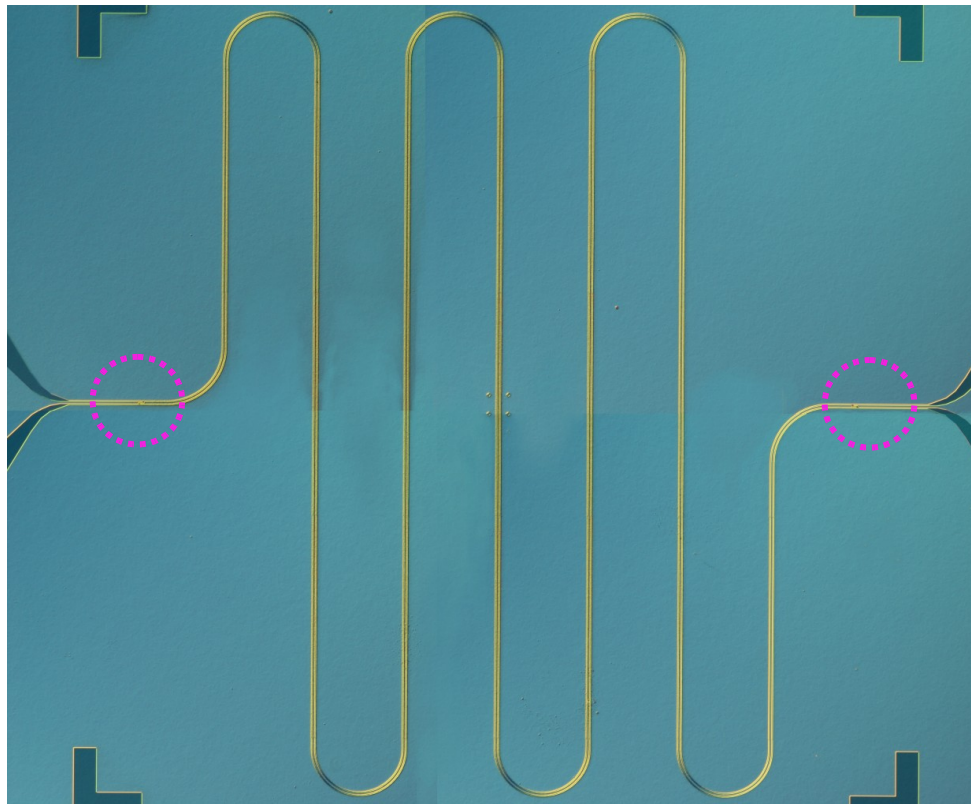
Widely tunable parametric amplifier based on a superconducting quantum interference device array resonator

M. A. Castellanos-Beltran^{a)} and K. W. Lehnert



- JJ gives current dependent inductance – nonlinear inductance
- SQUID makes for tunable nonlinearity
- Array resonator \Rightarrow nonlinear oscillator, narrow band parametric amplifier, band is tunable with SQUID.
- Matched array \Rightarrow wide band parametric amplifier. Attempted by Yurke et al. *Appl. Phys. Lett.* **69** (20), 11 November 1996

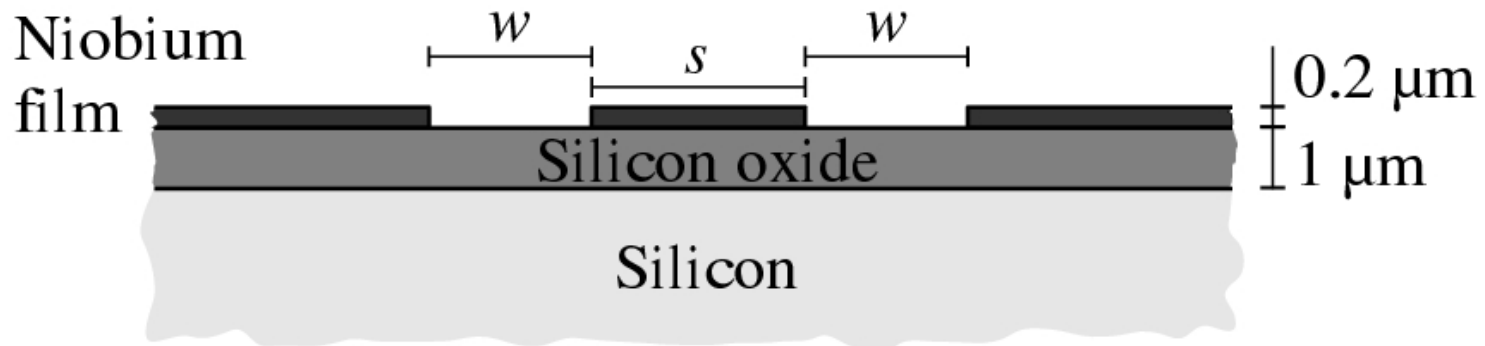
Array not really necessary: Thin-film, narrow strip, low critical current

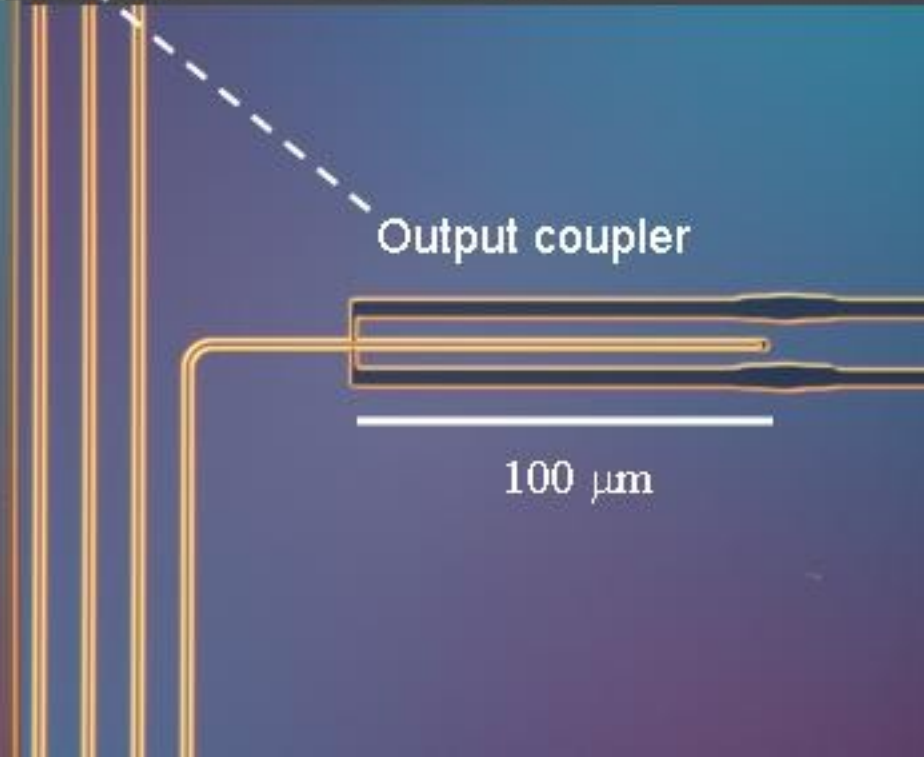
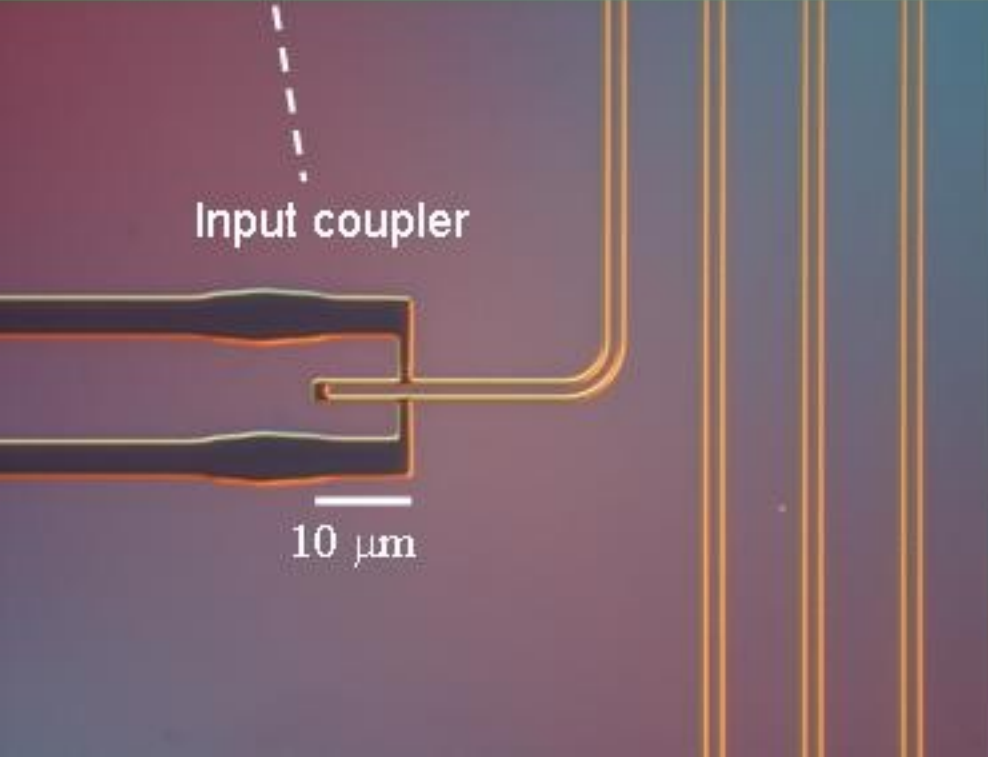
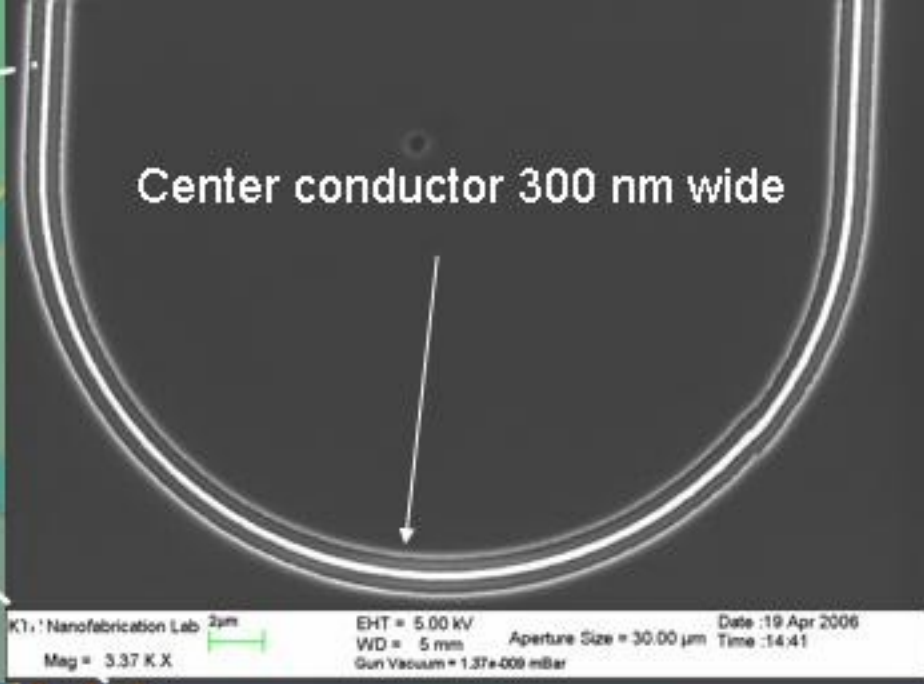
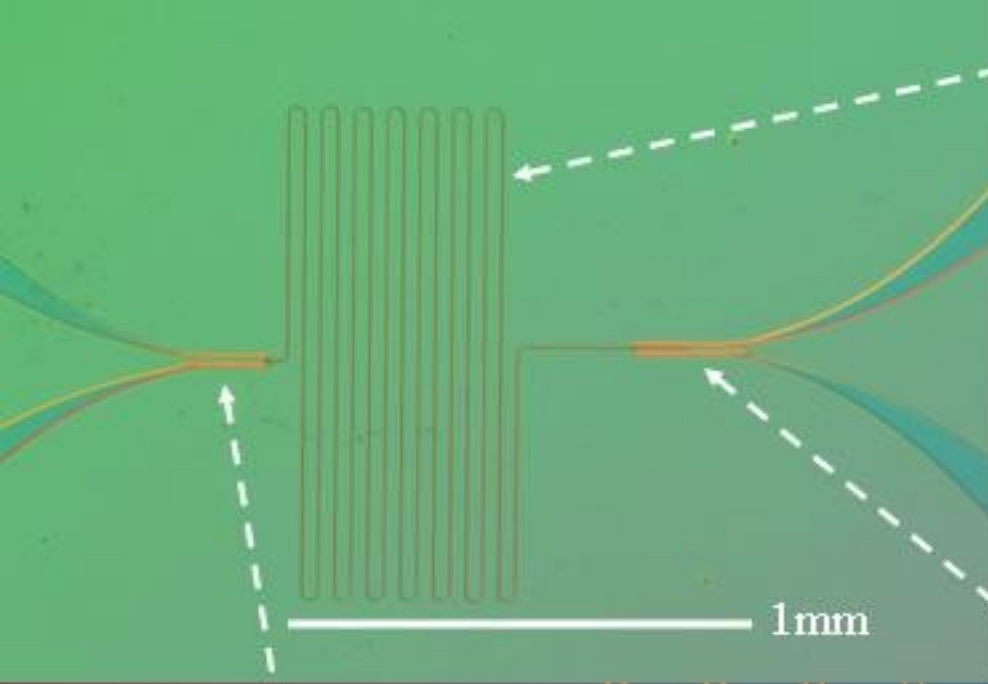


CPW resonators at KTH

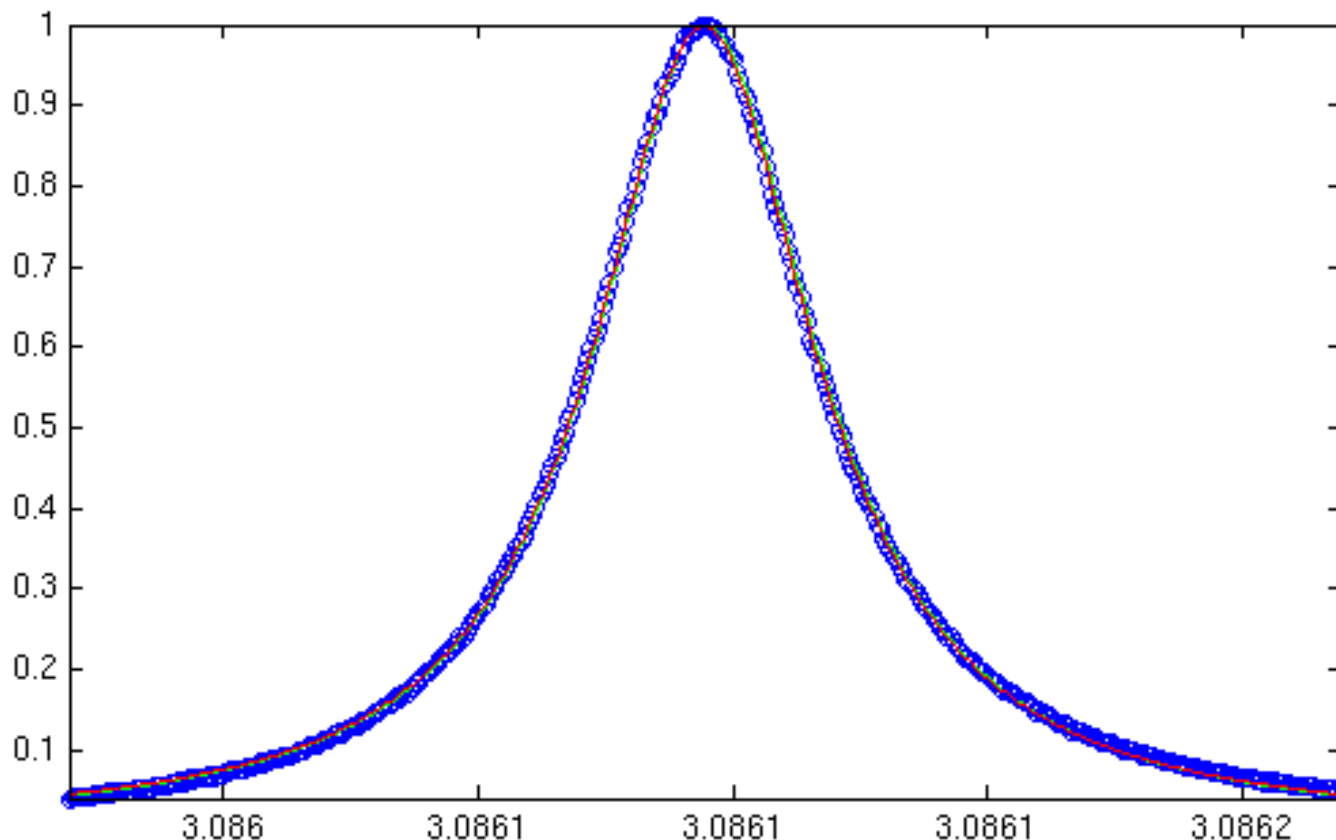
Niobium process:

- Nb thin film
- E-Beam Lithography
- Etch gaps BCl_3 ,





Low drive power, High Q oscillator



- Measured data
- Graphical fit, $f_0 = 3086094625$, $Q = 57415.714$, $A = 0$, $D = 1.7417e-05$
- Least square fit, $f_0 = 3086094258.2414$, $Q = 57485.615$, $A = 0.0015583$, $D = 1.7357e-05$

Increasing drive Power

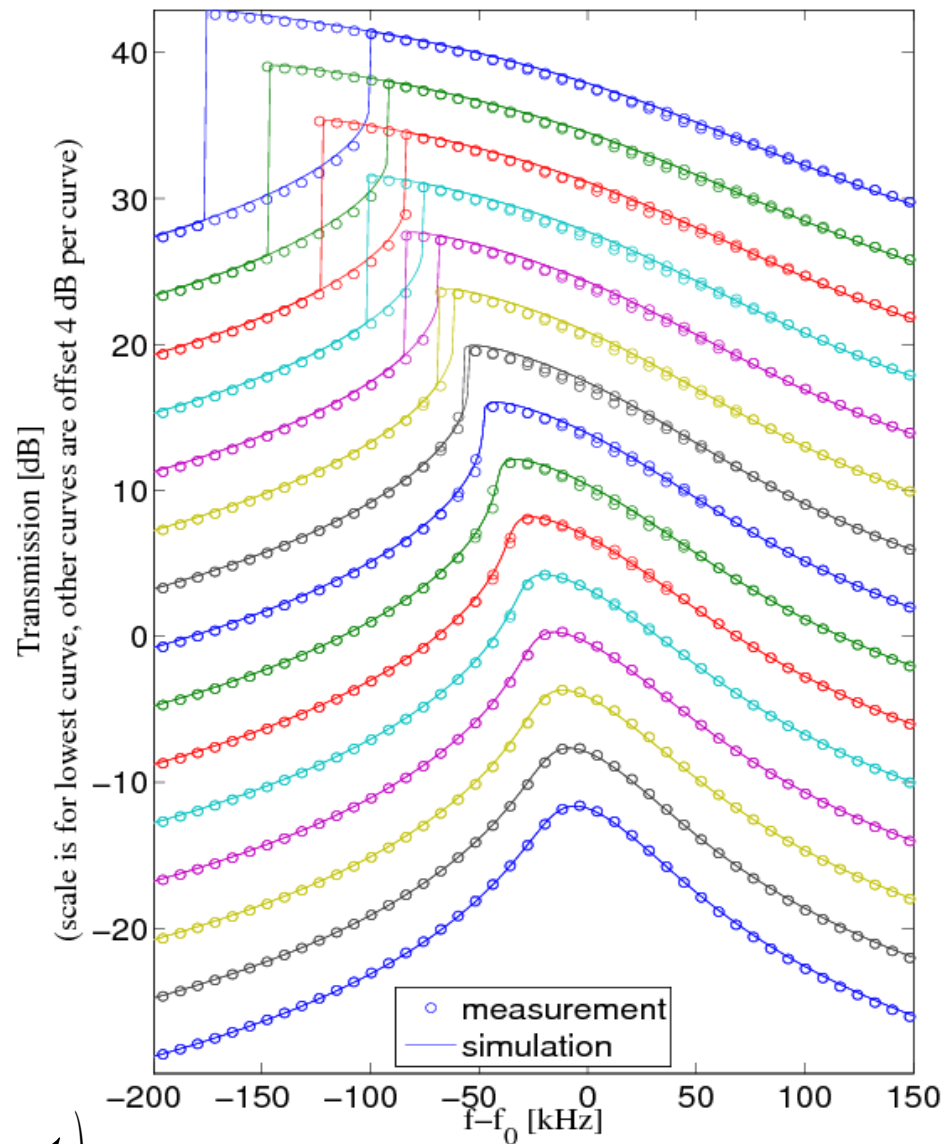
- Bending of resonance curve to lower frequency
- Bifurcation at critical power
- Well fit by nonlinear transmission line model
- Current dependent kinetic inductance:

$$L(I) = L_0 + \Delta L \left(\frac{I}{I_b} \right)^2$$

Duffing Oscillator

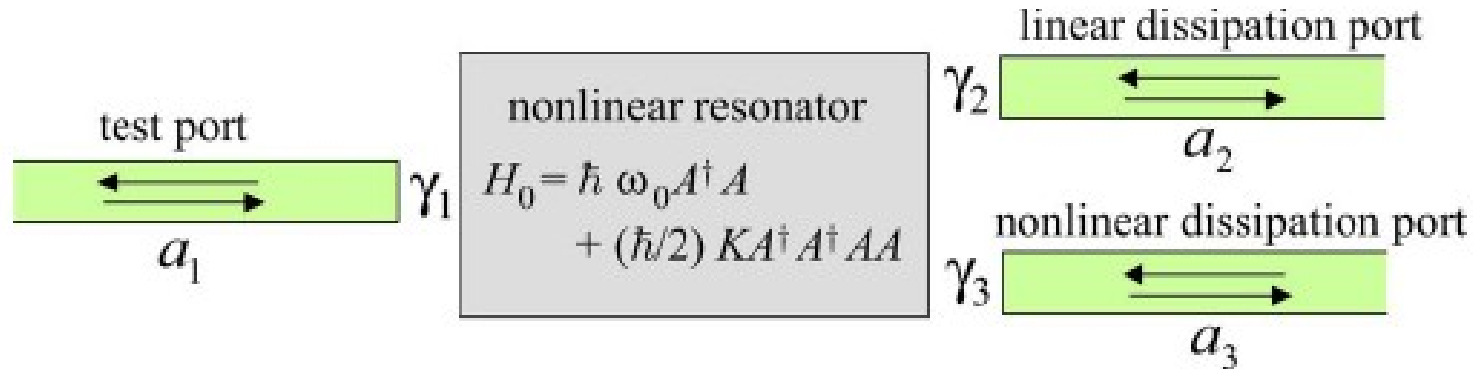
$$Q^2 \ddot{I} - \dot{I} - I - \beta I^3 = I_D \cos(\omega_D t)$$

$$\beta = \frac{\Delta L}{L_0 I_b^2}$$



Kerr Nonlinearity for Parametric Amplification

Yurke and Buks, Jour. Lightwave Tech. **24**, 5054 (2006)



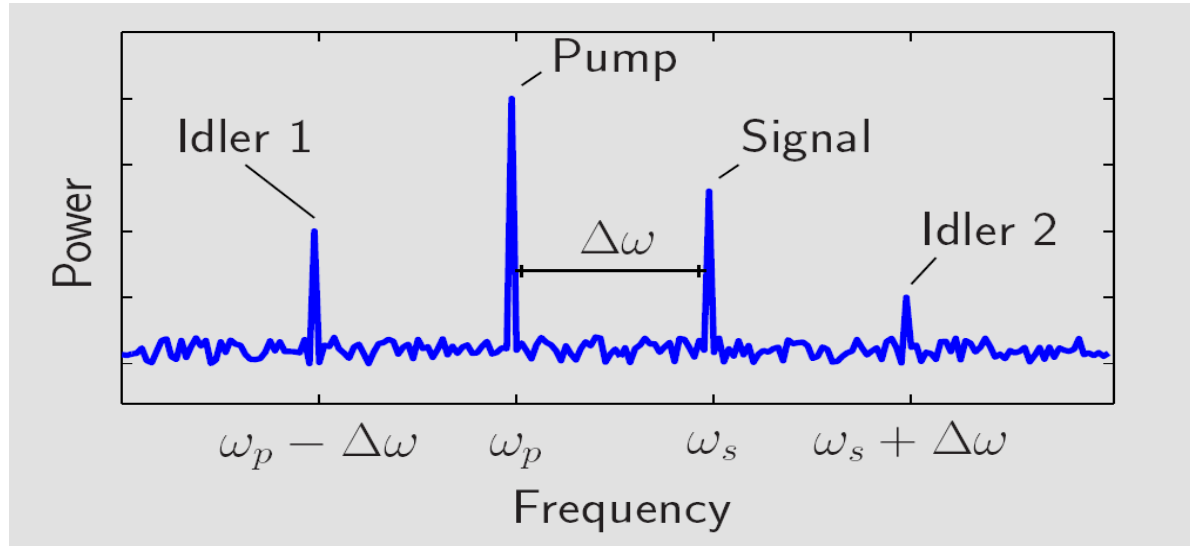
Condition for having a bistable regime $|K| > \sqrt{3} \gamma_3$

Critical input power at onset of bistability $\frac{4}{3\sqrt{3}} \frac{(\gamma_1 + \gamma_2)^3 (K + \gamma_3)}{(|K| - \sqrt{3} \gamma_3)^3}$

Also calculate parametric gain and intermodulation gain..... formulas--

Intermodulation and Parametric Amplification

$$I^3 = [I_p \cos(\omega_p t) + I_s \cos(\omega_s t)]^3 =$$
$$6I_p^2 I_s \cos(\omega_s t) + 3I_p^2 I_s \cos((\omega_p - \Delta\omega)t) + 3I_p I_s^2 \cos((\omega_s + \Delta\omega)t)$$



- Idlers - intermodulation products (IMPs), generated by nonlinearity
- Hierarchy of IMPs separated by $\Delta \omega$
- Degenerate mode $\omega_p = 2\omega_s$ ($\Delta \omega = \omega_s$)
- Doubly Degenerate mode $\omega_p = \omega_s$ ($\Delta \omega = 0$)
- Non-degenerate mode $\Delta \omega \neq 0 \ll \omega_s$

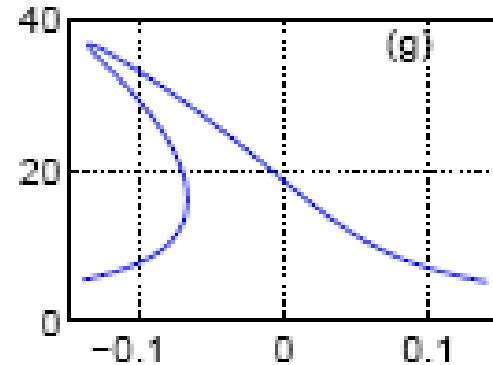
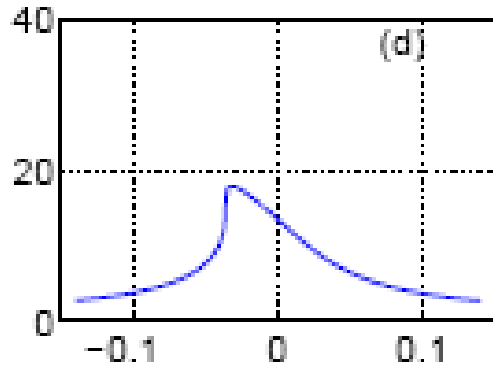
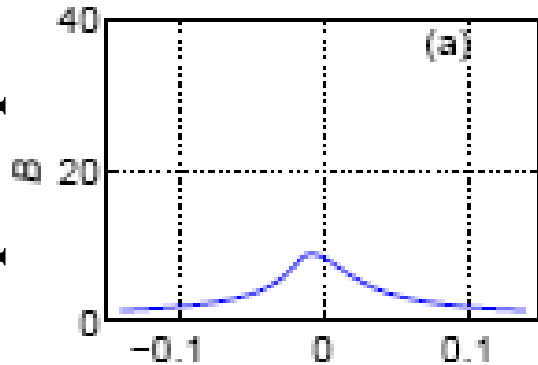
Kerr Non-Linearity for parametric Amplification

Pump Amplitude

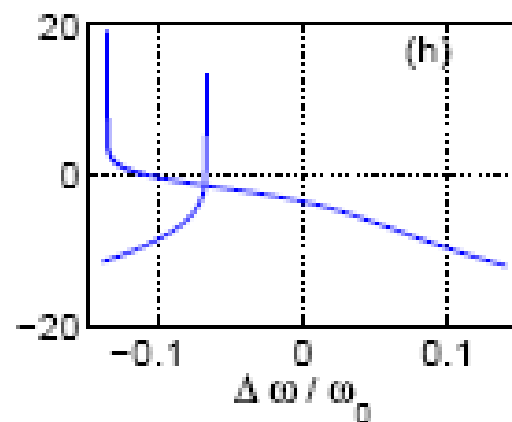
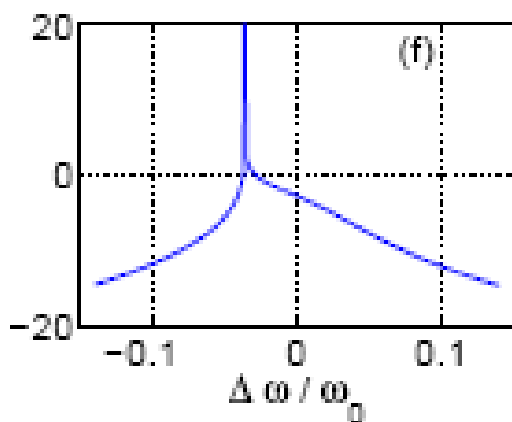
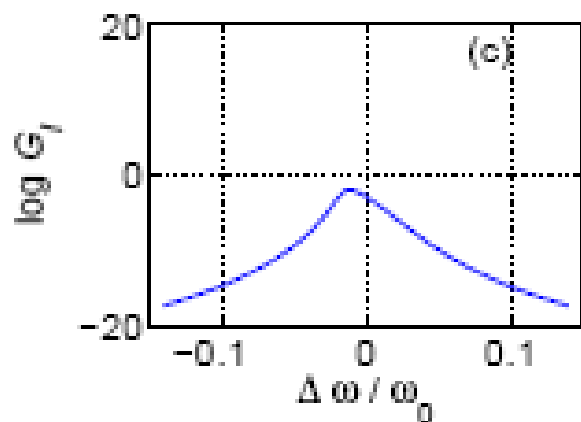
$$b_1^{\text{in}} = 0.5 b_{1c}^{\text{in}}$$

$$b_1^{\text{in}} = b_{1c}^{\text{in}}$$

$$b_1^{\text{in}} = 2 b_{1c}^{\text{in}}$$

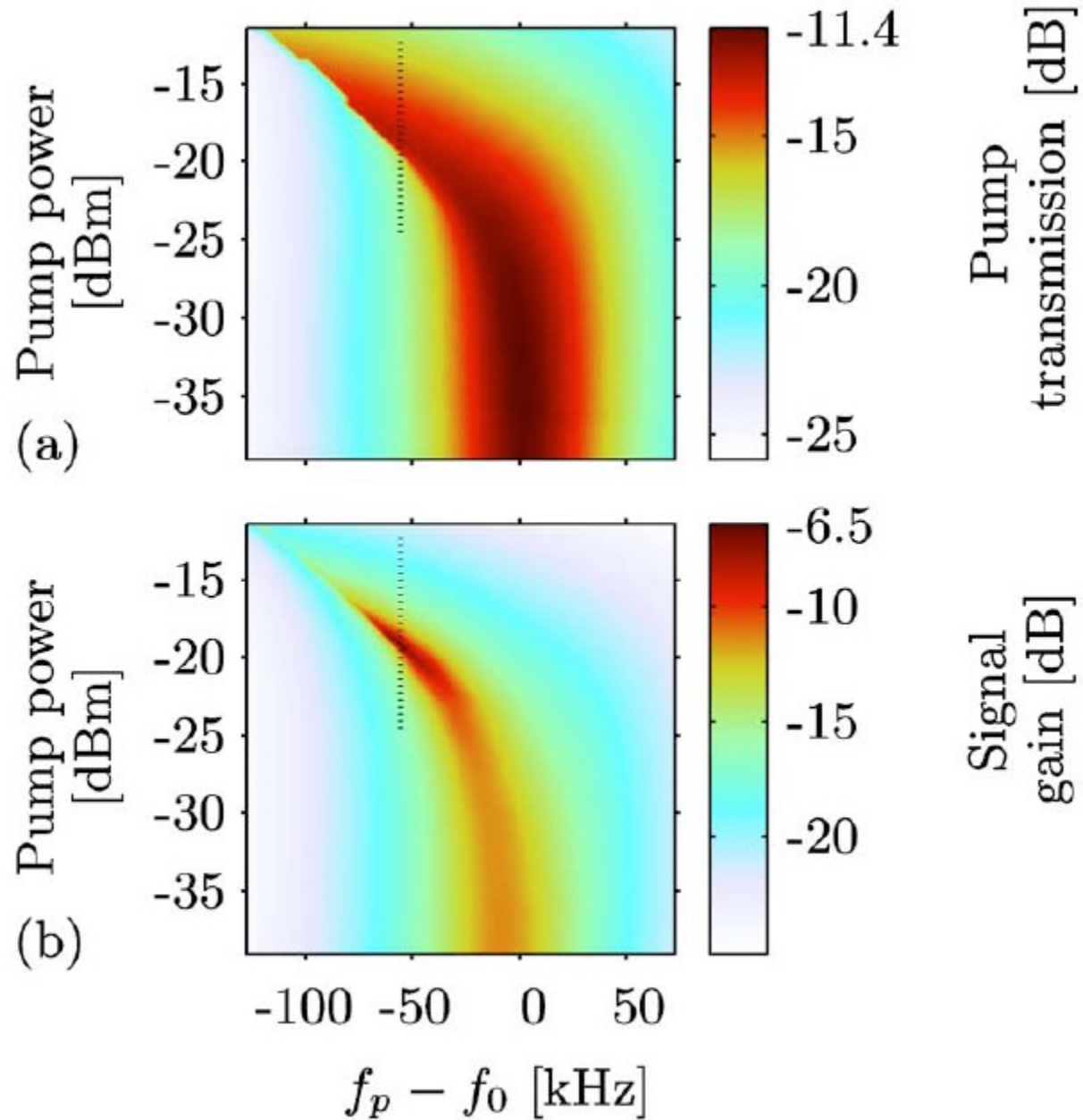


Gain ($\Delta \omega = 0$)

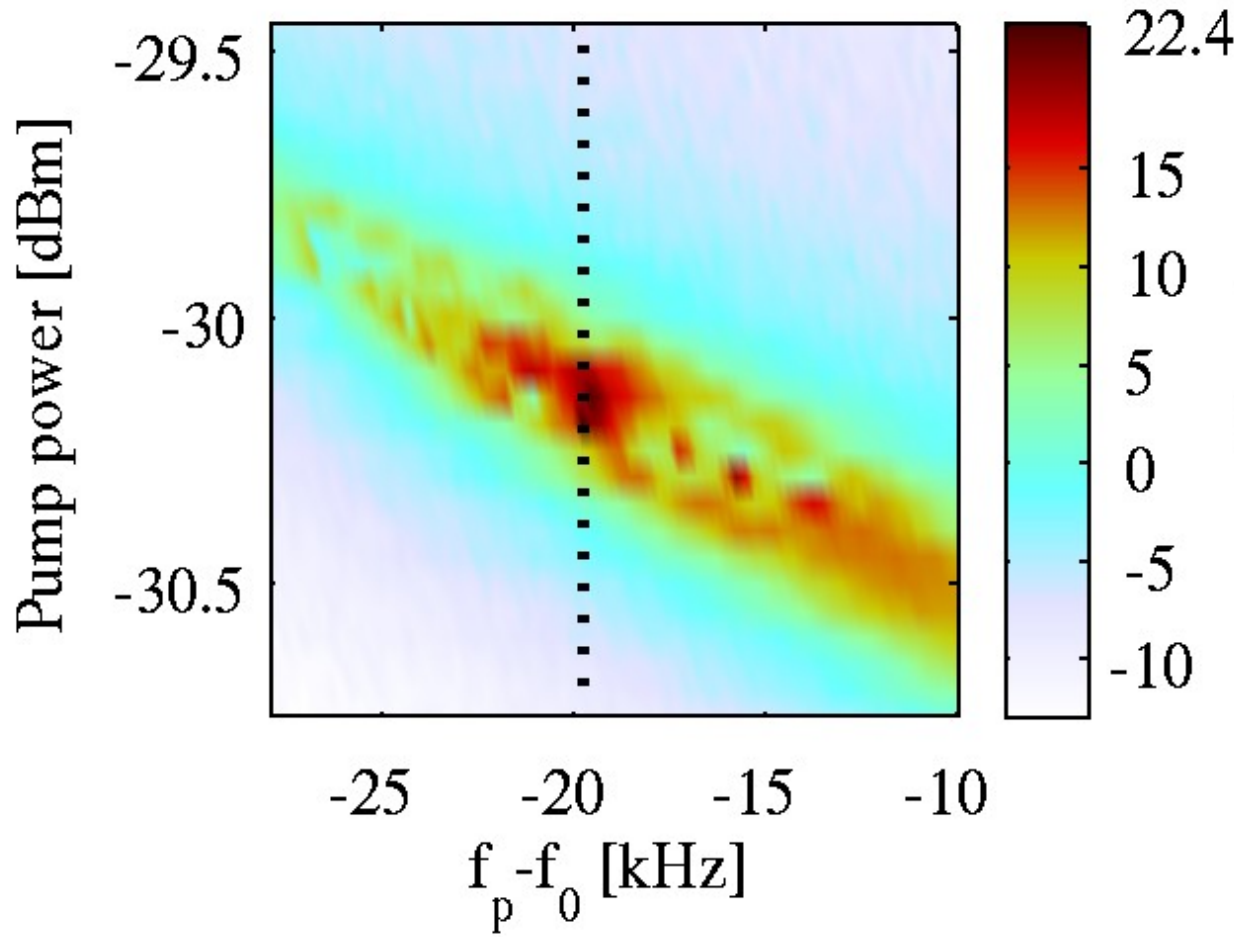


Yurke and Buks, Jour. Lightwave Tech. **24**, 5054 (2006)

Pump power dependence : Sample 1



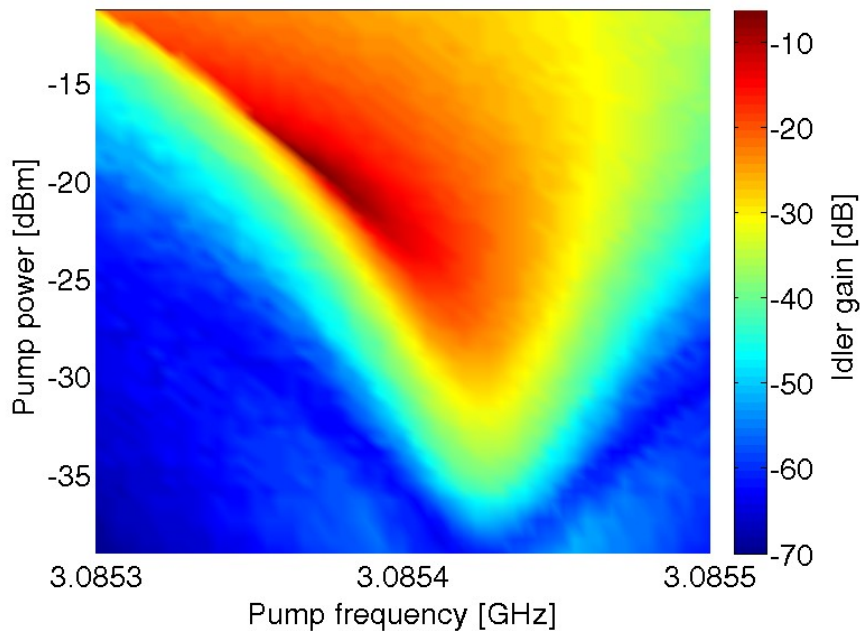
Zoom around maximum gain: sample 2



Nonlinearities and parametric amplification in superconducting stripline resonators. E. Tholén, A. Ergül, E. Doherty, F. M. Weber, F. Gregris and D. B. Haviland. *Appl. Phys. Lett.*

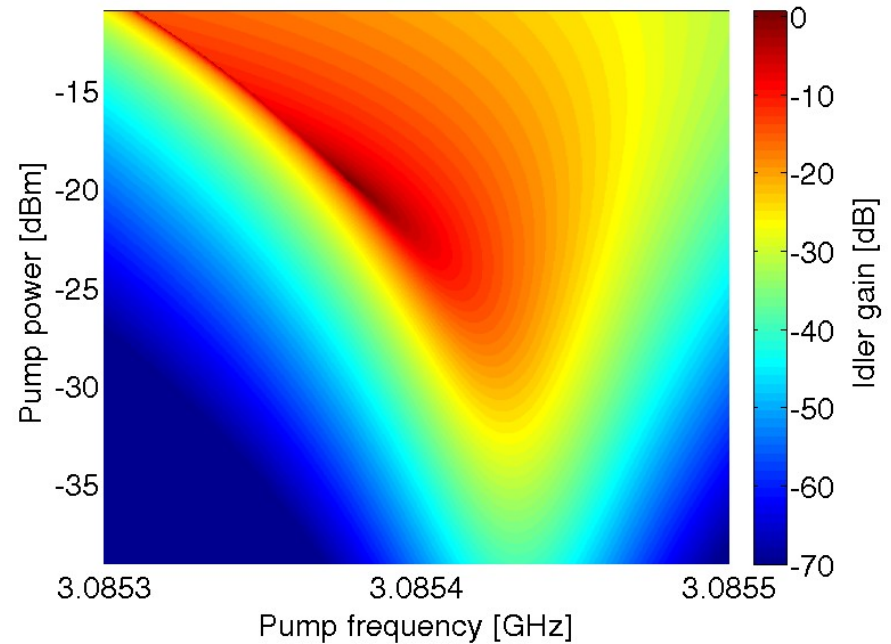
Intermodulation (Idler) Gain

Experiment (Sample 1)



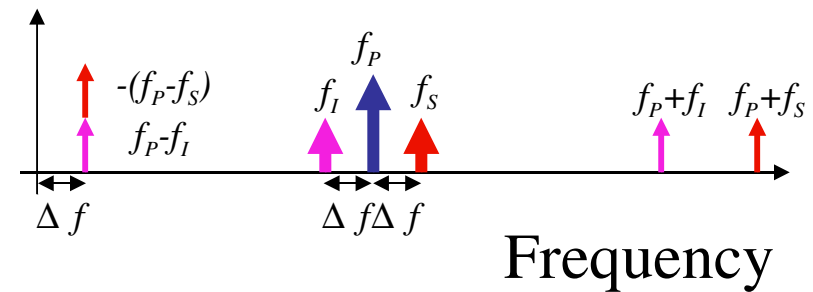
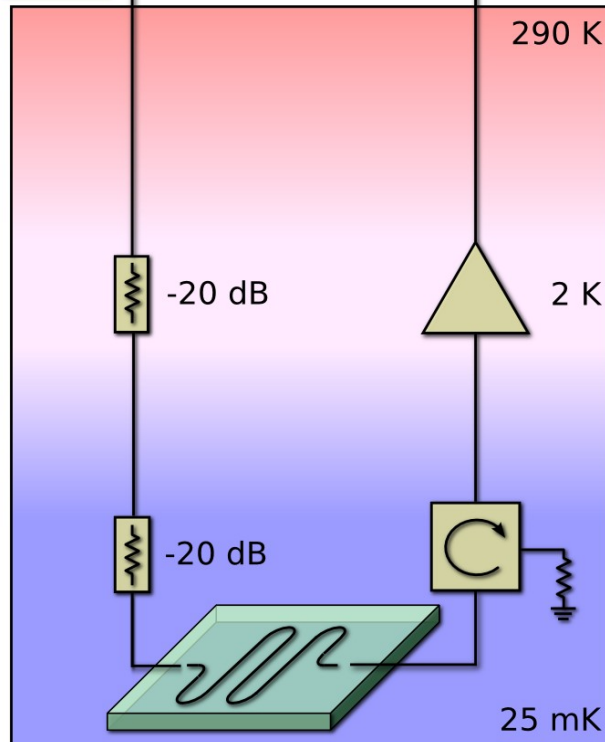
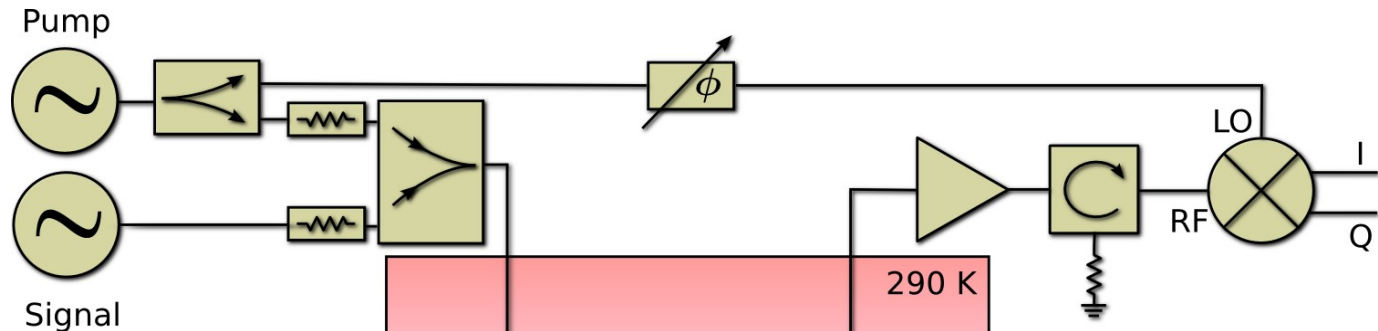
E. Tholén *et al.* unpublished

Theory



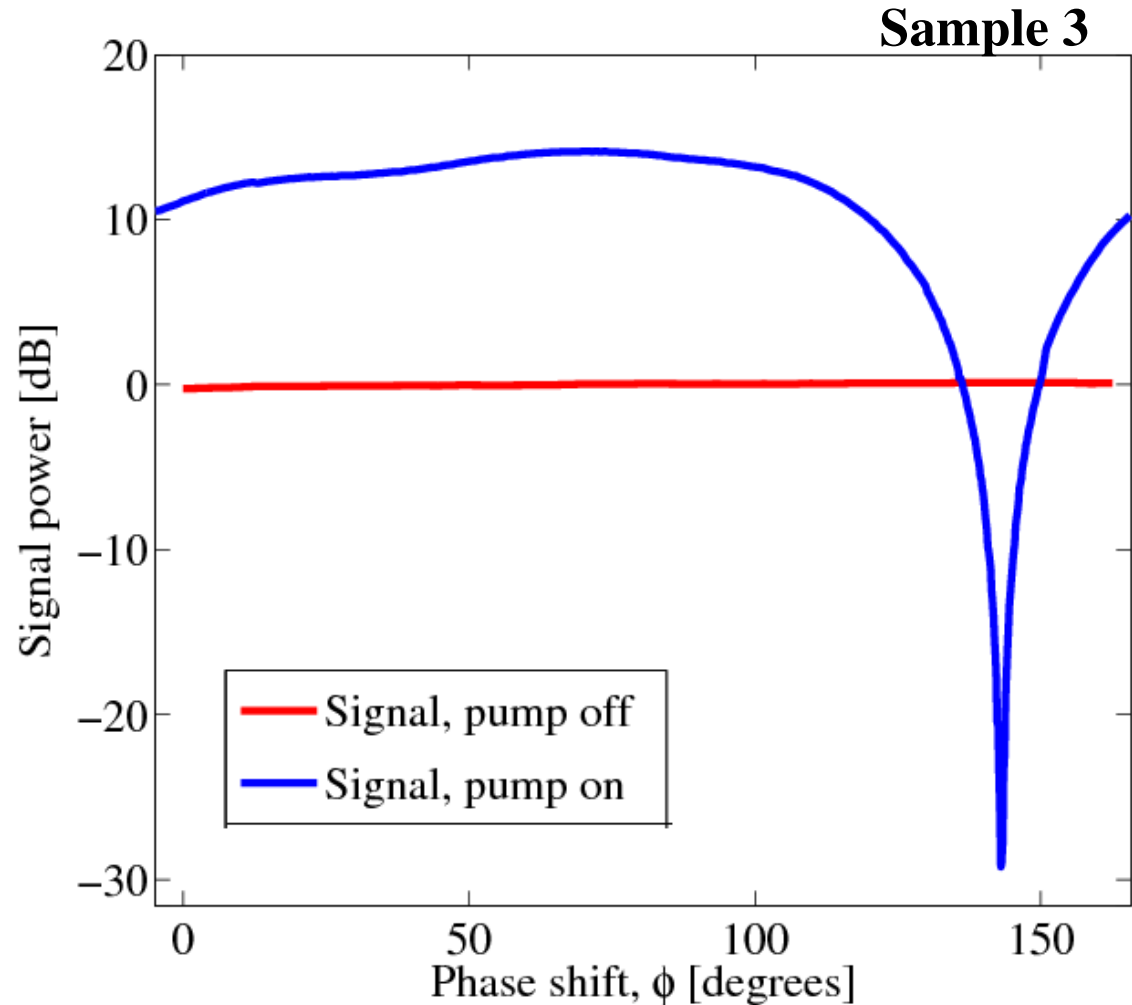
Yurke and Buks, *Jour. Lightwave Tech.* **24**, 5054 (2006)
Plots: E. Tholén

Phase sensitive amplification



-30dB signal deamplification

- Deamplify Noise – noise squeezing
- Deamplify quantum zero point fluctuations
⇒ Squeezed States

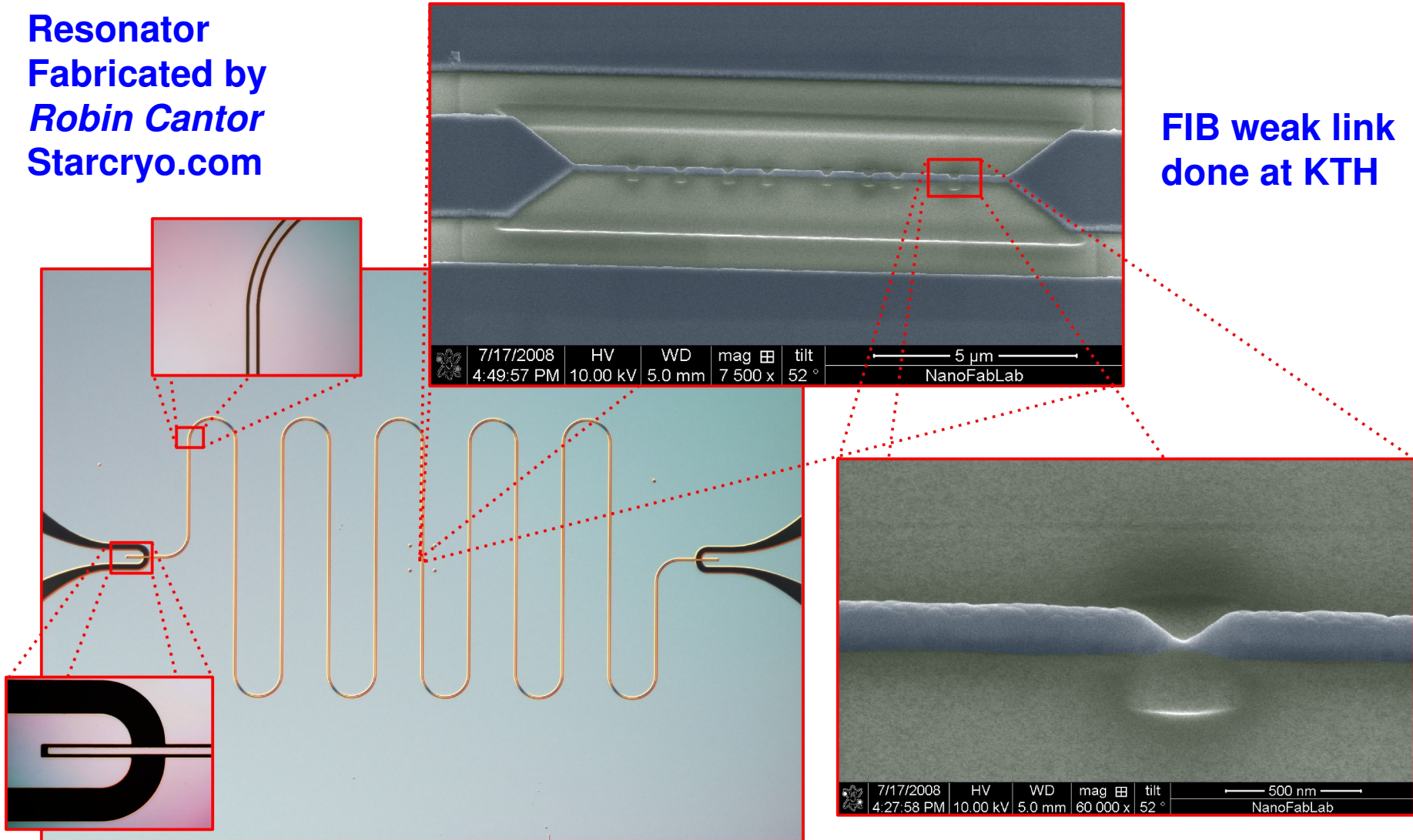


E. Tholen *et al.* unpublished

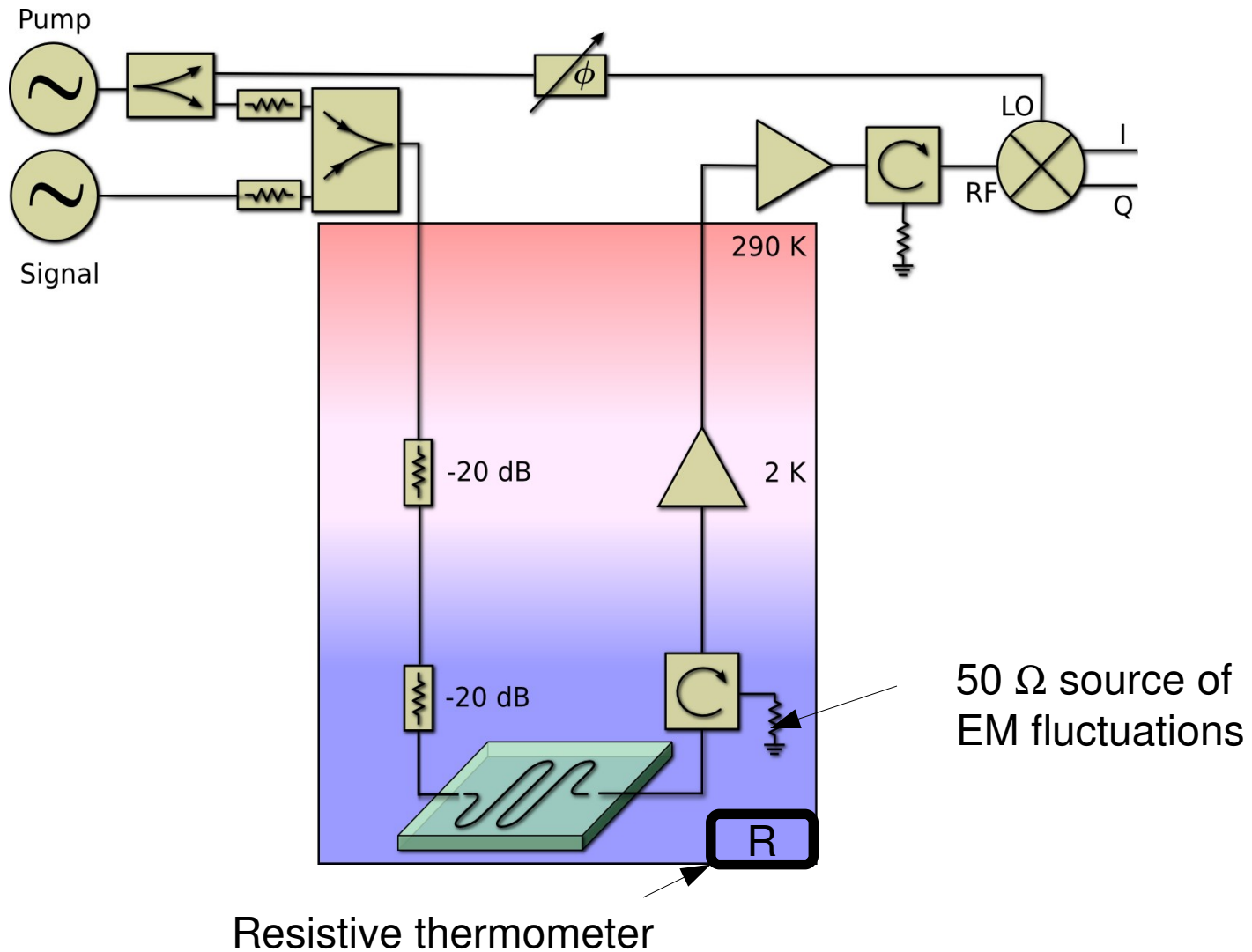
Weak link array resonator center

Resonator
Fabricated by
Robin Cantor
Starcryo.com

FIB weak link
done at KTH



Calibrating noise measurement



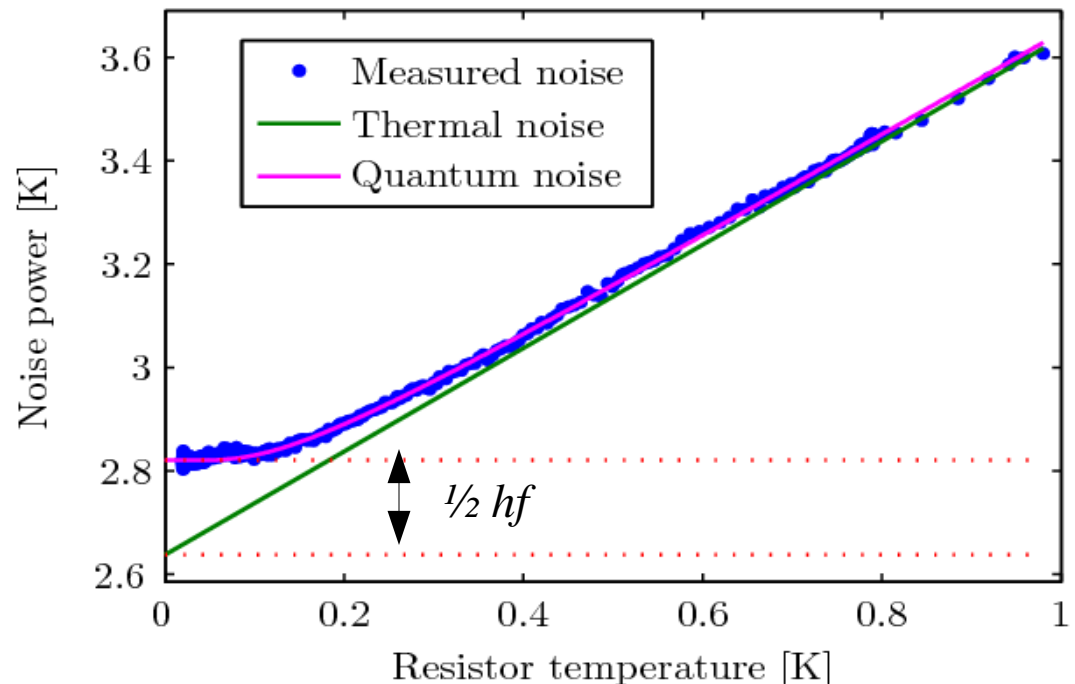
Calibrating noise measurement

$$\langle E \rangle = \hbar\omega \left(\frac{1}{2} + \langle n \rangle \right)$$

In thermal equilibrium photons are Bose-Einstein distributed, i.e.

$$\langle n \rangle = \frac{1}{e^{\frac{\hbar\omega}{kT}} - 1}$$

$$\langle E \rangle = \hbar\omega \left(\frac{1}{2} + \frac{1}{e^{\frac{\hbar\omega}{kT}} - 1} \right)$$



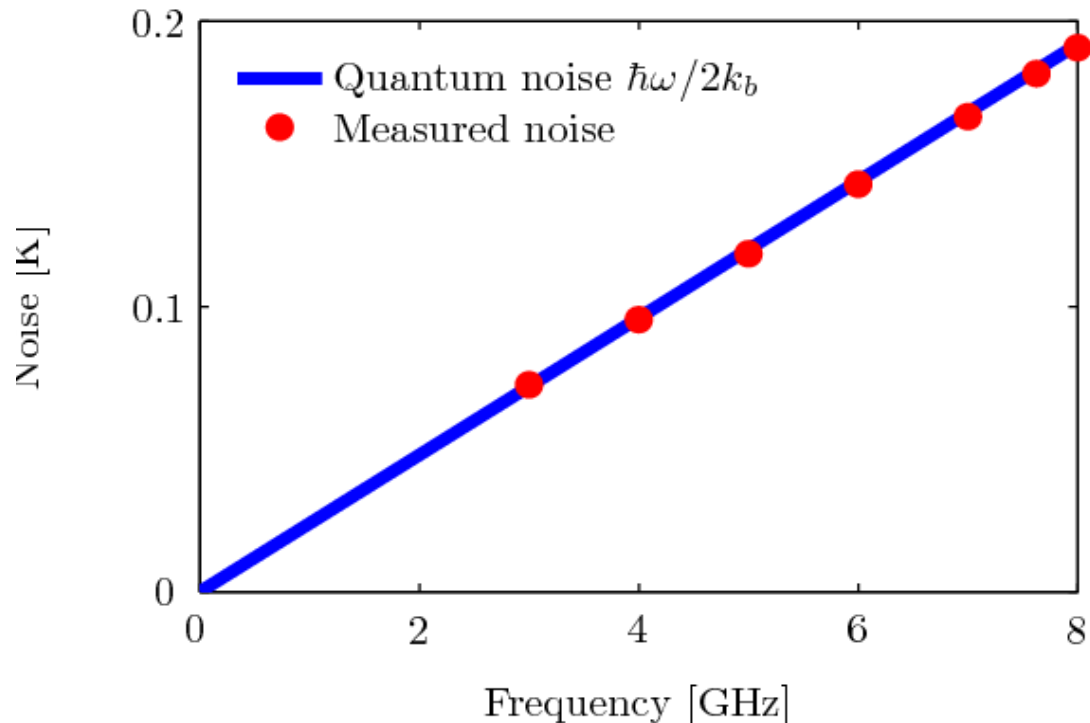
Measuring quantum noise

$$\langle E \rangle = \hbar\omega \left(\frac{1}{2} + \langle n \rangle \right)$$

In thermal equilibrium photons are Bose-Einstein distributed, i.e.

$$\langle n \rangle = \frac{1}{e^{\frac{\hbar\omega}{kT}} - 1}$$

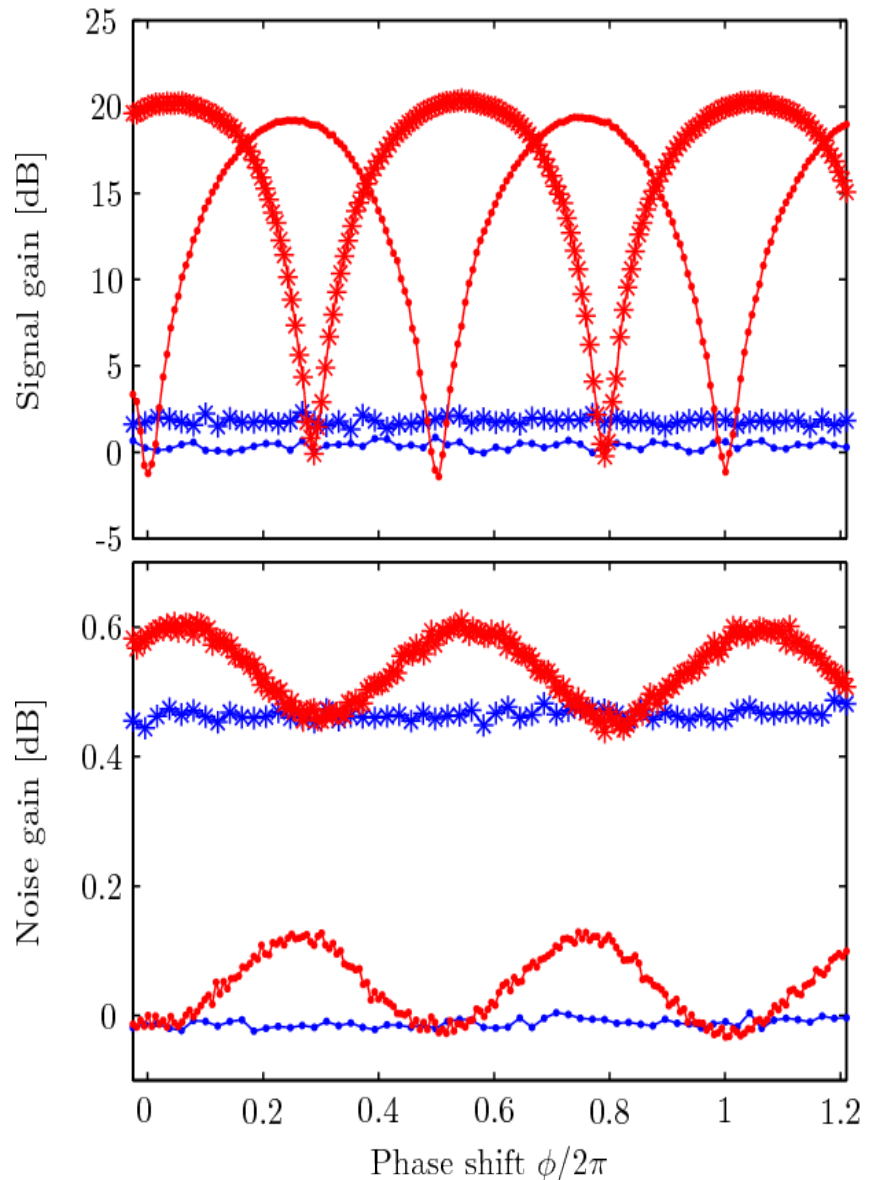
$$\langle E \rangle = \hbar\omega \left(\frac{1}{2} + \frac{1}{e^{\frac{\hbar\omega}{kT}} - 1} \right)$$



Attempting to squeeze quantum noise

Summary weak link PA

- Good Low Power Bifurcation
- Good signal gain
- Poor signal Squeezing
- No Quantum noise squeezing
- Is quantum noise squeezing possible with pair-breaking nonlinearity?



Observation of Zero-Point Noise Squeezing via a Josephson-Parametric Amplifier

R. Movshovich, B. Yurke, and P. G. Kaminsky

AT&T Bell Laboratories, Murray Hill, New Jersey 07974

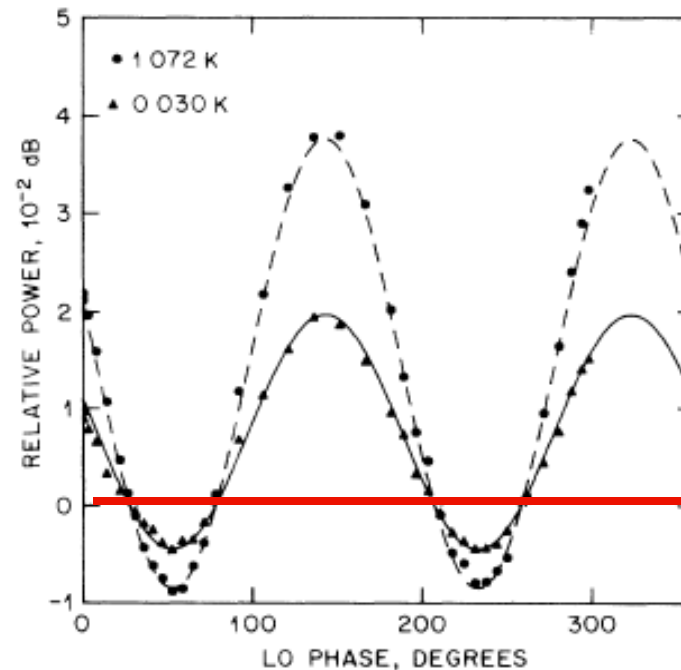
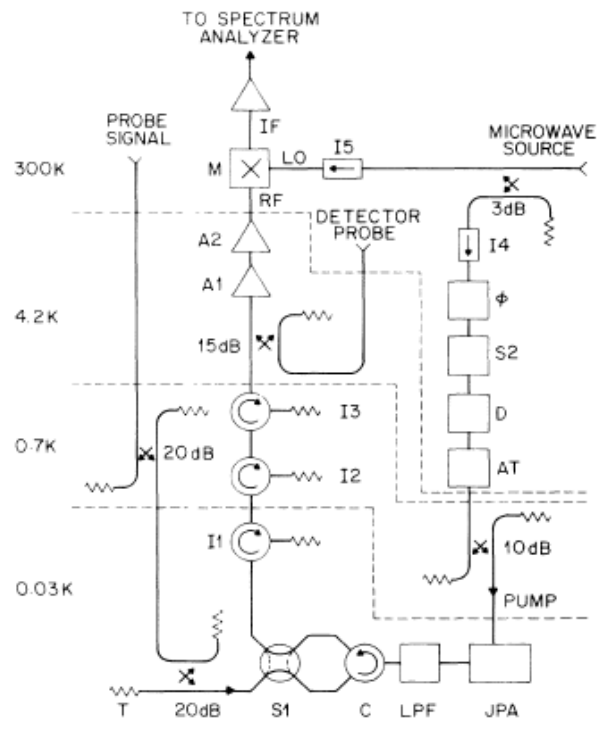
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(Received 7 June 1990)



Pump-off
level

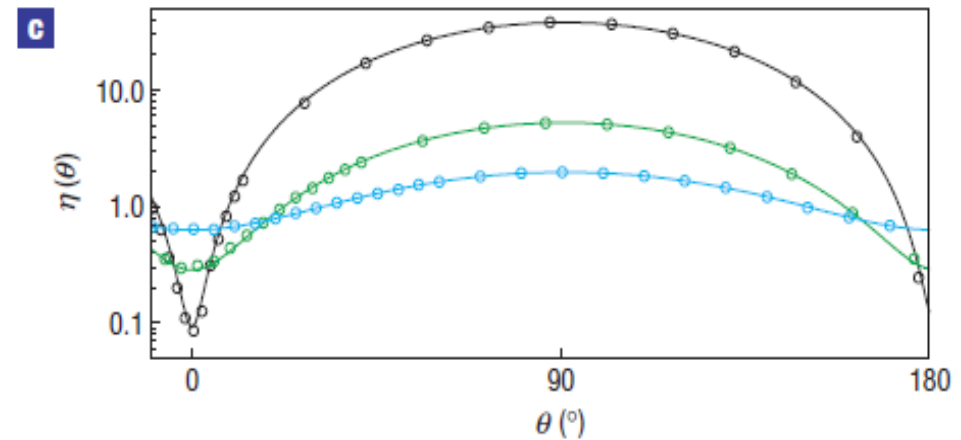
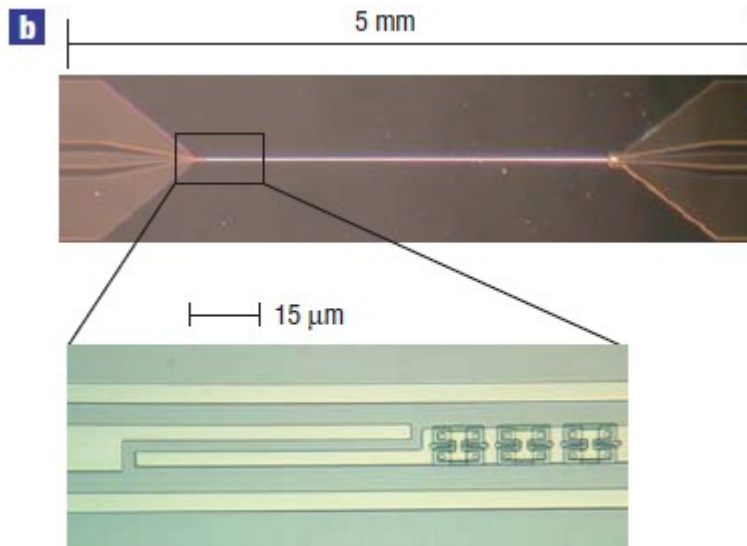
Amplification and squeezing of quantum noise with a tunable Josephson metamaterial

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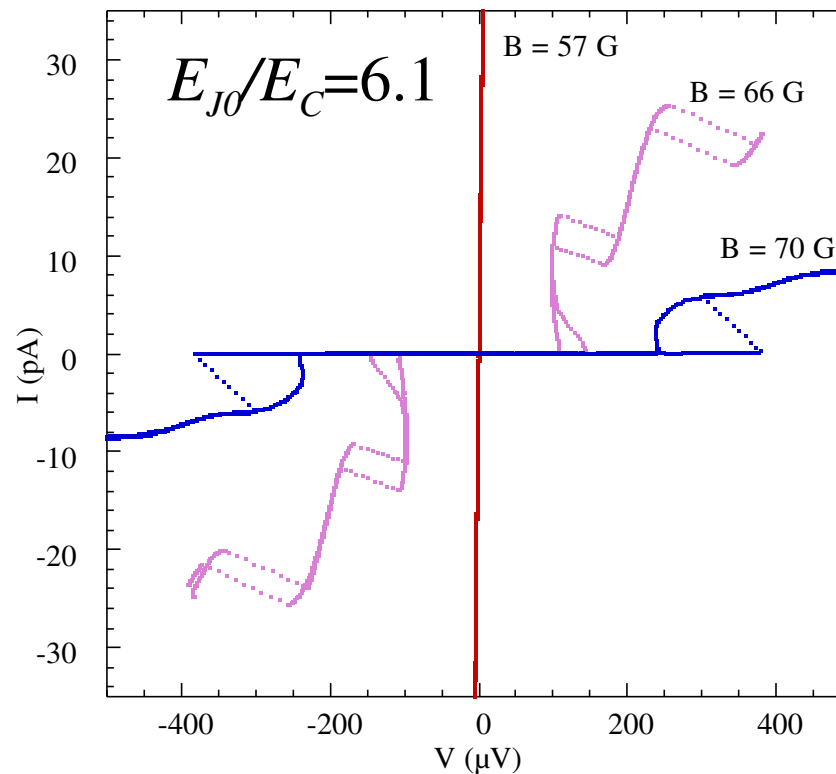
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Superconductor to Insulator Transition

- When $Z_A \gg R_Q = h/4e^2 = 6.45 \text{ k}\Omega$
- Phase charge duality

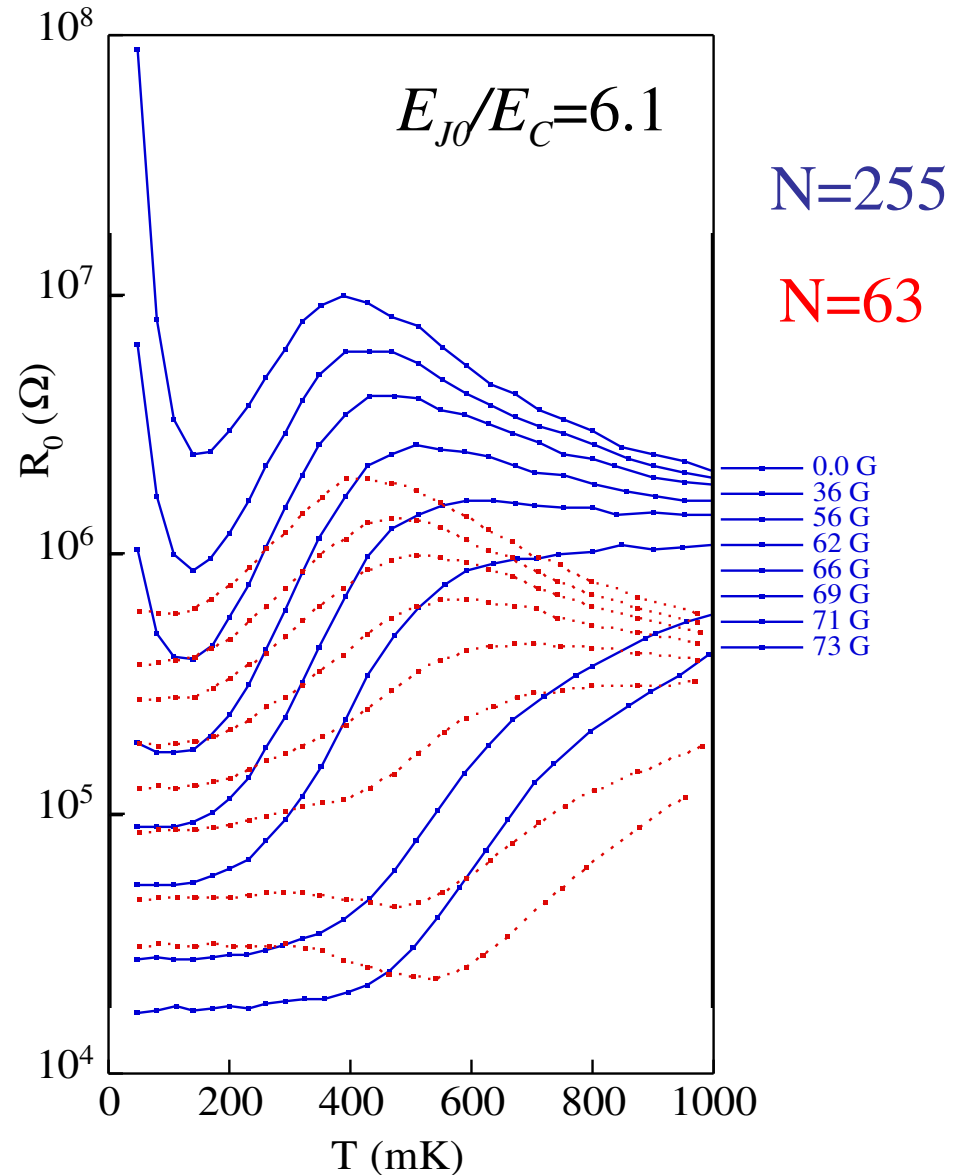
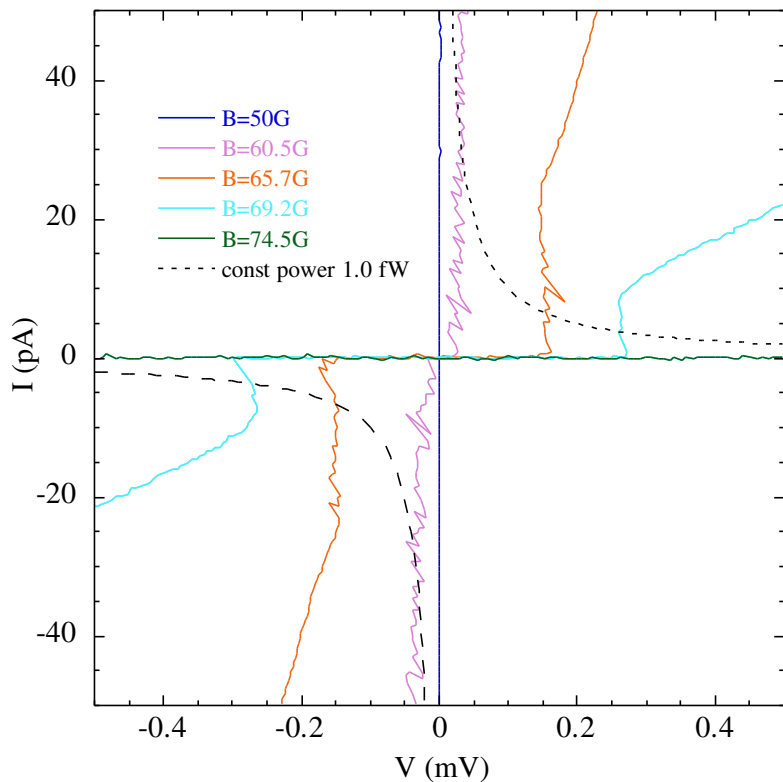


Quantum Phase Transition in 1D array

Quantum Phase Transition

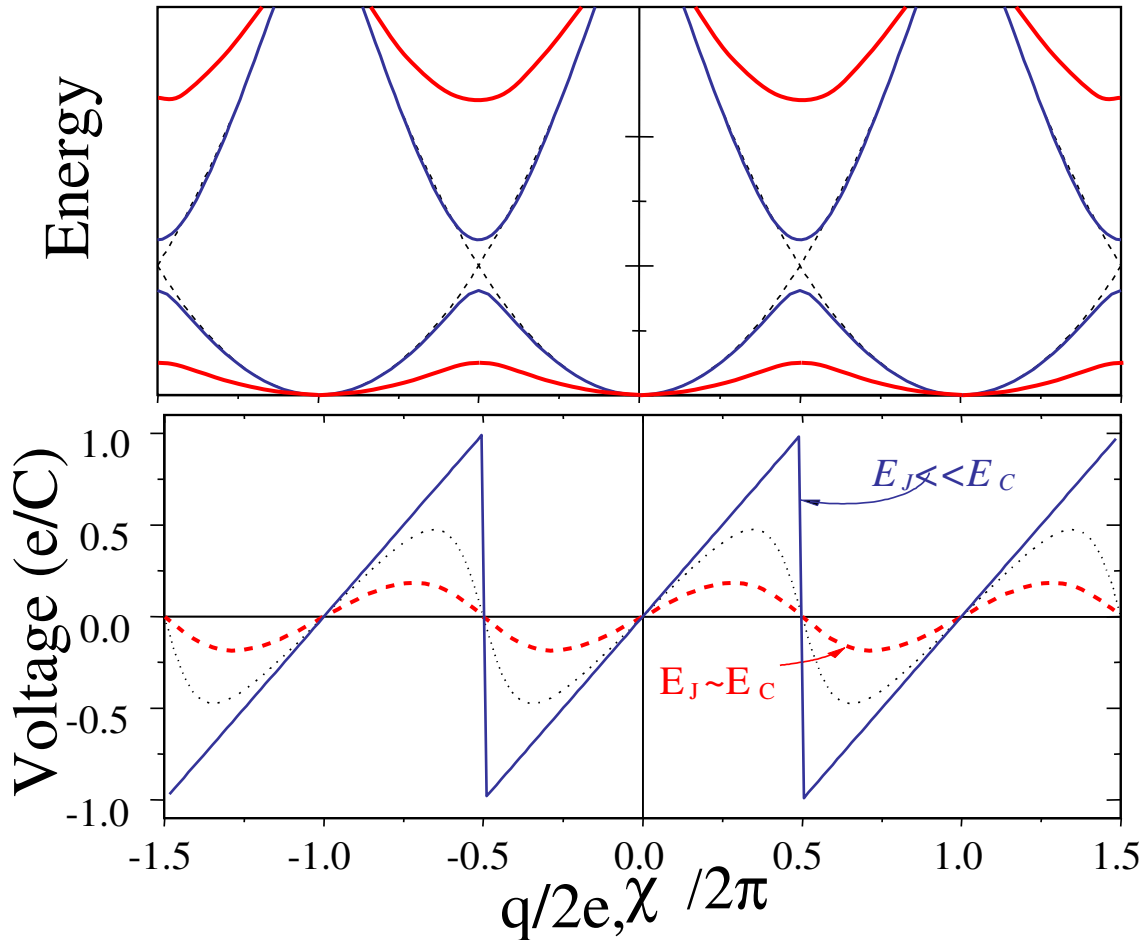
Tune E_J with Φ_{ext}

Superconductor \Rightarrow Insulator



Quasi Charge description of Josephson Junction

Averin, Likharev and Zorin 1984



$$H = \frac{Q^2}{2C} - E_J \cos\left(2\pi \frac{\Phi}{\Phi_0}\right)$$

$$V = \frac{dE_0}{dq} = V_C \text{saw } \chi$$

Critical Voltage: $V_C(E_J/E_C)$

dimensionless quasi-charge

$$\chi = \frac{2e}{2\pi} q$$

$$I = \frac{2e}{2\pi} \dot{\chi}$$

Voltage leads:
2x60 SQUID arrays
SQUID size:
 $2 \times (0.1 \times 0.3) \mu\text{ m}^2$



Current leads:
2x15 junctions arrays
Junction size:
 $(0.1 \times 0.1) \mu\text{ m}^2$



Single junction
 $(0.2 \times 0.1) \mu\text{ m}^2$



Temperature dependence of I-V curve

Solid lines Theory with:

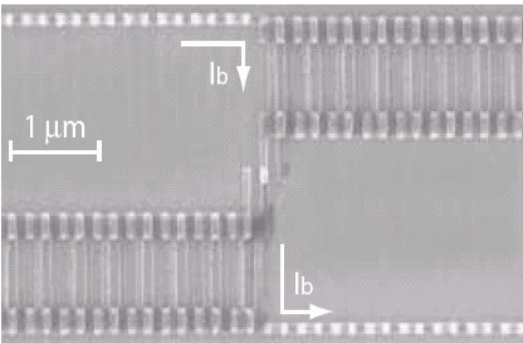
$$V_C (T=0) = 30 \mu\text{ V}$$

$$R_{\text{fit}} = 150 \text{ k}\Omega$$

$$T_{\text{meas}} = 50 \text{ mK}$$
$$T_{\text{fit}} = 160 \text{ mK}$$

$$T_{\text{meas}} = 250 \text{ mK}$$
$$T_{\text{fit}} = 260 \text{ mK}$$

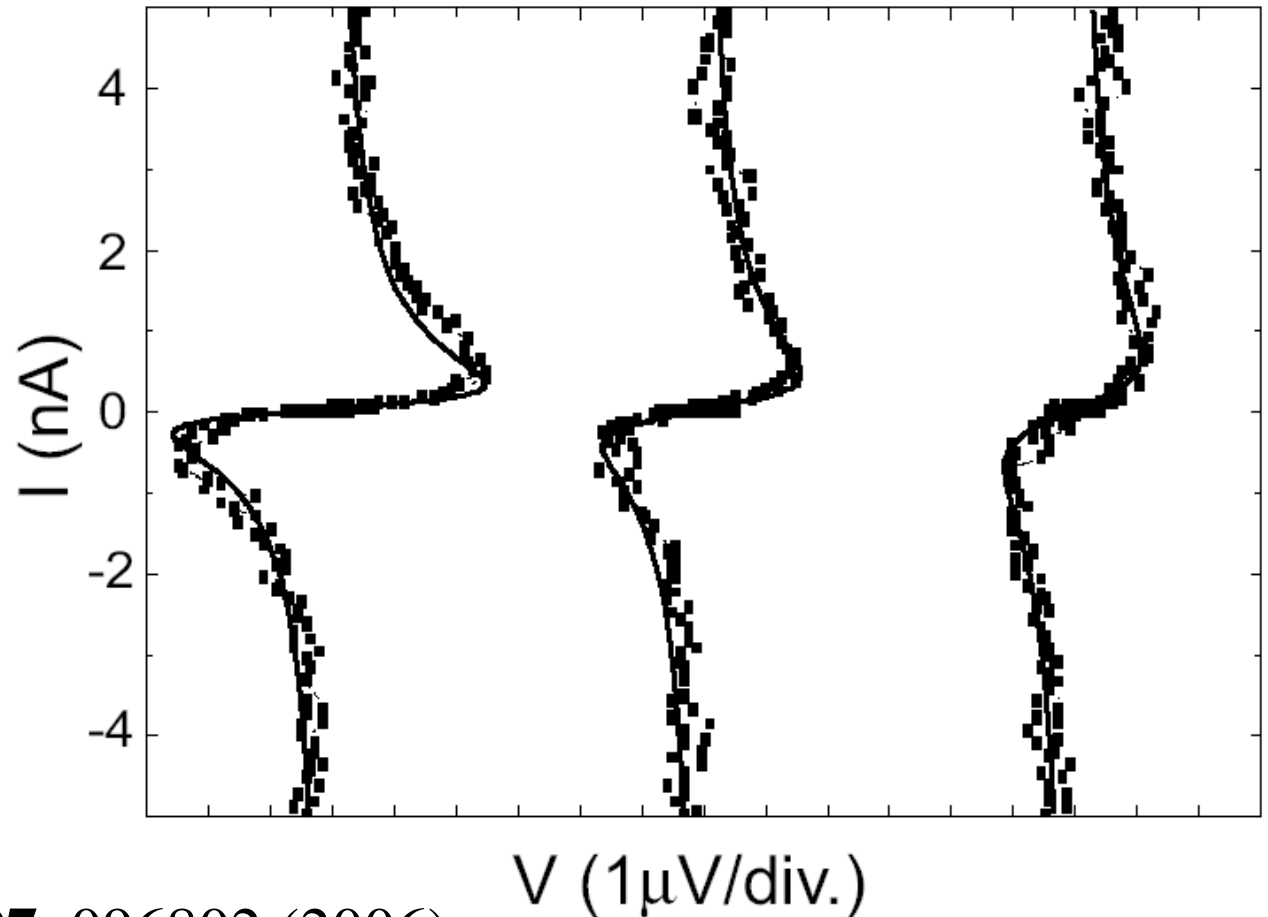
$$T_{\text{meas}} = 300 \text{ mK}$$
$$T_{\text{fit}} = 400 \text{ mK}$$



$$E_J/E_C \sim 3$$

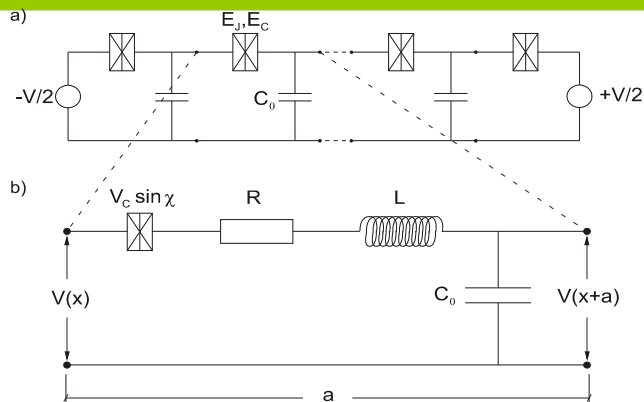
$$C \sim 0.9 \text{ fF}$$

$$R_N \sim 2 \text{ k}\Omega$$



1D Series Array: Quasicharge Dynamics

Peter Ågren, Ph.D Thesis, KTH, 2001



Phase

Quasicharge

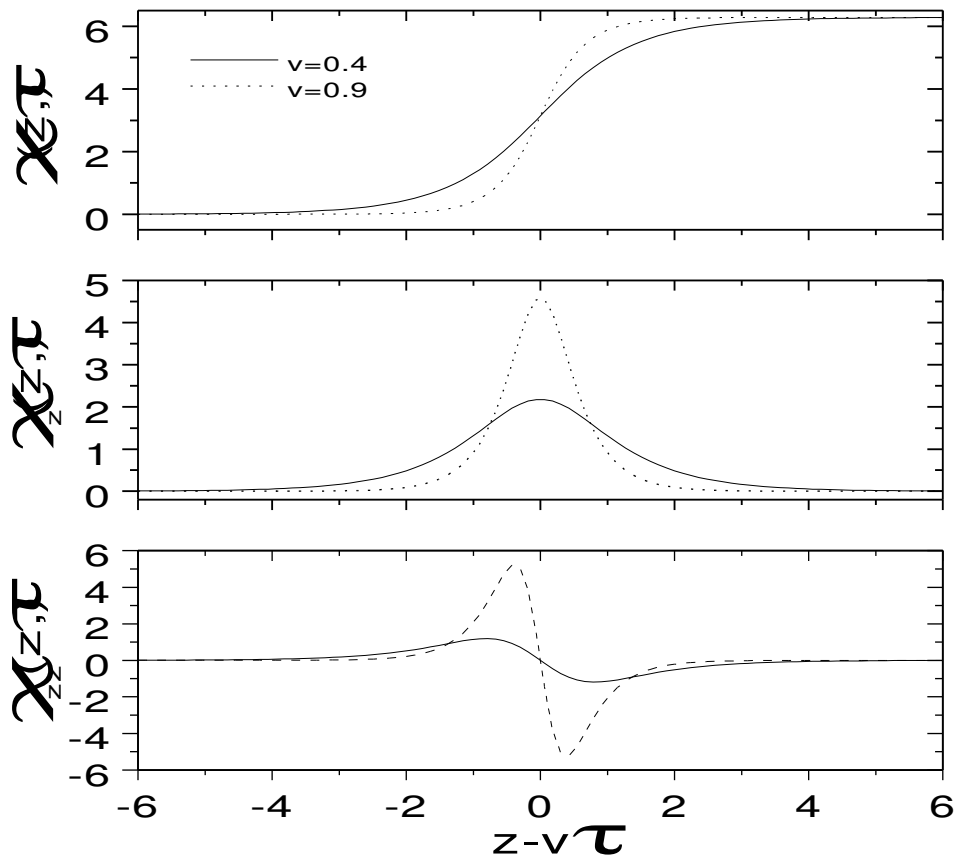
Magnetic Flux

Potential

Super Current

Electric field

$$\partial_{xx}\chi - \frac{1}{v_0^2}\partial_{tt}\chi - \frac{1}{\lambda_s^2}\text{saw}\chi = rc_0\partial_t\chi$$



Conclusions

- Classical, linear Electrodynamics
 - microwave photonic band gap
 - impedance matching possible for stripline geometry
- Classical nonlinear Electrodyamics
 - parametric amplifier
 - Noise squeezing, vacuum squeezing
- Quantum limit
 - Coulomb blockade of Cooper pairs
 - Charge solitons – duality to fluxon

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Carsten Hutter

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New EU project: SCOPE Single Cooper Pair Electronics

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