

THE UNIVERSITY OF MINNESOTA

GRADUATE SCHOOL

Report  
of  
Committee on Thesis

The undersigned, acting as a Committee of the Graduate School, have read the accompanying thesis submitted by Elmer John Forsberg for the degree of Mechanical Engineer. They approve it as a thesis meeting the requirements of the Graduate School of the University of Minnesota, and recommend that it be accepted in partial fulfillment of the requirements for the degree of Mechanical Engineer.

John J. Dather  
Chairman  
Frank B. Rowley  
E. L. Travis

Date June 24, 1922

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The undersigned, acting as a Committee of the Graduate School, have read the accompanying thesis submitted by Clarence Jewett Eddy for the degree of Mechanical Engineer. They approve it as a thesis meeting the requirements of the Graduate School of the University of Minnesota, and recommend that it be accepted in partial fulfillment of the requirements for the degree of Mechanical Engineer.

John J. Flather  
Chairman  
Frank B. Rowley  
E. L. Tuve

Date June 24, 1922

The Effect of the Length of Pipe  
on the Distribution of Air in the  
Test of Fans and Blowers

A Thesis

Submitted to the Faculty of the  
Graduate School

of the

University of Minnesota

by

Clarence John Eddy

Elmer John Forsberg

in Partial Fulfillment of the  
Requirements for the degree of

Mechanical Engineer

June

1922

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AUG 3 '35  
L.S. W. J. W.

### ACKNOWLEDGEMENT

We take pleasure in acknowledging Professor J. J. Flather for the assistance and helpful criticisms given in the thesis.

We also wish to thank Professor F. B. Rowley and Mr. G. L. Tuve for their helpful advice, also, the Assistants in the laboratory for their assistance in setting up the apparatus and for the use of the equipment.

## INTRODUCTION

The effect of the length of pipe on the distribution of air in the test of blowers.

This thesis work, of which Professor J.J. Flather was the advisor, was undertaken by Mr. C.J. Eddy and Mr. E.J. Forsberg to determine the effect of the length used with the distribution of air in that pipe and to devise some method by which the distribution would be equalized. Mr. G. Tuve performed some tests during the summer months of 1921 on the same blower without using the equalizers. Our tests were conducted on the balcony of the Experimental Engineering Building while Mr. Tuve's were conducted in the power plant of the Electrical Engineering Building. Mr. Tuve's tests were conducted using various openings and different sized pulleys on the blower as were ours, but were not carried out with the purpose of equalizing the distribution of the air in the pipe; special attention being paid to the efficiency of the fan and the design of blades and aprons for the blower.

In order to get the most possible out of this work it was thought necessary to spend considerable time looking up information which would have a direct bearing on the work. This information was secured from the libraries of the University and City from books, magazines, journals, and bulletins. Considerable time was spent on material concerning the use of the pitot tube which was very necessary since the largest part of this work consisted of pitot tube readings. After a method of procedure was decided upon and a number of preliminary tests had been run, however, an article was published in the Journal of the American Society of Heating and Ventilating Engineers entitled "Methods of Measuring Fan Delivery" by E.N. Fales, of Dayton, Ohio who was an aeronautical engineer at McCook Field; the tests being run under the war department air service. The fans used in these tests, however, were what was called a Simmons 4 blade fan and was not a rotary fan such as the type used in the research work which is included in this cover.

## OBJECT

The object of this research was pointed out in the introduction. In order to accomplish this work a definite procedure was decided upon and carried out. As has been stated Mr. Tuve carried out a number of experiments along the same line paying more particular attention to the design of blades and aprons for the blower itself. His results were available for us to use but were of little or no value to us as a source of comparison since the tests Mr. Tuve ran were run on the apparatus when it was set up in the forge shop and the Electrical Building with which a different motor was used and also different ammeters and voltmeters. The differential gages used were the same in both cases as was also the special A B C pitot tube.



APPARATUS

Centrifugal Air Fan manufactured by the ~~Hacking~~<sup>ney</sup> manufacturing Company of St. Paul.

Direct Current motor No. 33977 (Northern)

Form C Amperes 19 Speed 1150

Volts 230 H.P. 5

Fort Wayne Electric Works of the General Electric Company Fort Wayne, Indiana.

Rheostat no. 114024 starting service.

H.P. 20 Volts 230

General Electric Company U.S.A.

Rheostat no. 43633 Field Service.

Ohms 75 Amperes 2-4 volts 250

General Electric Company U.S.A.

Field Rheostat

Two Ellison Differential Draft Gages 0-1.5" Pressure.

One Ellison Differential Draft Gage 0-1.0" pressure.

Two pulleys 15" and 24" in diameter for use on the blower.

Pipe 23' - 8" long and 34 inches in diameter with a rectangular fan outlet attachment 2'-1 $\frac{1}{2}$ " by 2'-8 $\frac{3}{4}$ " and 2'-2'-3" long.

Milli-voltmeter No. 3299

Shunt 25 Ampere

Voltmeter No. 3381

Tubing for draft gages as shown on the photograph.

Fan outlet openings of approximately 1/2, 5/8, 3/4, and 7/8 of the total area of the opening.

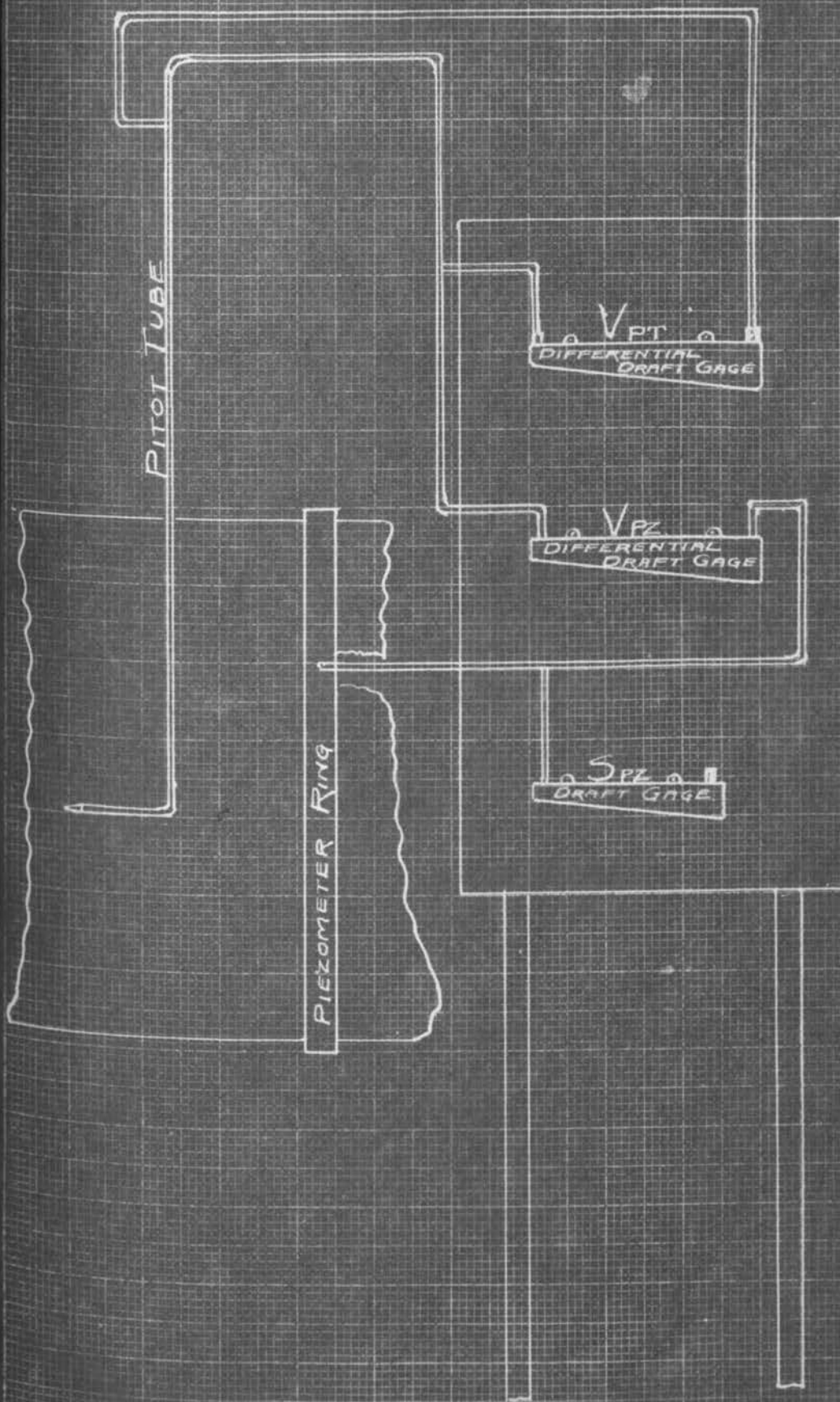
Attachments for pitot tubes with marked distances on them showing the distance that the pitot tube has been inserted in the pipe.

Revolution counter and stop watch.

Two equalizers as shown in photograph.

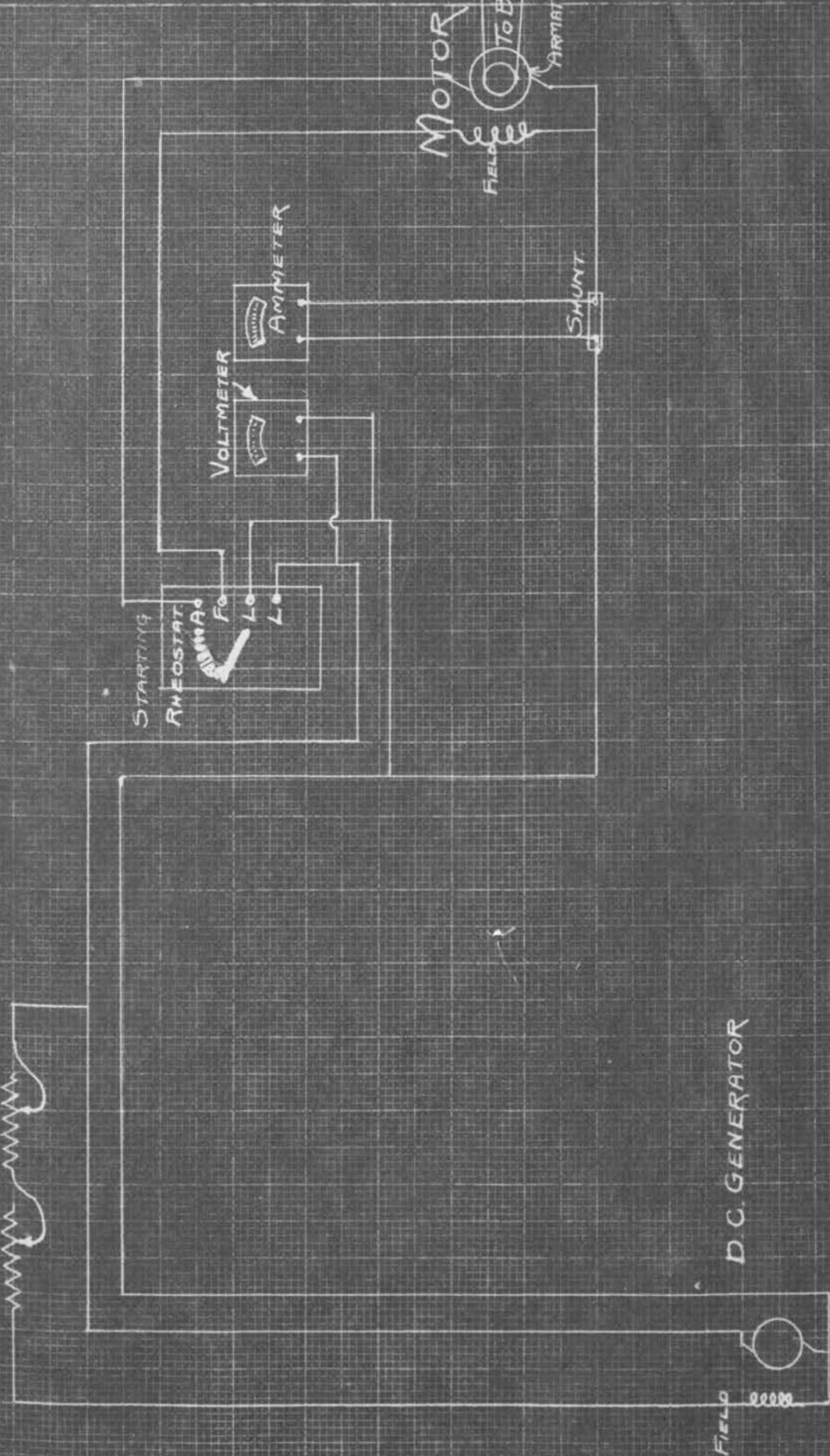
Pitot tube arrangement with draft gages and pipe layout, with wiring diagrams as shown in blue prints.

# ARRANGEMENT OF PITOT TUBE AND DRAFT GAGES.



# WIRING DIAGRAM

FIELD RESISTANCES



D.C. GENERATOR

FIELD

MOTOR

BELT  
TO BLOWER

ARMATURE

FIELD

SHUNT

VOLTMETER

AMMETER

STARTING

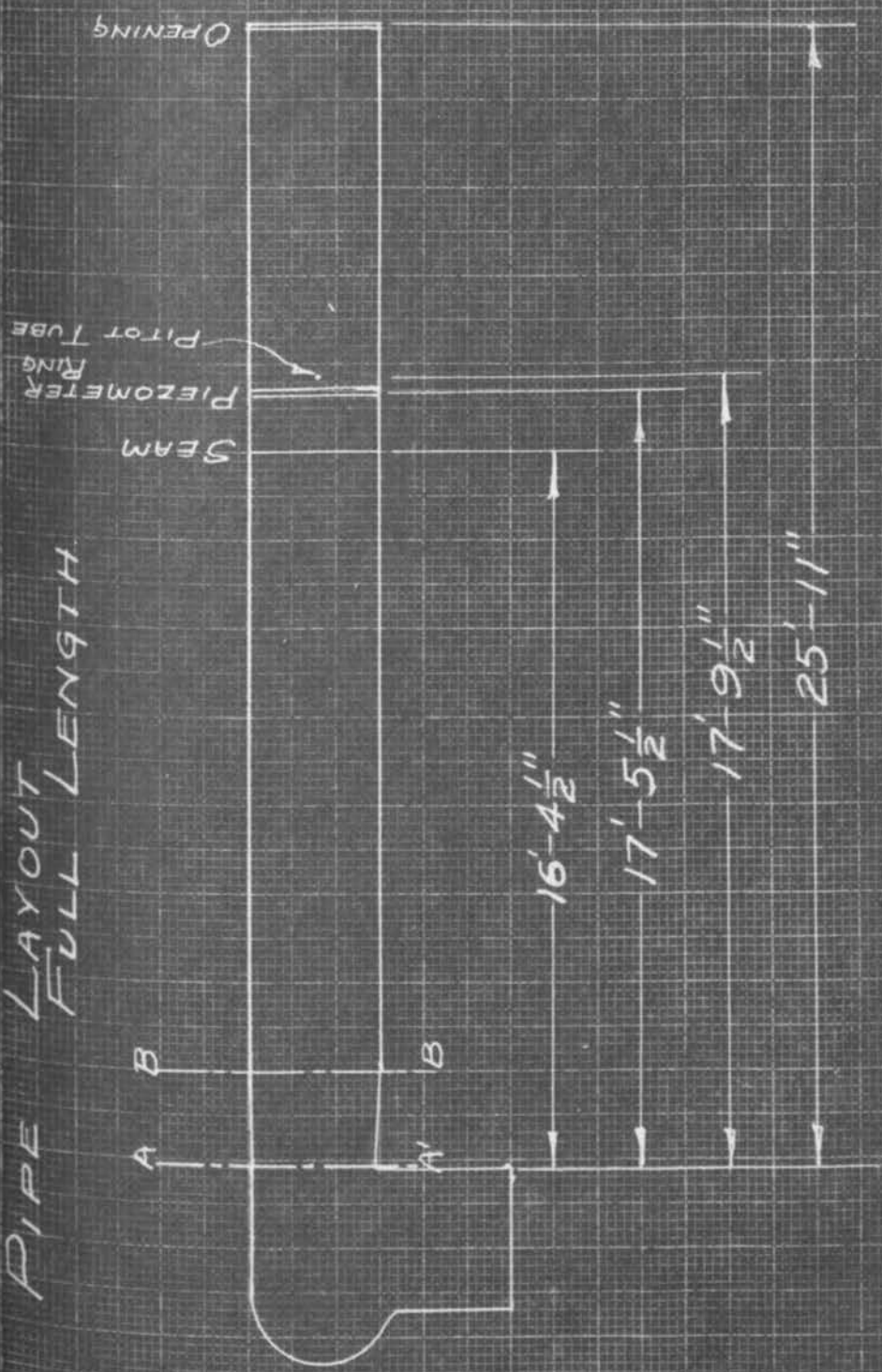
RHEOSTAT

Fo

Lo

Lo

PIPE LAYOUT FULL LENGTH



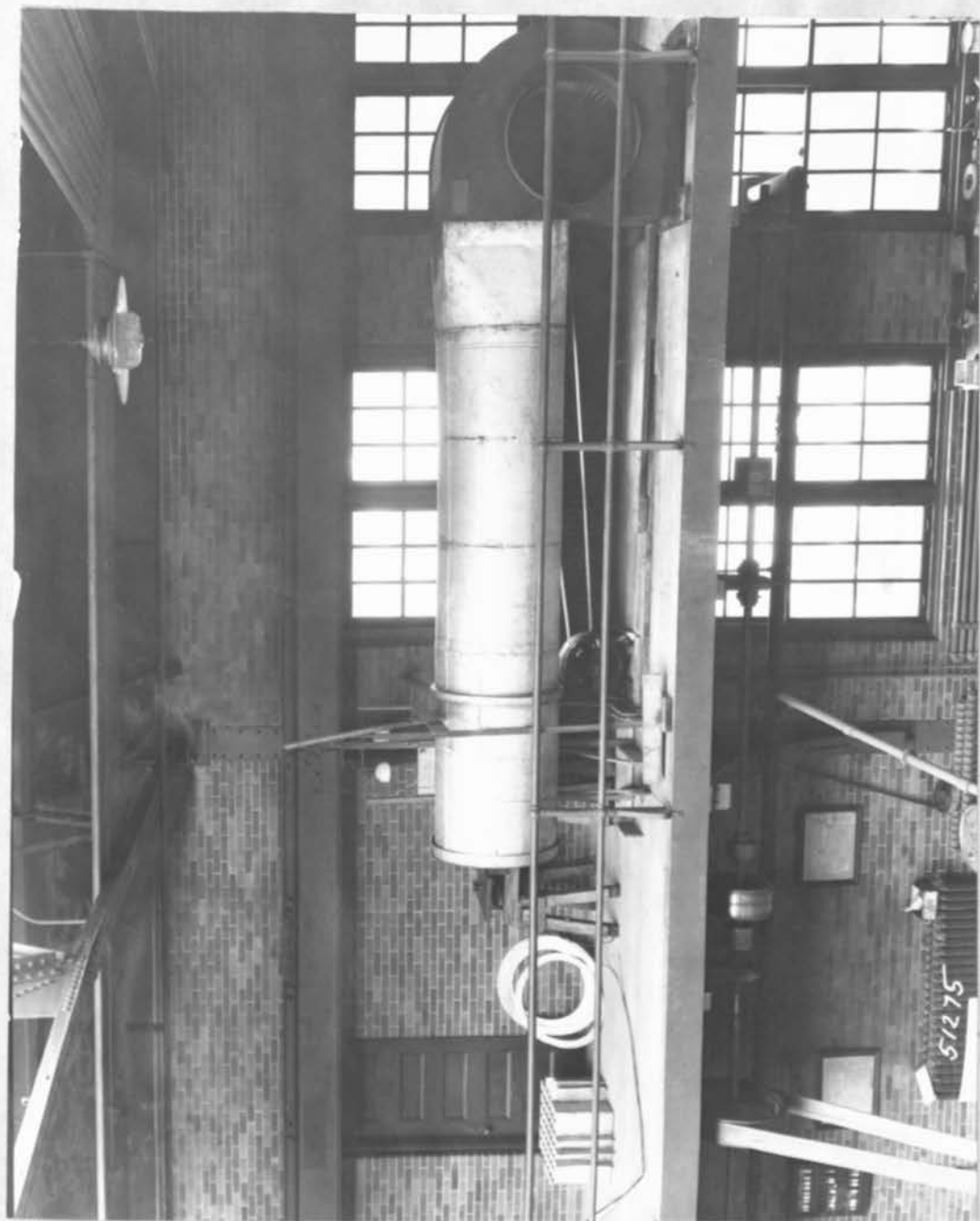
SECTION BB



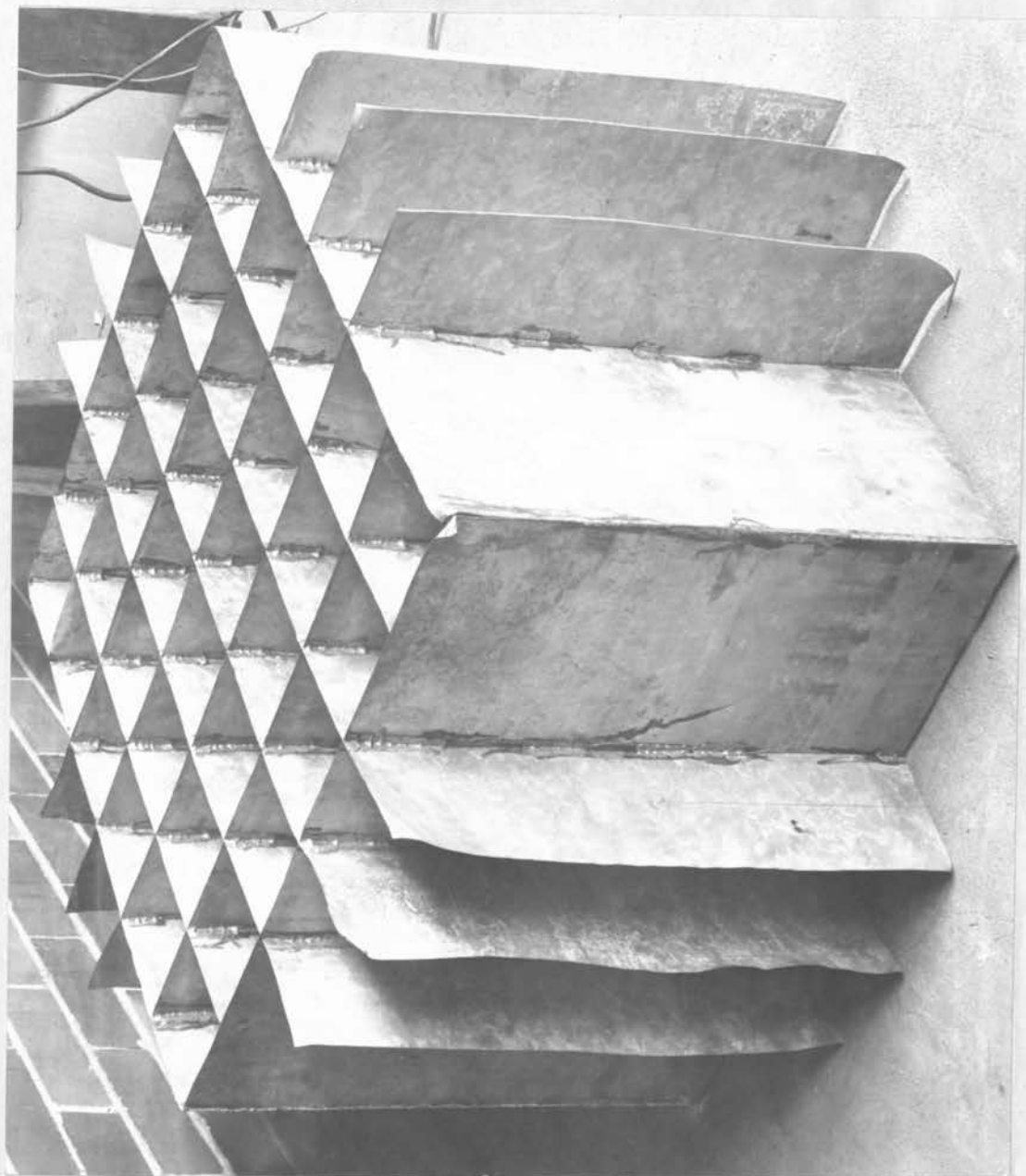
SECTION AA



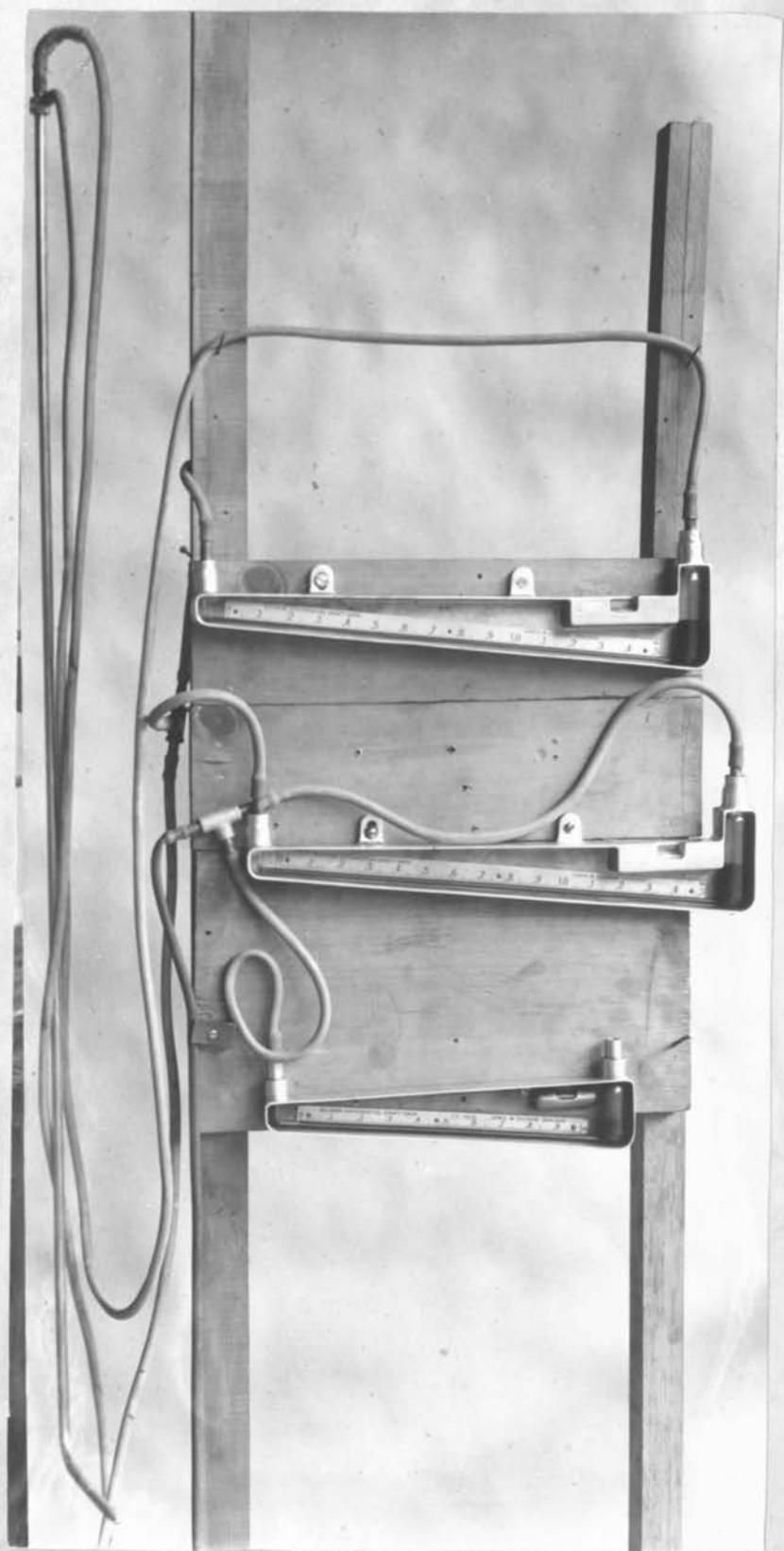




EQUALIZER.









## GENERAL DESCRIPTION OF TESTS CONDUCTED

The length of pipe necessary for an even distribution of air in that pipe varies from 10 to 40 diameters. By an ~~an~~ even distribution of air is meant a distribution so arranged that the maximum velocity is at the center of the pipe and it gradually decreases toward the outside of the pipe. Different authorities give different values for the distance required for this even distribution. In the discussion # by Mr. Taylor <sup>it is</sup> ~~he~~ states that 10 diameters are required for an even distribution. In his work, Mr. Taylor used some small brass tubes  $5/8$ " (1.58cm),  $7/8$ " (2.22cm), and  $1\frac{1}{2}$ " (3.81)cm in diameter. The velocity distribution became constant at a distance of about 200 cm. using these tubes. Using the 3.81 cm tube as a basis of reference a length of tube of approximately 50 diameters would be required in this case. The maximum velocity at the center increased with increasing distance from the fan outlet. This can plainly be seen from the curves which were given for distances of 78.6, 154.5 and 230.7 cm from the fan outlet.

# The Flow of Air Through Small Brass Tubes

T.S. Taylor A.S.M.E. 1920 P. 121

The length of pipe used was 243.6 cm. The velocity at the walls of the tubes dropped off very rapidly and could not be observed. The ratio of the average velocity to the maximum velocity at the distances given above was .82 to .85. This ratio was decreased by the presence of dirt or other material. The coefficient of friction is higher for the low velocities. In an article # published by J.E. Emswiller <sup>It is</sup> ~~he~~ states that the velocity at the center is ahead at 40 diameters.

An article # published in the Heating and Ventilating Magazine states that the pitot tube should be placed from 10 to 20 diameters from the fan outlet and the center reading should be multiplied by .8 to get the average velocity. This is about the same constant above referred to using a length of from 10 to 20 diameters.

As stated in Mr. Taylors article an even distribution is obtained by using the 50 diameter pipe. In our work if we used a 40 diameter pipe to give an even distribution it would require a 1360" pipe or 113.3'

#A.S. H. & V. E. Vol. 22 P. 537 J.E. Emswiller

# Heating and ventilating Magazine Feb. 1919 Vol. 16.

This length of pipe would be very expensive and cumbersome to handle. Our problem, then, was to devise some method by which an even distribution could be obtained using a shorter length of pipe. The method which was decided upon and finally used was that of using a honeycombed arrangement which was made of 24 gage sheet metal (as shown in the photographs) to break and distribute the air in the pipe. The honey combed arrangement consisted of 4" squares with a length of 18". There were approximately six of these squares to a side making a 24" square with a diameter of 34". The three center pieces had projecting ends on them.

The pitot tube is the most reliable and accurate instrument for the measurement of the velocity of the air in the pipe. This method is more reliable and accurate than the anemometer method. The anemometer may show an inaccuracy of 10% due to dryness of the bearings. If an anemometer were used it would have to be frequently calibrated. There is no inaccuracy due to the tips of the pitot tube.

Readings were taken of the velocity of the air in the pitot tube using the static in the pitot tube, velocity of air in the pitot tube using the piezometer ring as static, and the static of the piezometer ring. If only one side of the two upper draft gages were used and only the straight connection of the pitot tube the draft gages would record the total pressure. Since the other side of the two upper draft gages were attached to the static of the piezometer ring and pitot tube the differential gages read the velocity of the piezometer and pitot tube. The lower draft gage had only one connection so that it read only the static of the piezometer ring. This piezometer ring encircles the blower pipe, which has holes inserted in it, so that the static air flowing from the pipe into this piezometer ring is recorded by the draft gage. Twenty readings were taken for each opening. Ten readings were taken across one section of the pipe and ten at right angles to these readings. The openings we used in running these tests were approximately  $\frac{1}{2}$  5/8,  $\frac{3}{4}$  and 7/8.

Readings were taken at equal areas in the pipe. A very simple method # of obtaining the diameters of these areas is by dividing the diameter of the pipe by the square root of twice the number of readings from the center to the outside of the pipe and multiplying by the square root of three, five, etc. for the second, third, etc. readings. Since our pipe was 34" in diameter the first diameter would be 34 divided by the square root of two times five or 10.76". The second diameter would be 10.76 times the square root of three or 18.6".

The blower speed, motor voltage, and amperage were also recorded. The static pressure of the pitot tube may be obtained by adding the static and velocity pressures of the piezometer ring and subtracting the velocity of the pitot tube. In reducing to standard conditions the static pressure varies as the R.P.M. squared. The velocity pressure varies directly as the R.P.M. The horse power at the fan pulley varies as the R.P.M. cubed.

Friction in inches  $\frac{\text{Velocity}^2 \text{ times length in feet}}{40 \text{ times diameter in feet}}$

# Measurement of Air in Fan Work C.H. Treat A.S.M.E.

P. 1019 Vol. 34 1912

The pressure on the pitot tube equals  $\frac{Wv^2}{2g}$  where W is the weight of a cubic foot of air, v is the velocity in feet per second, and g is the acceleration of gravity equals 32.174. One cubic foot of water weighs 62.37 pounds. If i is the manometer reading in inches

$$\frac{Wv^2}{2g} = \frac{i \text{ times } 62.37}{12}$$

$$v^2 = \frac{2i \text{ times } 32.174 \text{ times } 62.37}{12 W}$$

$$v = 18.29 \sqrt{\frac{i}{W}} \text{ Feet per second}$$

$$v = 60 \text{ Times } 18.29 \sqrt{\frac{i}{W}} \text{ Feet per minute}$$

W, the weight of air, depends upon the pressure, temperature, and moisture content.

A graphical method # of obtaining the mean velocity across any section in the pipe is included in this thesis

Since Mr. Ruvé's tests were run under different conditions as above outlined it was deemed wise after a consultation with Professor Flather to run some tests using the full length of pipe with no equalizer as a



basis of reference. This was done using four different openings of approximately  $\frac{1}{2}$ ,  $\frac{5}{8}$ ,  $\frac{3}{4}$ , and  $\frac{7}{8}$  all at the same fan speed.

After this first series of tests <sup>was</sup> ~~were~~ made considerable time was spent waiting for the first equalizer which finally came and the second series of tests run were with the full length of pipe and with the equalizer placed 5' 1" from the fan opening.

The next test conducted was with the long length of pipe and with one equalizer placed 7' 1" from the fan opening. These tests were all made with the original length of pipe of 25' 11" and since the investigation being carried on is to find out the effect of the length of pipe on airflow it was next decided to shorten the length of pipe to a 14'  $2\frac{1}{2}$ " length or about five times the diameter of the pipe.

This was done and a series of tests made; the first being a test with no equalizers in the pipe which could be used as a basic test or for something to refer to.

The next test run was with the short length of pipe with one equalizer placed 5' 1" from the mouth of the fan.

The results from these tests not thought to satisfy the requirements and after another consultation with Professor Flather it was decided that another equalizer would be made and the series of tests with two equalizers run. An order was made for another equalizer but due to financial stringencies of the firm who was to furnish the equipment a lengthy delay occurred which slowed up the progress of the investigation, but meanwhile the apparatus was changed back from the short length of pipe to the long length, and a series of tests run with a smaller diameter of pulley on the blower which changed the speed considerably.

The first test run with the higher speed, as before were basic tests with no equalizers. By this time the second equalizer had been completed so that the next test that was run was a test with two equalizers placed 5' 1" and 13' 2" from the mouth of the blower.

Another set of tests <sup>was</sup> ~~were~~ run partly for the purpose of checking former results. This set of tests was run with a short length of pipe. Four tests being made with no equalizer, four with equalizers spaced 2' 3" from fan opening, four with equalizers spaced 6' 7" from fan opening and final four tests being run with two equalizers the first being spaced 2' 3" from fan opening, the second 6' 7" from fan opening. All four openings were used in these tests and both top and side readings were taken and plotted on graphs. A set of readings was taken with the equalizer blades placed parallel to the fan blades, at an angle of 19 degrees, and at an angle of 45 degrees. The results of these tests were also plotted. In running the set of tests with the two equalizers the blades of the equalizer nearest the fan opening were placed at an angle of 45 degrees while the blades of the second equalizer were left parallel to the fan blades. This was done to get the maximum effect of the distribution of air. This was also done with the set using one equalizer at 45 degrees.



DATA SHEET FOR MOTOR CALIBRATION

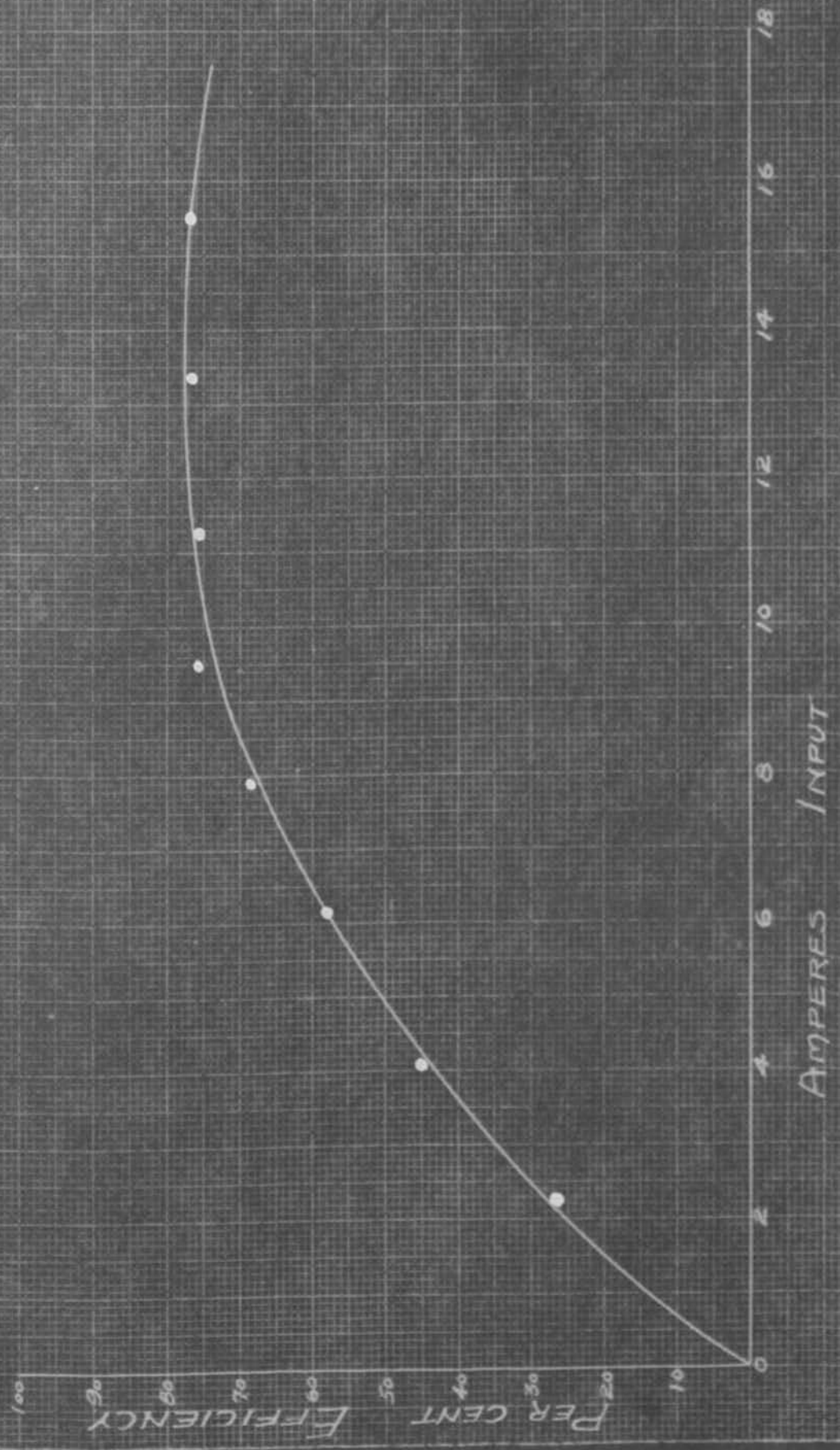
Average Tare Weight 8.86 lbs.

	R.P.M.	Net Wt. lbs.	Volts Obs.	volts Cor.	Amps. Obs.	Amps. Cor.
1	1090	1.00	228	230.55	4.03	4.125
2	1085	2.00	229	231.35	6.00	6.072
3	1095	3.00	230	232.20	7.75	7.92
4	1078	4.00	231	233.15	9.42	9.50
5	1058	5.00	228	230.55	11.17	11.28
6	1060	6.00	229	231.35	13.17	13.345
7	1060	7.00	230	232.20	15.32	15.412

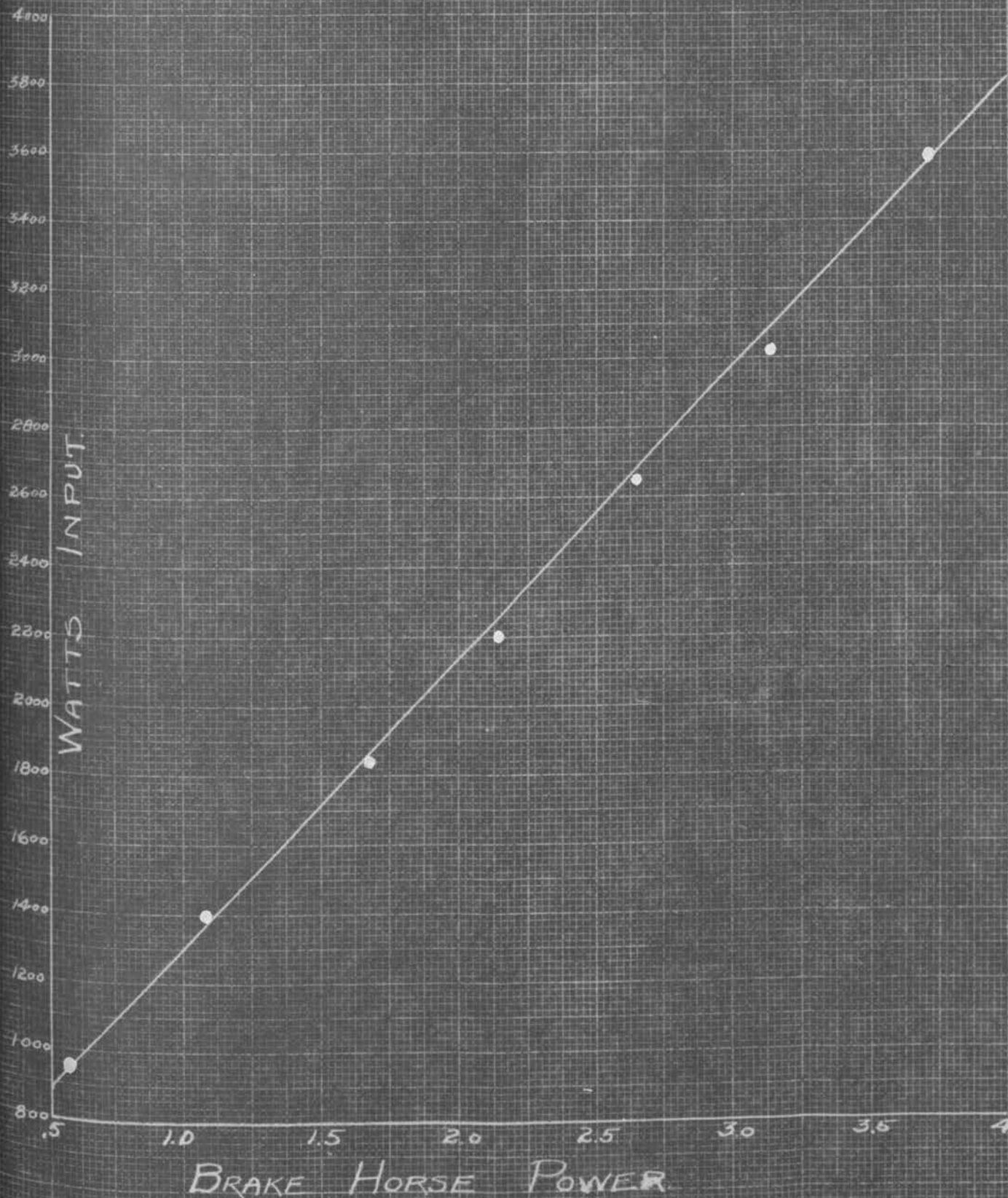
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	Watts	E.H.P.	W.N.	B.H.P.	Eff.
1	950	1.276	1090	.545	42.7
2	1400	1.878	2170	1.085	57.8
3	1840	2.47	3285	1.642	66.30
4	2210	2.97	4312	2.156	75.8
5	2650	3.48	5290	2.645	76.0
6	3080	4.13	6360	3.180	77.0
7	3580	4.80	7420	3.710	77.3

# CALIBRATION CURVE OF FAX MOTOR



# CALIBRATION OF FAN MOTOR



### Calibration of Instruments

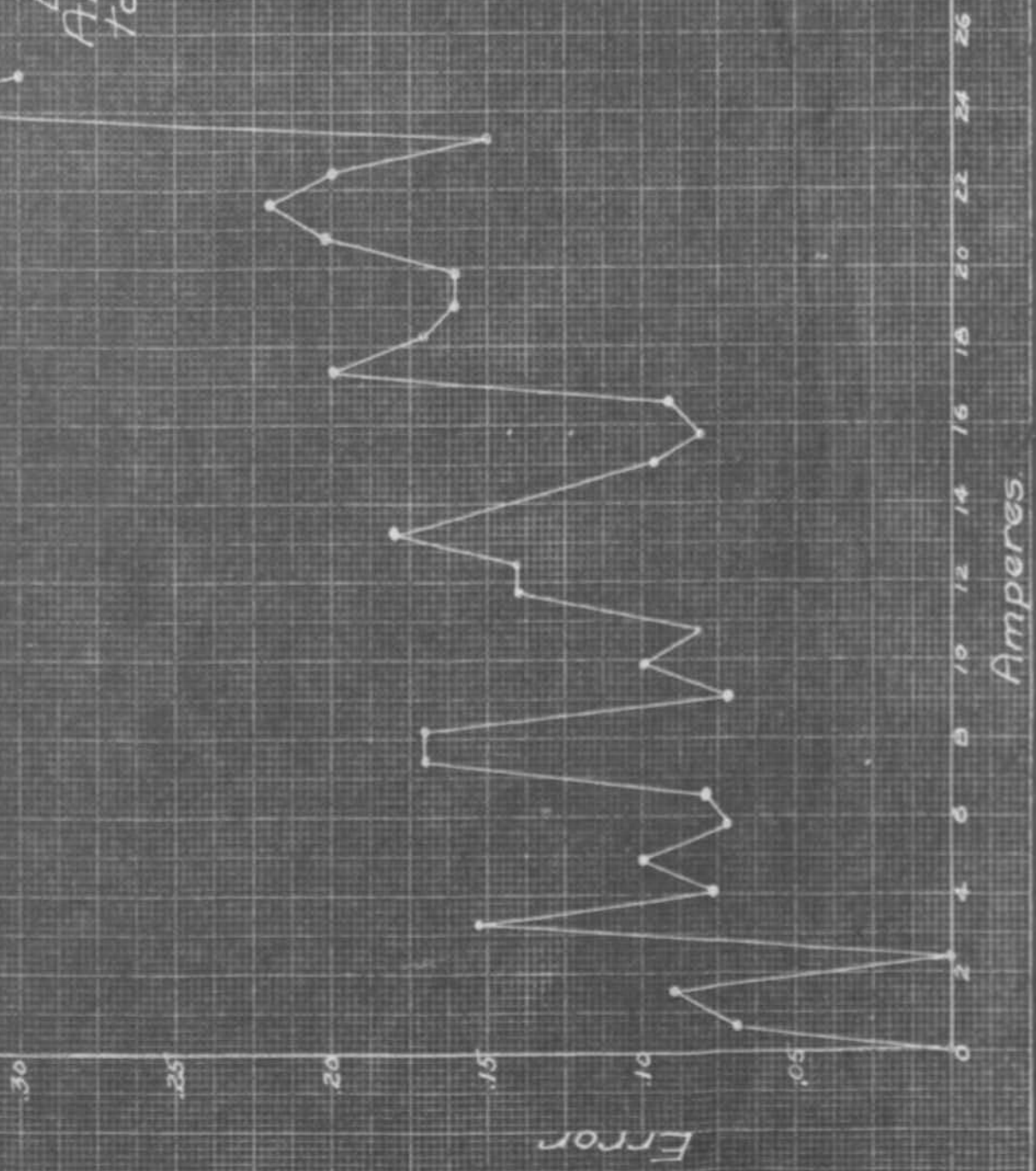
Ammeter # 3299			30 ampere shunt #8349 56-10		
Standard	#3299	Error	Standard	#3299	Error
.9	10	.067	15.10	180	.100
1.75	20	.087	15.90	190	.080
2.50	30	.000	16.76	200	.090
3.35	40	.015	17.70	210	.200
4.25	50	.080	18.50	220	.170
5.10	60	.100	19.33	230	.160
5.90	70	.070	20.16	240	.160
6.75	80	.080	21.00	250	.20
7.67	90	.170			
8.50	100	.170			
9.25	110	.070			
10.10	120	.100			
10.90	130	.080			
11.80	140	.140			
12.64	150	.140			
13.50	160	.180			
14.30	170	.140			



Calibration of Milli-Voltmeter

No. 3299

Error in Amperes Added to Reading



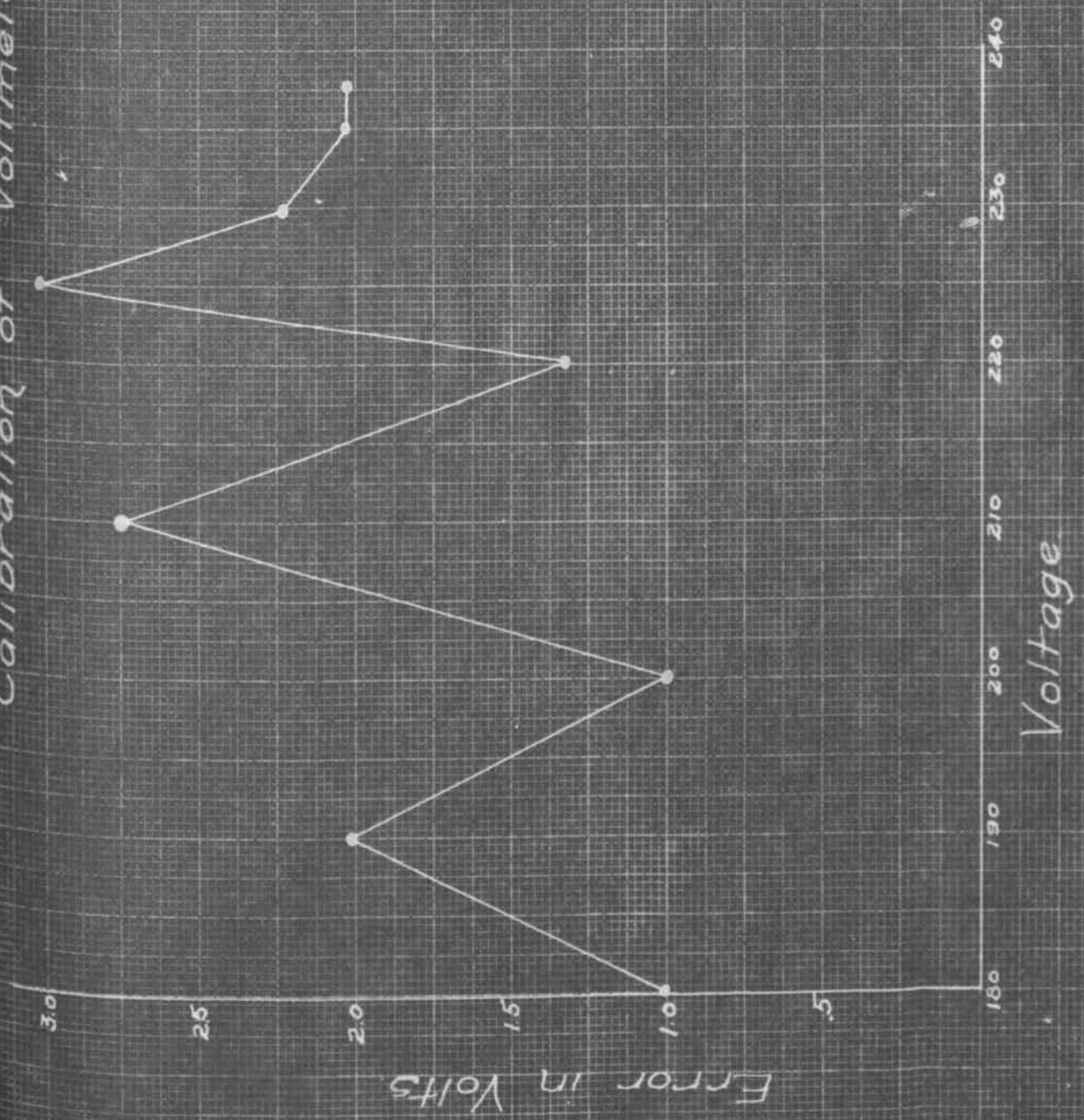
Calibration of Instruments (con't)

Voltmeter #3381

Standard	#3381	Error
201	200	1.0
212.7	210	2.7
221.3	220	1.3
232.2	230	2.2
240.0	238	2.0
237.0	235	2.0
228.0	225	3.0
192.0	190	2.0
181.0	180	1.0

Calibration of Voltmeter No. 3381

Error Added to Reading



FAN TEST NUMBER 1

May 8, 1922.

1/2 Opening

Length of pipe 23 ft.

Test run with no equalizer.

	Volts	Amperes	R.P.M.
1st	230	210/12	395
2nd	230	210/12	395
Av.	230	17.5	395

Top Readings			Side Readings				
	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	-.002	+.001	.000		-.002	+.001	.000
1	.166	.195	1.500	1	.130	.132	1.542
2	.196	.222	1.501	2	.175	.166	1.538
3	.219	.238	1.501	3	.191	.181	1.543
4	.228	.247	1.502	4	.200	.198	1.544
5	.230	.244	1.503	5	.215	.207	1.543
6	.171	.176	1.500	6	.230	.212	1.543
7	.136	.140	1.504	7	.221	.220	1.539
8	.125	.129	1.506	8	.218	.206	1.535
9	.124	.140	1.502	9	.200	.190	1.539
10	.081	.103	1.500	10	.150	.162	1.543

FAN TEST NUMBER 2

May 9, 1922

5/8 Opening

Length of pipe 23 ft.

Test run with no equalizer.

	Volts	Amperes	R.P.M.
1st	228	240/12	390
2nd	228	243/12	392
Av.	228	20.25	391

Top Readings			Side Readings				
	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	-.002	-.001	.000		-.002	-.001	.000
1	.300	.325	1.230	1	.314	.325	1.252
2	.290	.310	1.228	2	.386	.394	1.255
3	.284	.286	1.229	3	.340	.331	1.250
4	.270	.280	1.231	4	.310	.300	1.253
5	.275	.281	1.231	5	.300	.272	1.250
6	.284	.271	1.231	6	.270	.240	1.250
7	.270	.265	1.228	7	.230	.200	1.257
8	.245	.250	1.230	8	.195	.282	1.258
9	.220	.230	1.232	9	.186	.199	1.261
10	.150	.140	1.219	10	.190	.211	1.251

FAN TEST NUMBER 3

May 8, 1922

3/4 Opening

Length of pipe 23 ft.

Test run with no equalizer.

	Volts	Amperes	R.P.M.
1st	235	282/12	391
2nd	234	282/12	393
Av.	234.5	23.5	392

Top Readings

Side Readings

	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	-.002	-.001	.000		-.002	-.001	.000
1	.382	.462	.918	1	.391	.421	.933
2	.412	.460	.920	2	.431	.447	.933
3	.372	.397	.930	3	.462	.460	.937
4	.358	.388	.923	4	.461	.451	.938
5	.403	.413	.929	5	.461	.437	.938
6	.410	.390	.917	6	.372	.328	.938
7	.357	.347	.920	7	.349	.315	.938
8	.342	.345	.922	8	.310	.309	.940
9	.287	.321	.924	9	.341	.369	.939
10	.202	.202	.952	10	.297	.337	.932

FAN TEST NUMBER 4

May 9, 1922.

7/8 Opening

Length of pipe 23 ft.

Test run with no equalizer.

	Volts	Amperes	R.P.M.
1st	229	285/12	375
2nd	225	292/12	375
Av.	227 1/2	24.33	375

Top Readings

Side Readings

	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	-.001	-.001	.000		-.001	-.001	.000
1	.510	.565	.593	1	.415	.442	.602
2	.520	.558	.594	2	.490	.495	.608
3	.480	.492	.593	3	.490	.498	.607
4	.470	.472	.596	4	.500	.471	.603
5	.485	.470	.591	5	.520	.490	.603
6	.440	.350	.597	6	.450	.395	.609
7	.390	.330	.596	7	.410	.475	.609
8	.350	.341	.597	8	.408	.408	.610
9	.290	.335	.598	9	.420	.454	.610
10	.230	.258	.598	10	.310	.370	.603

FAN TEST NUMBER 5

December 15, 1921.

Full opening

Length of pipe 23 ft.

Test run with 1 equalizer 34" from fan opening

	Volts	Amperes	R.P.M.
1st.	225	142.5/12	257
2nd.	222	142.5/12	257
Av.	223½	11.89	257

	Top Readings			Side Readings		
	V pt.	V. pz.	S pz.	V. pt.	V pz.	S. pz
Zero	-.013	+.030	+.020	-.013	+.030	+.020
1	.113	.161	.038	.541	.563	.038
2	.139	.176	.083	.491	.513	.039
3	.155	.184	.038	.407	.431	.039
4	.200	.231	.038	.310	.330	.039
5	.221	.251	.038	.230	.255	.039
6	.211	.241	.038	.227	.262	.040
7	.282	.310	.039	.291	.320	.040
8	.310	.330	.039	.408	.442	.041
9	.303	.320	.039	.440	.467	.041
10	.181	.281	.039	.377	.403	.041



FAN TEST NUMBER 6

FEBRUARY 20, 1922

$\frac{1}{2}$  Opening

Length of pipe 23 ft.

One Equalizer spaced 5' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st.	230	92/12	280.23
2nd.	230.5	94/12	283
Av.	230.25	7.83	281.5

	Top Readings			Side Readings		
	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	-.013	-.030	+.020	-.013	-.030	+.020
1	.032	.120	.695	.100	.171	.697
2	.032	.190	.691	.120	.179	.696
3	.037	.105	.686	.097	.169	.697
4	.032	.108	.689	.089	.160	.698
5	.036	.110	.688	.091	.169	.698
6	.119	.194	.686	.064	.136	.697
7	.164	.240	.692	.071	.147	.692
8	.168	.242	.692	.099	.170	.698
9	.168	.241	.692	.096	.171	.699
10	.143	.213	.699	.071	.146	.707

FAN TEST NUMBER 7

FEBRUARY 20, 1922.

5/8 Opening.

Length of Pipe 23 ft.

One equalizer spaced 5' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st.	V 230	109/12	282
2nd.	230	109/12	283
Av.	230	8.08	282.5

	Top Readings			Side Readings		
	V pt.	V pz.	S. pz.	V pt.	V pz.	S pz.
Zero	-.013	+.030	+.020	-.013	+.030	+.020
1	.097	.171	.612	.069	.147	.610
2	.103	.178	.613	.125	.194	.606
3	.120	.199	.613	.117	.197	.611
4	.125	.201	.612	.107	.192	.596
5	.150	.230	.614	.116	.196	.608
6	.120	.200	.617	.140	.225	.614
7	.139	.217	.612	.165	.248	.612
8	.179	.251	.617	.171	.259	.600
9	.195	.269	.615	.230	.319	.605
10	.140	.209	.620	.158	.235	.610

FAN TEST NUMBER 8

FEBRUARY 20, 1922.

3/4 Opening

Length of pipe 23 ft.

One equalizer spaced 5' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st.	219	112/12	266
2nd.	219	112/12	266
Av.	219	9.33	266

Top Readings

Side Readings

	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	-.013	+.03	+.02	-.013	+.03	+.02
1	.091	.153	.419	.135	.192	.418
2	.103	.163	.419	.172	.240	.412
3	.105	.161	.420	.190	.250	.412
4	.142	.197	.420	.200	.262	.415
5	.149	.209	.420	.170	.224	.414
6	.164	.222	.420	.154	.208	.419
7	.171	.231	.421	.160	.220	.418
8	.197	.251	.420	.182	.243	.417
9	.219	.281	.423	.266	.321	.419
10	.150	.210	.420	.242	.300	.416

FAN TEST NUMBER 9

FEBRUARY 20, 1922.

7/8 Opening

Length of pipe 23 ft.

One equalizer spaced 5' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st.	229	130/12	272
2nd.	230	131/12	276
Av.	229½	10.83	274

	Top Readings			Side Readings		
	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	-.013	+.030	+.02	-.013	+.030	+.02
1	.262	.311	.318	.119	.153	.314
2	.310	.357	.321	.119	.153	.314
3	.283	.330	.321	.128	.168	.313
4	.284	.332	.321	.133	.173	.314
5	.221	.261	.321	.171	.213	.313
6	.199	.239	.321	.229	.271	.315
7	.245	.286	.322	.259	.301	.316
8	.282	.327	.322	.276	.320	.316
9	.308	.351	.322	.290	.339	.317
10	.295	.342	.322	.187	.227	.317

FAN TEST NUMBER 10

FEBRUARY 23, 1922.

$\frac{1}{2}$  Opening

Length of pipe 23 ft.

One equalizer spaced 7' 1" from fan opening

	Volts	Amperes	R.P.M.
1st.	234	93/12	284
2nd.	234	98/12	280
Av.	234	7.95	282

Top Readings

Side Readings

	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	o	+.026	+.029	o	+.026	+.029
1	.088	.177	.699	.036	.134	.679
2	.088	.177	.700	.050	.150	.682
3	.100	.191	.704	.066	.164	.677
4	.091	.175	.706	.060	.153	.678
5	.120	.210	.699	.069	.168	.688
6	.050	.148	.701	.124	.223	.698
7	.048	.132	.704	.128	.223	.690
8	.048	.132	.703	.166	.260	.689
9	.036	.128	.705	.150	.248	.688
10	.030	.119	.690	.159	.240	.699

FAN TEST NUMBER 11

FEBRUARY 23, 1922.

5/8 Opening

Length of pipe 23 ft.

One equalizer spaced 7' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st.	225	97/12	263
2nd.	220	97/12	264
Av.	222.5	7.91	263.5

Top Readings

Side Readings

	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	-.003	+.019	+.019	-.003	+.019	+.019
1	.070	.149	.517	.114	.192	.530
2	.070	.150	.520	.120	.202	.527
3	.065	.147	.525	.134	.217	.527
4	.077	.156	.520	.108	.184	.529
5	.110	.192	.522	.118	.198	.530
6	.089	.170	.520	.112	.192	.523
7	.103	.187	.522	.103	.180	.533
8	.103	.187	.521	.132	.216	.530
9	.148	.231	.530	.150	.230	.531
10	.082	.162	.521	.188	.263	.525

FAN TEST NUMBER 12

FEBRUARY 23, 1922.

$\frac{3}{4}$  Opening

Length of pipe 23 ft.

One equalizer spaced 7' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st.	222	108/12	262
2nd.	219	108/12	260
Av.	220.5	9	261

Top Readings

Side Readings

	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	-.003	+.019	+.019	-.003	+.019	+.019
1	.115	.170	.423	.108	.163	.421
2	.127	.174	.422	.195	.253	.422
3	.083	.140	.426	.210	.268	.424
4	.090	.152	.428	.186	.243	.421
5	.122	.188	.428	.203	.261	.420
6	.150	.224	.427	.141	.199	.425
7	.186	.249	.425	.130	.189	.424
8	.170	.230	.425	.174	.230	.423
9	.175	.236	.429	.193	.247	.422
10	.103	.168	.426	.242	.301	.427

FAN TEST NUMBER 13

FEBRUARY 23, 1922.

7/8 Opening

Length of pipe 23 ft.

One equalizer spaced 7' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st.	229	126/12	270
2nd.	226	125/12	270
Av.	227.5	10.45	270

	Top Readings			Side Readings		
	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	0	+ .023	+ .028	- .003	+ .019	+ .019
1	.172	.212	.311	.2	.25	.312
2	.180	.222	.311	.278	.326	.315
3	.118	.157	.312	.270	.315	.317
4	.122	.162	.312	.220	.260	.316
5	.140	.182	.312	.230	.270	.317
6	.215	.261	.310	.188	.221	.315
7	.272	.320	.310	.170	.213	.315
8	.253	.297	.310	.269	.310	.315
9	.259	.302	.310	.352	.392	.315
10	.165	.201	.310	.391	.429	.315



FAN TEST NUMBER 14

May 11, 1922.

1/2 Opening

Length of pipe 23 ft.

First equalizer spaced 5' 1" from fan opening.

Second equalizer spaced 13' 2" from fan opening.

	Volts	Amperes	R.P.M.
1st	227	187/12	384
2nd	217	182/12	374
Av.	222	15.37	379

Top Readings

Side Readings

	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	-.003	-.001	.000		-.003	-.001	.000
1	.069	.097	1.286	1	.224	.204	1.303
2	.079	.102	1.300	2	.198	.304	1.309
3	.084	.110	1.298	3	.216	.312	1.304
4	.097	.117	1.298	4	.216	.312	1.308
5	.099	.122	1.295	5	.188	.200	1.316
c	.170	.196	1.295	c	.146	.170	1.312
6	.247	.280	1.288	6	.115	.122	1.308
7	.247	.285	1.277	7	.115	.126	1.309
8	.258	.250	1.276	8	.160	.166	1.309
9	.242	.232	1.276	9	.135	.148	1.310
10	.121	.193	1.296	10	.079	.080	1.305

FAN TEST NUMBER 15

May 10, 1922.

5/8 Opening

Length of pipe 23 ft.

First equalizer spaced 5' 1" from fan opening.

Second equalizer spaced 13' 2" from fan opening.

	Volts	Amperes	R.P.M.
1st	230	214/12	384
2nd	228	214/12	382
Av.	229	17.83	383

Top Readings

Side Readings

	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	+.002	.000	-.002		+.002	.000	.000
1	.192	.228	1.115	1	.180	.151	1.130
2	.205	.239	1.117	2	.128	.157	1.129
3	.232	.274	1.117	3	.150	.186	1.133
4	.275	.267	1.119	4	.174	.209	1.137
5	.277	.292	1.111	5	.200	.240	1.139
c	.222	.231	1.109	c	.220	.251	1.136
6	.230	.250	1.107	6	.250	.290	1.140
7	.304	.330	1.107	7	.218	.261	1.140
8	.302	.320	1.110	8	.270	.309	1.139
9	.305	.321	1.110	9	.232	.290	1.144
10	.252	.247	1.131	10	.152	.208	1.140

FAN TEST NUMBER 16

May 12, 1922.

3/4 Opening

Length of pipe 23 ft.

First equalizer spaced 5' 1" from fan opening.

Second equalizer spaced 13' 2" from fan opening.

	Volts	Amperes	R.P.M.
1st	239	268/12	394
2nd	230	260/12	389
Av.	234.5	22.0	391.5

Top Readings

Side Readings

	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	-.003	-.001	+.002		-.003	-.001	+.022
1	.305	.291	.907	1	.152	.122	.931
2	.332	.338	.918	2	.142	.112	.942
3	.310	.322	.920	3	.163	.166	.941
4	.370	.379	.918	4	.181	.182	.949
5	.357	.364	.916	5	.224	.221	.948
c	.268	.278	.914	c	.266	.272	.947
6	.250	.252	.915	6	.352	.362	.942
7	.272	.282	.916	7	.318	.321	.950
8	.380	.378	.914	8	.408	.417	.952
9	.408	.402	.914	9	.337	.350	.952
10	.295	.322	.922	10	.222	.231	.950

FAN TEST NUMBER 17

May 9, 1922.

7/8 Opening

Length of pipe 23 ft.

First equalizer spaced 5' 1" from fan opening.

Second equalizer spaced 13' 2" from fan opening.

	Volts	Amperes	R.P.M.
1st	234	280/12	379
2nd	230	282/12	372
Av.	232	25.5	375.5

Top Readings			Side Readings				
	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	+.002	.000	-.002		+.002	.000	-.003
1	.352	.322	.589	1	.232	.213	.578
2	.390	.378	.582	2	.195	.162	.578
3	.383	.368	.583	3	.239	.227	.578
4	.446	.432	.582	4	.254	.201	.580
5	.428	.420	.582	5	.277	.290	.581
c	.320	.306	.580	c	.315	.330	.580
6	.335	.330	.580	6	.415	.421	.580
7	.341	.340	.586	7	.403	.403	.580
8	.450	.458	.587	8	.480	.499	.583
9	.546	.542	.589	9	.421	.435	.582
10	.462	.462	.589	10	.282	.292	.581

FAN TEST NUMBER 18

MARCH 7, 1922.

$\frac{1}{2}$  Opening

Length of pipe 14 Ft. 2"

Test run with no equalizer.

	Volts	Amperes	R.P.M.
1st.	230	87/12	279
2nd.	230	88/12	279
Av.	230	7.30	279

	Top Readings			Side Readings		
	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	.000	.000	.000	.000	.000	.000
1	.076	.10	.674	.065	.106	.713
2	.090	.119	.674	.080	.122	.710
3	.107	.130	.676	.086	.122	.709
4	.118	.142	.679	.099	.133	.707
5	.130	.149	.680	.109	.130	.708
6	.068	.080	.670	.142	.171	.705
7	.050	.068	.677	.163	.193	.706
8	.050	.070	.688	.160	.196	.713
9	.050	.071	.692	.168	.200	.701
10	.025	.053	.688	.132	.174	.710

FAN TEST NUMBER 19

MARCH 8, 1922

5/8 Opening

Length of Pipe 14' 2"

Test run with no equalizer.

	Volts	Amperes	R.P.M.
1st.	230	108/12	279
2nd	229	107/12	282
Av.	229.5	8.91	280.5

	Top Readings			Side Readings		
	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	.000	.000	.000	.000	.000	.000
1	.091	.107	.662	.082	.090	.661
2	.095	.096	.661	.123	.138	.665
3	.096	.098	.661	.139	.153	.668
4	.103	.107	.660	.138	.150	.670
5	.131	.138	.668	.142	.152	.671
6	.125	.133	.668	.140	.150	.670
7	.117	.125	.665	.141	.158	.668
8	.112	.123	.664	.160	.178	.674
9	.110	.127	.663	.200	.225	.674
10	.087	.100	.667	.212	.232	.678

FAN TEST NUMBER 20

MARCH 8, 1922.

$\frac{3}{4}$  Opening

Length of pipe 14' 2"

Test run with no equalizer.

	Volts	Amperes	R.P.M.
1st.	230	118/12	281
2nd.	230	119/12	279
Av.	230	9.87	280

Top Readings

Side Readings

	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	.000	.000	.000	.000	.000	.000
1	.172	.169	.506	.080	.072	.502
2	.145	.138	.506	.120	.106	.506
3	.132	.113	.516	.130	.100	.503
4	.140	.119	.500	.174	.140	.507
5	.179	.158	.502	.195	.170	.504
6	.219	.208	.507	.192	.179	.503
7	.223	.220	.507	.185	.186	.505
8	.220	.219	.507	.214	.222	.502
9	.200	.200	.508	.248	.269	.509
10	.130	.139	.504	.272	.293	.508

FAN TEST NUMBER 21

March 7, 1922.

7/8 Opening

Length of pipe 14' 2"

Test run with no equalizer.

	Volts	Amperes	R.P.M.
1st.	230	128/12	277
2nd.	231	129/12	279
Av.	230.5	10.70	278

	Top Readings			Side Readings.		
	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	.000	.000	.000	.000	.000	.000
1	.278	.270	.348	.130	.090	.344
2	.203	.173	.343	.129	.069	.338
3	.195	.171	.345	.150	.080	.341
4	.173	.127	.343	.170	.092	.348
5	.232	.186	.343	.251	.188	.340
6	.297	.257	.349	.242	.212	.340
7	.302	.273	.349	.271	.251	.341
8	.293	.270	.348	.300	.292	.345
9	.289	.285	.348	.307	.312	.345
10	.152	.156	.349	.280	.290	.347



FAN TEST NUMBER 22

May 22, 1922.

1/2 Opening

Length of pipe 14 ft. 2 in.

One equalizer spaced 5' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st	230	193/12	389
2nd	228	195/12	389
Av.	229	16.16	389

Top Readings				Side Readings			
	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	+.002	-.002	-.004		+.024	-.015	-.010
1	.058	.130	1.377	1	.170	.220	1.365
2	.067	.127	1.375	2	.243	.250	1.350
3	.055	.105	1.360	3	.240	.220	1.345
4	.049	.079	1.350	4	.200	.200	1.350
5	.061	.101	1.340	5	.165	.140	1.360
c	.149	.200	1.375	c	.100	.120	1.355
6	.207	.227	1.380	6	.054	.074	1.360
7	.270	.270	1.360	7	.053	.062	1.357
8	.299	.359	1.350	8	.080	.087	1.360
9	.271	.300	1.355	9	.100	.130	1.350
10	.233	.283	1.375	10	.100	.127	1.345

FAN TEST NUMBER 23

May 22, 1922.

5/8 Opening

Length of pipe 14 ft. 2 in.

One equalizer spaced 5' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st	229	257/12	389
2nd	231	239/12	397
Av.	230	19.83	393

Top Readings				Side Readings			
	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	+.003	-.015	.000		-.002	-.012	.000
1	.210	.250	1.143	1	.123	.173	1.190
2	.248	.295	1.153	2	.182	.213	1.175
3	.265	.300	1.180	3	.182	.215	1.155
4	.301	.309	1.175	4	.227	.257	1.160
5	.260	.280	1.160	5	.230	.280	1.165
c	.251	.289	1.165	c	.251	.301	1.170
6	.268	.318	1.175	6	.222	.272	1.170
7	.238	.288	1.180	7	.188	.218	1.175
8	.273	.313	1.195	8	.205	.255	1.180
9	.305	.355	1.185	9	.265	.315	1.195
10	.255	.300	1.180	10	.220	.270	1.190

FAN TEST NUMBER 24

May 24, 1922.

3/4 Opening Length of pipe 14 ft. 2 in.

One equalizer spaced 5' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st	230	272/12	391
2nd	230	272/12	391
Av.	230	22.66	391

Top Readings				Side Readings			
	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	+.003	-.016	.000		+.003	-.017	.000
1	.330	.380	.850	1	.123	.173	.852
2	.423	.473	.855	2	.152	.202	.851
3	.432	.480	.852	3	.173	.223	.850
4	.409	.450	.847	4	.180	.230	.845
5	.350	.375	.850	5	.207	.257	.850
c	.257	.300	.855	c	.332	.382	.851
6	.216	.250	.860	6	.407	.440	.855
7	.210	.260	.855	7	.356	.400	.852
8	.270	.320	.845	8	.330	.347	.848
9	.314	.364	.850	9	.333	.372	.851
10	.336	.386	.845	10	.342	.382	.852

FAN TEST NUMBER 25

May 24, 1922

7/8 Opening Length of pipe 14 ft. 2 in.

One equalizer spaced 5' 1" from fan opening.

	Volts	Amperes	R.P.M.
1st	230	307/12	388
2nd	230	307/12	388
Av.	230	25.6	388

Top Readings			Side Readings				
	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	+.030	-.020	.000		+.003	-.017	.000
1	.480	.485	.560	1	.152	.192	.559
2	.562	.570	.557	2	.167	.205	.558
3	.531	.551	.556	3	.182	.220	.556
4	.523	.540	.553	4	.210	.250	.557
5	.400	.410	.553	5	.245	.280	.557
c	.304	.310	.555	c	.337	.377	.556
6	.300	.307	.554	6	.460	.500	.559
7	.402	.410	.557	7	.507	.547	.560
8	.509	.510	.556	8	.498	.535	.560
9	.643	.649	.555	9	.490	.530	.559
10	.594	.600	.557	10	.510	.550	.557

FAN TEST NUMBER 26

May 20, 1922.

1/2 Opening      Length of pipe 14 ft. 2 in.

First equalizer spaced 3' 9" from fan opening.

Second equalizer spaced 7' 7" from fan opening.

	Volts	Amperes	R.P.M.
1st	235	195/12	401
2nd	239	195/12	403
Av.	237	16.25	402

Top Readings			Side Readings				
	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	-.01	+.002	-.012		-.01	+.002	-.012
1	.090	.180	1.410	1	.281	.371	1.390
2	.082	.172	1.400	2	.333	.423	1.392
3	.063	.143	1.395	3	.272	.362	1.397
4	.050	.130	1.390	4	.236	.326	1.402
5	.038	.118	1.392	5	.112	.190	1.400
c	.080	.160	1.390	c	.036	.103	1.397
6	.133	.913	1.397	6	.023	.100	1.395
7	.241	.321	1.392	7	.060	.142	1.400
8	.240	.320	1.395	8	.173	.263	1.410
9	.251	.341	1.397	9	.105	.195	1.397
10	.221	.311	1.400	10	.160	.250	1.405

FAN TEST NUMBER 27

May 19, 1922.

5/8 Opening                      Length of pipe 14 ft. 2 in.

First equalizer spaced 3' 9" from fan opening.

Second equalizer spaced 7' 7" from fan opening.

	Volts	Amperes	R.P.M.
1st	232	228/12	386
2nd	230	224/12	383
Av.	231	18.85	384.5

Top Readings

Side Readings

	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	+.001	+.01	-.006		-.003	+.01	-.003
1	.175	.238	1.165	1	.233	.295	1.162
2	.200	.250	1.170	2	.300	.325	1.165
3	.192	.220	1.167	3	.260	.310	1.170
4	.280	.340	1.170	4	.288	.316	1.175
5	.330	.365	1.176	5	.290	.355	1.172
c	.380	.375	1.167	c	.296	.385	1.162
6	.248	.300	1.175	6	.185	.230	1.165
7	.268	.340	1.170	7	.156	.213	1.172
8	.150	.200	1.172	8	.181	.226	1.170
9	.192	.212	1.175	9	.124	.290	1.170
10	.128	.178	1.170	10	.216	.264	1.168

FAN TEST NUMBER 28

May 19, 1922.

3/4 Opening          Length of pipe 14 ft. 2 in.

First equalizer spaced 3' 9" from fan opening.

Second equalizer spaced 7' 7" from fan opening.

	Volts	Amperes	R.P.M.
1st	227	270/12	387
2nd	228	268/12	387
Av.	227.5	22.42	387

Top Readings

Side Readings

	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	-.001	-.01	+.006		-.001	-.01	+.006
1	.309	.379	.867	1	.457	.507	.871
2	.378	.458	.872	2	.412	.462	.870
3	.340	.410	.875	3	.348	.408	.869
4	.428	.460	.878	4	.252	.278	.870
5	.380	.440	.877	5	.246	.306	.869
c	.340	.396	.875	c	.450	.510	.868
6	.190	.250	.879	6	.391	.451	.871
7	.191	.251	.876	7	.286	.340	.869
8	.124	.184	.875	8	.304	.360	.868
9	.139	.199	.874	9	.321	.380	.867
10	.121	.191	.875	10	.292	.362	.866

FAN TEST NUMBER 29

May 19, 1922.

7/8 Opening

Length of pipe 14 ft. 2 in.

First equalizer spaced 3' 9" from fan opening.

Second equalizer spaced 7' 7" from fan opening.

	Volts	Amperes	R.P.M.
1st	231	310/12	387
2nd	232	310/12	391
Av.	231.5	25.83	389

Top Readings

Side Readings

	V pt.	V pz.	S pz.		V pt.	V pz.	S pz.
Zero	+.005	+.008	--.009		+.005	+.006	--.009
1	.441	.491	.547	1	.471	.497	.550
2	.584	.644	.550	2	.447	.479	.552
3	.519	.560	.552	3	.332	.382	.555
4	.630	.680	.555	4	.285	.345	.560
5	.462	.502	.556	5	.263	.313	.557
c	.495	.545	.557	c	.592	.627	.559
6	.355	.400	.555	6	.553	.603	.558
7	.308	.329	.558	7	.432	.482	.559
8	.210	.250	.559	8	.390	.392	.560
9	.221	.270	.560	9	.413	.415	.561
10	.170	.196	.561	10	.405	.455	.561



FAN TEST NUMBER 30

$\frac{1}{2}$  Opening

JUNE 6, 1922

Length of pipe 14 ft 2"

Test run with no equalizer.

Barometer 28.92 Temperature 91.3 Rel. Humid.

	Volts	Amperes	R.P.M.
1st.	231	207/12	410
2nd	232	216/12	1212
Av.	231.5	17.62	411

	Top readings			Side Readings.		
	V pt.	V pz.	S pz.	v pt.	V pz.	S pz.
Zero	-.003	-.006	-.000	-.003	-.006	-.009
1	.123	.213	1.420	.149	.241	1.380
2	.150	.233	1.420	.203	.357	1.380
3	.183	.261	1.420	.221	.371	1.375
4	.199	.269	1.444	.247	.392	1.370
5	.232	.292	1.430	.282	.427	1.370
c	.277	.317	1.430	.253	.380	1.385
6	.283	.330	1.435	.163	.273	1.380
7	.301	.351	1.435	.130	.257	1.385
8	.321	.379	1.435	.137	.263	1.385
9	.323	.397	1.450	.113	.245	1.380
10	.233	.310	1.445	.097	.241	1.380

FAN TEST NUMBER 31

JUNE 6, 1922

5/8 Opening

Length of pipe 14' 2"

Test run with no equalizer.

Barometer 28.92 Temperature 91.3 Rel. Humid.

	Volts	Amperes	R.P.M.
1st.	230	225/12	406
2nd.	231	225/12	406
Av.	230.5	18.75	406

	Top Readings			Side Readings		
	v pt.	v pz.	S pz.	v pt.	v pz.	S pz.
Zero	-.003	-.006	-.017	1.000	-.006	-.003
1	.152	.192	1.22	.310	.398	1.220
2	.120	.140	1.23	.331	.401	1.210
3	.138	.152	1.230	.287	.340	1.215
4	.193	.213	1.230	.266	.320	1.220
5	.250	.271	1.220	.280	.331	1.210
c	.290	.320	1.230	.280	.330	1.218
6	.293	.327	1.240	.250	.302	1.210
7	.310	.353	1.215	.240	.292	1.220
8	.370	.422	1.235	.230	.286	1.210
9	.412	.462	1.240	.230	.289	1.220
10	.445	.502	1.245	.200	.265	1.220

FAN TEST NUMBER 32

JUNE 6, 1922

3/4 Opening Length of pipe 14' 2"

Test run with no equalizer

Barometer 28.92 Temperature 91.3 Rel. Humid.

	Volts	Amperes	R.P.M.
1st.	231	290/12	405
2nd	230	293/12	408
Av.	230.5	24.3	406.5

	Top Readings			Side Readings		
	V pt.	V pz.	S pz.	v pt.	v pz.	S pz.
Zero	.001	.000	.000	-.006	-.005	-.005
1	.396	.216	.959	.375	.430	.932
2	.142	.142	.945	.360	.410	.910
3	.170	.130	.930	.280	.301	.909
4	.221	.167	.937	.261	.271	.915
5	.312	.257	.939	.307	.297	.905
c	.411	.382	.940	.357	.321	.909
6	.400	.397	.940	.402	.382	.915
7	.412	.421	.940	.381	.371	.913
8	.467	.487	.940	.351	.347	.910
9	.542	.577	.942	.310	.336	.910
10	.562	.610	.945	.265	.317	.920

FAN TEST NUMBER 33

JUNE 6, 1922

7/8 Opening

Length of pipe 14' 2"

Barometer 28.92 Temperature 91.3 Rel. Humid.

	volts	Amperes	R.P.M.
1st	231	320/12	401
2nd	229	315/12	399
Av.	230	26.45	400

	Top Readings			Side Readings.		
	v pt.	v pz.	S pz.	v pt.	v pz.	S pz.
Zero	-.004	-.014	-.006	-.003	-.004	-.003
1	.211	.192	.642	.487	.541	.605
2	.212	.161	.645	.501	.531	.600
3	.231	.141	.638	.443	.443	.600
4	.268	.135	.639	.377	.341	.602
5	.382	.232	.632	.401	.347	.611
c	.482	.372	.635	.445	.365	.615
6	.492	.400	.637	.503	.403	.610
7	.532	.479	.637	.455	.365	.603
8	.620	.592	.642	.371	.310	.597
9	.645	.640	.645	.342	.337	.600
10	.506	.506	.641	.205	.235	.604

FAN TEST NUMBER 34

June 7 1922

$\frac{1}{2}$  Opening

Length of pipe 14' 2"

1 Equalizer spaced 2 feet 3 in. from fan opening.

Barometer	Temperature	Rel. Humid.
volts	Amperes	R.P.M.
1st. 230	210/12	413
2nd. 231	215/12	415
Av. 230.5	17.87	414

	Top Readings			Side Readings.		
	v pt.	v pz.	s pz.	v pt.	v pz.	spz.
Zero	-.003	-.006	-.009	-.003	-.006	-.010
1	.068	.140	1.420	.193	.280	1.400
2	.079	.148	1.415	.230	.315	1.395
3	.070	.135	1.390	.240	.328	1.390
4	.058	.126	1.415	.210	.296	1.395
5	.049	.118	1.400	.170	.258	1.400
c	.103	.170	1.405	.128	.209	1.405
6	.200	.273	1.395	.074	.150	1.400
7	.260	.341	1.390	.100	.180	1.380
8	.282	.358	1.400	.150	.233	1.365
9	.278	.350	1.390	.190	.276	1.375
10	.240	.310	1.385	.172	.251	1.390

FAN TEST NUMBER 35b

June 7, 1922

5/8 Opening

Length of Pipe 14' 2"

One equalizer spaced 2' 3" from fan opening.

	volts	Amperes	R.P.M.
1st.	228	248/12	496
2nd.	229	260/12	404
Av.	228.5	21.15	405

Top Readings  
Equal. blades par. to fan blades

Side Readings  
19 to horizontal

	v pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	-.003	-.006	-.010	-.005	-.006	-.015
1	.262	.320	1.160	.109	.170	1.160
2	.270	.325	1.185	.158	.213	1.150
3	.266	.320	1.200	.143	.203	1.170
4	.280	.333	1.200	.161	.212	1.150
5	.268	.320	1.195	.190	.250	1.150
c	.230	.280	1.210	.270	.339	1.160
6	.200	.244	1.180	.260	.328	1.175
7	.150	.200	1.180	.280	.349	1.165
8	.148	.190	1.195	.260	.329	1.170
9	.160	.215	1.180	.290	.352	1.165
10	.118	.169	1.165	.280	.342	1.140

FAN TEST NUMBER 35b

June 7 1922

5/8 Opening

Length of pipe 14' 2"

one equalizer spaced 2' 3" from fan opening.

	volts	Amperes	R.P.M.
1st.	235	260/12	410
2nd.	231	252/12	406
Av.	233	21.33	408

	Side readings Equalizer blades 45 to Hor.			Side Readings Equal. blades par. to Hor.		
	V pt.	v pz.	s pz.	v pt.	v pz.	s pz.
Zero	-.005	-.006	-.015	-.005	-.006	-.015
1	.135	.210	1.165	.111	.171	1.13
2	.171	.215	1.165	.131	.187	1.15
3	.164	.230	1.170	.163	.230	1.18
4	.183	.253	1.175	.183	.251	1.18
5	.201	.281	1.170	.183	.252	1.18
c	.271	.350	1.160	.281	.351	1.165
6	.251	.325	1.150	.260	.327	1.150
7	.251	.325	1.150	.253	.325	1.150
8	.261	.341	1.130	.263	.340	1.155
9	.305	.385	1.130	.290	.360	1.150
10	.295	.367	1.140	.281	.357	1.155

FAN TEST NUMBER 36

June 7 1922

3/4 Opening

Length of pipe 14' 2"

One equalizer spaced 2' 3" from fan opening.

	Volts	Amperes	R.P.M.
1st.	229	285/12	101
2nd	233	286/12	404
Av.	231	23.80	402.5

Top Readings  
Equalizer blades parallel to horizontal

Side Readings

	v pt.	v pz.	S pz.	v pt.	V pz.	S pz.
Zero	-.002	.002	-.004	-.006	-.006	-.006
1	.380	.443	.860	.163	.207	.851
2	.420	.491	.859	.193	.231	.850
3	.390	.462	.868	.174	.210	.860
4	.420	.491	.872	.153	.193	.862
5	.360	.420	.873	.153	.193	.865
c	.330	.378	.879	.257	.307	.861
6	.270	.328	.870	.371	.420	.850
7	.254	.311	.879	.395	.445	.862
8	.310	.366	.873	.367	.417	.870
9	.310	.378	.864	.412	.462	.862
10	.220	.280	.863	.413	.463	.867



FAN TEST NUMBER 37

June 8 1922.

7/8 Opening

Length of pipe 14' 2"

One equalizer spaced 2' 3" from fan opening.

	Volts	Amperes	R.P.M.
1st.	232	320/12	397
2nd.	232	320/12	397
Av.	232	26.66	397

Top Readings  
Equalizer blades 45 to horizontal

Side Readings

	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	.000	.002	-.012	-.006	-.005	-.005
1	.549	.581	.549	.192	.217	.541
2	.573	.613	.547	.211	.241	.531
3	.603	.643	.550	.211	.231	.535
4	.583	.620	.552	.187	.207	.533
5	.423	.453	.550	.222	.242	.535
c	.357	.392	.553	.351	.371	.533
6	.372	.412	.550	.483	.507	.531
7	.387	.423	.556	.482	.502	.539
8	.452	.482	.553	.505	.535	.537
9	.468	.497	.557	.505	.531	.536
10	.384	.410	.567	.521	.551	.546

FAN TEST NUMBER 38

June 8 1922

1/2 Opening

Length of pipe 14' 2"

One equalizer spaced 6 feet 7 Inches from fan opening

Barometer 28.90 Temperature 75.7 Rel. Humi. .

	Volts	Amperes	R.P.M.
1st.	231	220/12	410
2nd.	230	222/12	408
Av.	230.5	18.5	409

Top Readings Side Readings  
Equalizer blades 45 to horizontal.

	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	.002	.001	-.020	.002	.001	-.020
1	.112	.330	1.360	.189	.322	1.355
2	.120	.238	1.370	.242	.382	1.355
3	.139	.260	1.360	.223	.353	1.345
4	.157	.271	1.345	.221	.356	1.345
5	.170	.289	1.350	.231	.371	1.365
c	.269	.388	1.370	.221	.357	1.355
6	.250	.370	1.365	.089	.223	1.345
7	.330	.449	1.370	.073	.207	1.340
8	.282	.398	1.365	.060	.200	1.355
9	.331	.446	1.380	.060	.200	1.360
10	.269	.376	1.375	.060	.200	1.365

FAN TEST NUMBER 39

June 9, 1922

5/8 Opening

Length of pipe 14' 2"

One equalizer spaced 6' 7" from fan opening.

Barometer 28.90 Temperature 75.7 Rel. Humid.

	Volts	Amperes	R.P.M.
1st.	230	255/12	399
2nd	230	250/12	401
Av.	230	21.04	400

Top Readings

Side Readings

Equalizer blades 45 to horizontal

	V pt.	V pz.	S pz.	V pt.	V pz.	Spz.
Zero	.002	.001	-.020	.002	.001	-.020
1	.161	.277	1.175	.271	.371	1.165
2	.192	.285	1.175	.271	.371	1.145
3	.202	.286	1.170	.227	.327	1.155
4	.209	.289	1.170	.183	.281	1.175
5	.231	.326	1.165	.207	.305	1.170
c	.217	.305	1.160	.249	.349	1.170
6	.286	.381	1.160	.231	.329	1.155
7	.310	.402	1.180	.179	.286	1.170
8	.317	.410	1.175	.183	.289	1.180
9	.357	.453	1.175	.172	.272	1.180
10	.321	.407	1.165	.186	.291	1.180

FAN TEST NUMBER 40

June 9, 1922

3/4 Opening

Length of pipe 14' 2"

One equalizer spaced 6' 7" from fan opening.

Barometer 28.90 Temperature 75.7 Rel. Humid.

	Volts	Amperes	R.P.M.
1st.	230	273/12	392
2nd.	230	279/12	396
Av.	230	23.0	394

Top Readings                      Side Readings  
 Equalizer blades 45 to horizontal

	V pt.	V pz.	S pz.	V pt.	V pz.	S pz.
Zero	.002	.001	-.015	.001	.000	-.015
1	.170	.232	.891	.384	.451	.862
2	.200	.262	.880	.351	.421	.867
3	.207	.266	.870	.312	.380	.865
4	.219	.223	.875	.237	.299	.862
5	.305	.364	.878	.230	.296	.860
c	.267	.328	.880	.280	.356	.863
6	.280	.349	.871	.342	.410	.862
7	.370	.440	.878	.313	.393	.860
8	.380	.448	.880	.351	.421	.859
9	.500	.462	.882	.310	.379	.859
10	.460	.507	.884	.357	.430	.855

FAN TEST NUMBER 41

June 9, 1922

7/8 Opening

Length of pipe 14' 2"

One equalizer spaced 6' 7" from fan opening.

Barometer 28.90 Temperature 75.7 Rel. Humid.

	volts	Amperes	R.P.M.
1st.	230	280/12	381
2nd	228	290/12	379
Av.	229	23.75	380

Top Readings  
Equalizer blades 45 to horizontal.

Side Readings

	V pt.	V pz.	S pz.	V pt.	V pz.	Spz.
Zero	.001	.000	-.014	.001	.000	-.015
1	.203	.236	.550	.549	.569	.549
2	.259	.291	.551	.530	.559	.548
3	.241	.278	.555	.424	.453	.549
4	.249	.280	.558	.278	.307	.550
5	.317	.347	.552	.264	.292	.549
c	.286	.317	.556	.300	.333	.548
6	.402	.427	.551	.357	.393	.553
7	.446	.476	.553	.425	.456	.555
8	.442	.471	.552	.460	.597	.554
9	.552	.581	.551	.438	.466	.556
10	.486	.502	.557	.470	.510	.556

FAN TEST NUMBER 42

June 8, 1922

$\frac{1}{2}$  Opening

Length of pipe 14' 2"

One equalizer spaced 2' 3" out. Blades 45 to Hor.

Other equalizer spaced 6' 7" out. Blades Par. to fan.

	Volts	Amperes	R.P.M.
1st.	230	206/12	406
2nd.	230	212/12	408
Av.	230	17.41	407

Top Readings

Side Readings

	V pt.	V pz.	S pz.	V pt.	V pz.	Spz.
Zero	-.003	.000	.014	.000	.002	.015
1	.080	.154	1.40	.200	.289	1.380
2	.087	.163	1.385	.260	.356	1.375
3	.064	.141	1.410	.171	.263	1.385
4	.033	.118	1.395	.239	.327	1.370
5	.039	.117	1.395	.181	.272	1.400
c	.130	.214	1.390	.130	.220	1.400
6	.160	.237	1.387	.083	.170	1.420
7	.210	.298	1.400	.070	.159	1.415
8	.300	.374	1.390	.170	.257	1.395
9	.313	.396	1.390	.173	.260	1.385
10	.180	.240	1.408	1.246	.340	1.410

FAN TEST NUMBER 43

June 8, 1922

5/8 Opening

Length of pipe 14' 2"

First equalizer spaced 2' 3" out. Blades 45 to Hor.

Second Equalizer spaced 6' 7" out. Blades Par. to fan.

Barometer 28.95 Temperature 76.7 Rel. Humid.

Volts Amperes R.P.M.

1st.	229	242/12	395
2nd	229	245/12	395
Av.	229	20.29	395

Top Readings

Side Readings

	V pt.	v pz.	S pz.	v pt.	v pz.	S pz.
Zero	-.002	.000	.015	-.003	.000	.020
1	.141	.220	1.180	.167	.251	1.170
2	.247	.321	1.170	.212	.292	1.170
3	.207	.271	1.160	.162	.239	1.160
4	.249	.321	1.160	.189	.279	1.170
5	.301	.377	1.165	.247	.331	1.160
c	.283	.367	1.165	.347	.430	1.170
6	.312	.382	1.175	.273	.353	1.160
7	.206	.281	1.170	.197	.277	1.160
8	.252	.327	1.170	.265	.342	1.165
9	.319	.397	1.175	.259	.341	1.160
10	.203	.261	1.180	.313	.383	1.160

FAN TEST NUMBER 44

June 8, 1922.

3/4 Opening

Length of pipe 14' 2"

First equalizer spaced 3' 3" out. Blades 45 to Hor.

Second equalizer spaced 6' 7" out. Blades horizontal  
 Barometer 28.95 Temperature 76.7 Rel. Humid.

	Volts	Amperes	R.P.M.
1st.	232	275/12	398
2nd.	230	281/12	400
Av.	231	23.15	399

Top Readings

Side Readings.

	v pt.	v pz.	S pz.	v pt.	v pz.	Spz.
Zero	-.003	-.001	-.005	-.003	-.001	-.006
1	.352	.402	.882	.230	.285	.873
2	.410	.465	.882	.270	.330	.869
3	.320	.373	.883	.220	.278	.873
4	.390	.445	.882	.140	.192	.860
5	.410	.467	.881	.150	.208	.869
c	.260	.312	.880	.300	.358	.868
6	.280	.328	.882	.357	.420	.862
7	.235	.284	.879	.275	.332	.870
8	.290	.343	.875	.410	.461	.872
9	.418	.469	.869	.400	.463	.860
10	.320	.360	.879	.440	.500	.862



FAN TEST NUMBER 45

June 8, 1922

7/8 Opening

Length of pipe 14' 2"

First Equalizer spaced 2' 3" out. Blades 45 to hor.

Second equalizer spaced 6' 7" out. Blades horizontal.  
Barometer 28.95 Temperature 76.7 Rel. Humid.

	volts	Amperes	R.P.M.
1st.	228	300/12	389
2nd	227	302/12	389
Av.	227.5	25.08	389

	Top Readings			Side Readings.		
	v pt.	v pz.	Spz.	v pt.	v Pz.	Spz.
Zero	.002	-.002	.000	.002	.000	.000
1	.440	.450	.549	.231	.246	.550
2	.586	.606	.555	.240	.257	.550
3	.520	.522	.557	.160	.174	.551
4	.540	.551	.560	.151	.168	.549
5	.542	.475	.558	.198	.212	.549
c	.232	.350	.558	.410	.423	.550
6	.260	.278	.559	.440	.463	.557
7	.290	.309	.559	.350	.368	.553
8	.415	.425	.560	.491	.509	.554
9	.522	.538	.561	.445	.466	.553
10	.369	.381	.564	.530	.522	.559

## METHOD OF CALCULATIONS

The zero readings of each gage were recorded in each case, the readings being as constant as possible to obtain were taken. The zero readings were added or subtracted as indicated by the signs. An R.P.M. Correction to a constant speed 337 R.P.M. was made by multiplying the velocity pressure reading of the pitot tube by the ratio  $\frac{337}{\text{R.P.M.}}$ . This R.P.M. used in the denominator being the observed R.P.M.

We checked the static pressure using high and low speed by squaring the corresponding R.P.M. of the high and low speeds and multiplying the low speed static pressure by the R.P.M. squared of the high speed divided by the R.P.M. squared of the low speed.

CORRECTIONS TO STANDARD CONDITIONS

Test # 1

Test # 2

Length of pipe 23 ft.

Length of pipe 23 ft.

$\frac{1}{2}$  Opening

$\frac{5}{8}$  Opening

No equalizer

No equalizer

Top readings Side readings

Top readings Side readings

	Zero		R.P.M.			Zero		R.P.M.			Zero		R.P.M.	
	Cor.	Cor.	Cor.	Cor.		Cor.	Cor.	Cor.	Cor.		Cor.	Cor.	Cor.	
1	.168	.143	.132	.111	1	.302	.258	.316	.270					
2	.198	.169	.177	.151	2	.292	.249	.388	.331					
3	.221	.188	.193	.164	3	.286	.244	.342	.292					
4	.230	.196	.202	.172	4	.272	.232	.312	.266					
5	.232	.198	.217	.185	5	.277	.236	.302	.258					
6	.173	.147	.232	.197	6	.286	.244	.272	.232					
7	.138	.117	.223	.190	7	.272	.232	.232	.198					
8	.127	.108	.220	.187	8	.247	.210	.197	.168					
9	.126	.107	.202	.172	9	.222	.189	.188	.160					
10	.083	.071	.152	.129	10	.152	.130	.192	.164					

## CORRECTIONS TO STANDARD CONDITIONS

Test # 3

Test # 4

Length of pipe 23 ft.

Length of pipe 23 ft.

3/4 Opening

7/8 Opening

No equalizer

No equalizer

Side readings		Top readings		Top readings		Side readings			
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.		
Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.		
1	.393	.338	.384	.330	1	.511	.458	.416	.374
2	.433	.372	.414	.356	2	.512	.468	.491	.441
3	.464	.399	.374	.321	3	.481	.432	.491	.441
4	.463	.398	.360	.309	4	.471	.423	.501	.450
5	.463	.398	.405	.348	5	.486	.436	.521	.467
6	.374	.321	.412	.354	6	.441	.395	.451	.405
7	.351	.302	.359	.308	7	.391	.351	.411	.369
8	.312	.268	.341	.296	8	.351	.315	.409	.368
9	.343	.295	.289	.248	9	.291	.261	.420	.377
10	.299	.257	.204	.175	10	.231	.208	.310	.278

CORRECTIONS TO STANDARD CONDITIONS

Test # 6

Test # 7

Length of pipe 23 ft.

Length of pipe 23 ft.

$\frac{1}{2}$  Opening

$\frac{5}{8}$  Opening

1 Equalizer

1 Equalizer

Top readings		Side Readings		Top Readings		Side Readings	
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.
Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.
1	.045 .053	.113 .135	1	.110 .131	.082	.098	
2	.045 .053	.133 .159	2	.116 .138	.138	.165	
3	.050 .060	.110 .132	3	.133 .159	.130	.155	
4	.045 .053	.102 .122	4	.138 .165	.120	.143	
5	.049 .059	.104 .125	5	.163 .194	.129	.154	
6	.132 .158	.077 .092	6	.133 .159	.153	.183	
7	.177 .212	.084 .100	7	.152 .182	.178	.212	
8	.181 .216	.112 .134	8	.192 .230	.184	.220	
9	.181 .216	.109 .130	9	.208 .248	.243	.290	
10	.156 .187	.084 .100	10	.153 .183	.171	.204	

CORRECTION TO STANDARD CONDITIONS

Test # 8

Test # 9

Length of pipe 23 ft.

Length of pipe 23 ft.

3/4 Opening

7/8 Opening

1 Equalizer

1 Equalizer

Top Readings Side Readings				Top Readings Side Readings					
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.		
Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.		
1	.104	.1317	.148	.1875	1	.275	.338	.132	.162
2	.116	.1470	.185	.234	2	.323	.397	.132	.162
3	.118	.1492	.203	.257	3	.296	.364	.141	.173
4	.155	.1965	.213	.270	4	.297	.365	.146	.179
5	.162	.2050	.183	.232	5	.234	.288	.184	.226
6	.177	.224	.167	.212	6	.212	.261	.242	.297
7	.184	.233	.173	.219	7	.258	.317	.272	.334
8	.210	.266	.195	.247	8	.295	.363	.289	.355
9	.232	.294	.279	.354	9	.321	.395	.303	.372
10	.163	.206	.255	.323	10	.308	.379	.200	.246

## CORRECTIONS TO STANDARD CONDITIONS

Test # 10

Test # 11

Length of pipe 23 ft.

Length of pipe 23 ft.

 $\frac{1}{2}$  Opening $\frac{5}{8}$  Opening

1 Equalizer

1 Equalizer

Top Readings Side Readings				Top Readings Side Readings					
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.		
Cor.	Cor.	Cor	Cor.	Cor.	Cor.	Cor.	Cor.		
1	.088	.105	.036	.043	1	.073	.093	.117	.150
2	.088	.105	.050	.059	2	.073	.093	.123	.157
3	.100	.119	.066	.078	3	.068	.087	.137	.175
4	.091	.109	.060	.071	4	.080	.102	.111	.142
5	.120	.143	.069	.082	5	.113	.145	.121	.155
6	.050	.059	.124	.148	6	.092	.118	.115	.147
7	.048	.057	.128	.153	7	.106	.136	.106	.136
8	.048	.057	.166	.198	8	.106	.136	.135	.173
9	.036	.043	.150	.179	9	.151	.193	.153	.196
10	.030	.035	.159	.190	10	.085	.109	.191	.245

CORRECTIONS TO STANDARD CONDITIONS

Test # 12

Test # 13

Length of pipe 23 ft.

Length of pipe 23 ft.

3/4 Opening

7/8 Opening

1 Equalizer

1 Equalizer

Test # 12				Test # 13					
Top readings		Side Readings		Top readings		Side Readings			
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.		
Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.		
1	.118	.152	.111	.1432	1	.172	.215	.203	.254
2	.130	.1677	.198	.2560	2	.180	.225	.281	.351
3	.086	.111	.213	.275	3	.118	.147	.273	.341
4	.593	.120	.189	.244	4	.122	.152	.223	.279
5	.125	.161	.206	.266	5	.140	.175	.233	.291
6	.163	.210	.144	.186	6	.215	.269	.191	.239
7	.189	.244	.133	.171	7	.272	.340	.173	.216
8	.173	.224	.177	.229	8	.253	.316	.272	.340
9	.178	.230	.196	.253	9	.259	.324	.355	.443
10	.106	.137	.245	.316	10	.165	.206	.394	.492



## CORRECTIONS TO STANDARD CONDITIONS

Test # 14

Test # 15

Length of pipe 23 ft.

Length of pipe 23 ft.

 $\frac{1}{2}$  Opening $\frac{5}{8}$  Opening

2 Equalizers

2 Equalizers

Top Readings Side teadings				Top readings Side readings					
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.		
Cor.	Cor.	Cor.	Cor.	Cor.	Cor	Cor.	Cor.		
1	.072	.064	.227	.202	1	.190	.226	.178	.212
2	.082	.073	.201	.178	2	.203	.242	.126	.150
3	.087	.077	.219	.194	3	.230	.274	.148	.176
4	.100	.089	.219	.194	4	.273	.325	.172	.205
5	.102	.097	.191	.170	5	.275	.326	.198	.236
c	.173	.154	.149	.132	c	.220	.262	.218	.260
6	.250	.222	.118	.105	6	.228	.272	.248	.296
7	.256	.227	.118	.105	7	.302	.361	.216	.258
8	.261	.232	.163	.145	8	.300	.358	.268	.320
9	.245	.218	.138	.123	9	.303	.361	.230	.274
10	.124	.110	.082	.073	10	.250	.298	.150	.179

CORRECTIONS TO STANDARD CONDITIONS

Test # 16

Test # 17

Length of pipe 23 ft.

Length of pipe 23 ft.

3/4 Opening

7/8 Opening

2 Equalizers

2 Equalizers

Top readings Side readings

Top readings Side readings

Zero R.P.M.

Zero R.P.M.

Zero R.P.M.

Zero R.P.M.

Cor. Cor.

Cor. Cor.

Cor. Cor.

Cor. Cor.

1	.308	.265	.155	.1336	1	.350	.314	.230	.207
2	.335	.289	.145	.1250	2	.388	.349	.193	.173
3	.313	.270	.166	.143	3	.381	.342	.237	.213
4	.373	.321	.184	.1587	4	.444	.399	.252	.226
5	.360	.310	.227	.196	5	.426	.382	.275	.247
c	.271	.234	.269	.232	c	.318	.286	.313	.281
6	.253	.218	.355	.306	6	.333	.299	.413	.371
7	.275	.237	.321	.277	7	.339	.305	.401	.360
8	.383	.330	.411	.354	8	.448	.402	.478	.430
9	.411	.354	.340	.293	9	.544	.489	.419	.376
10	.298	.257	.225	.194	10	.460	.413	.280	.251

CORRECTIONS TO STANDARD CONDITIONS

Test # 18

Test # 19

Length of pipe 14 ft. 2in.

Length of pipe 14 ft. 2In.

$\frac{1}{2}$  Opening

$\frac{5}{8}$  Opening

No Equalizer

No Equalizer

Test # 18				Test # 19					
Top readings		Side readings		Top readings		Side readings			
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.		
Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.		
1	.076	.092	.065	.079	1	.091	.109	.082	.096
2	.090	.184	.080	.097	2	.095	.114	.123	.149
3	.107	.129	.086	.138	3	.096	.116	.139	.168
4	.118	.143	.099	.119	4	.103	.124	.138	.166
5	.130	.157	.109	.132	5	.131	.158	.142	.172
6	.068	.082	.142	.172	6	.117	.141	.140	.169
7	.050	.060	.163	.192	7	.112	.135	.141	.170
8	.050	.060	.160	.194	8	.110	.133	.160	.193
9	.050	.060	.168	.203	9	.087	.105	.200	.242
10	.025	.030	.132	.160	10	.087	.185	.212	.256

CORRECTIONS TO STANDARD CONDITIONS

Test # 20

Test # 21

Length of pipe 14' 2"

Length of pipe 14' 2"

3/4 Opening

7/8 Opening

No equalizer

No equalizer

Top readings Side readings Top readings Side readings

	Zero R.P.M. Cor. Cor.		Zero R.P.M. Cor. Cor.		Zero R.P.M. Cor. Cor.		Zero R.P.M. Cor. Cor.		
1	.172	.207	.076	.092	1	.278	.336	.130	.157
2	.145	.175	.120	.145	2	.203	.245	.129	.156
3	.132	.159	.130	.156	3	.195	.236	.150	.181
4	.140	.169	.174	.210	4	.173	.209	.170	.206
5	.179	.216	.195	.235	5	.232	.281	.251	.303
6	.219	.264	.192	.231	6	.297	.359	.242	.293
7	.223	.268	.185	.223	7	.302	.365	.271	.327
8	.220	.265	.214	.258	8	.293	.354	.300	.363
9	.200	.241	.248	.298	9	.289	.349	.307	.371
10	.130	.156	.272	.328	10	.152	.184	.280	.338

CORRECTIONS TO STANDARD CONDITIONS

Test # 22

Test # 23

Length of pipe 14 ft. 2 In

Length of pipe 14 ft. 2 In.

$\frac{1}{2}$  Opening

$\frac{5}{8}$  Opening

1 Equalizer

1 Equalizer

Top readings				Side readings				Top readings				Side readings			
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.
Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.
1	.056	.048	.146	.126	1	.207	.178	.125	.107						
2	.065	.056	.219	.190	2	.245	.210	.184	.158						
3	.053	.046	.216	.187	3	.262	.224	.184	.158						
4	.047	.040	.176	.152	4	.298	.256	.229	.197						
5	.059	.051	.141	.122	5	.257	.220	.232	.199						
c	.147	.127	.076	.065	c	.248	.212	.253	.217						
6	.205	.178	.030	.026	6	.265	.227	.224	.192						
7	.268	.232	.029	.025	7	.235	.202	.190	.163						
8	.297	.257	.056	.048	8	.270	.232	.207	.178						
9	.269	.232	.076	.065	9	.302	.259	.267	.229						
10	.231	.200	.276	.065	10	.252	.216	.222	.190						

## CORRECTIONS TO STANDARD CONDITIONS

Test # 24

Test # 25

Length of pipe 14 ft. 2 In. Length of pipe 14 ft. 2 In.

3/4 Opening

7/8 Opening

1 Equalizer

1 Equalizer

Top readings Side readings Top readings Side readings

	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.		Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.
1	.327	.282	.120	.103	1	.450	.391	.149	.129
2	.420	.362	.149	.229	2	.532	.462	.164	.142
3	.429	.371	.170	.147	3	.501	.435	.179	.156
4	.406	.350	.177	.153	4	.493	.427	.207	.180
5	.347	.299	.204	.176	5	.370	.322	.242	.210
c	.254	.219	.329	.284	c	.274	.248	.334	.290
6	.212	.183	.404	.348	6	.270	.234	.457	.397
7	.207	.178	.353	.304	7	.372	.322	.504	.438
8	.267	.230	.327	.282	8	.479	.416	.495	.430
9	.311	.268	.330	.385	9	.613	.532	.487	.423
10	.333	.287	.339	.292	10	.564	.490	.507	.440

## CORRECTIONS TO STANDARD CONDITIONS

Test # 26

Test # 27

Length of pipe 14 ft. 2 In

Length of pipe 14 ft. 2 In.

 $\frac{1}{2}$  Opening $\frac{5}{8}$  Opening

2 Equalizers

2 Equalizers

Top readings				Side readings				Top Readings				Side Readings			
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.
Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.
1	.100	.084	.291	.244	1	.174	.152	.236	.207						
2	.092	.077	.343	.288	2	.199	.174	.303	.266						
3	.073	.061	.282	.236	3	.191	.168	.263	.230						
4	.060	.050	.246	.206	4	.279	.245	.291	.255						
5	.048	.040	.122	.102	5	.329	.289	.293	.256						
c	.090	.075	.046	.038	c	.379	.333	.299	.262						
6	.143	.120	.033	.027	6	.247	.217	.188	.165						
7	.251	.210	.070	.059	7	.267	.235	.159	.139						
8	.250	.210	.115	.096	8	.149	.131	.184	.161						
9	.261	.218	.183	.153	9	.191	.168	.127	.111						
10	.231	.193	.170	.143	10	.127	.112	.219	.192						

CORRECTIONS TO STANDARD CONDITIONS

Test # 28

Test # 29

Length of pipe 14 ft. 2 In. Length of pipe 14 ft. 2 In.

3/4 Opening

7/8 Opening

2 Equalizers

2 Equalizers

Top readings		Side readings		Top readings		Side readings	
Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.
1 .310	.270	.458	.399	1 .436	.378	.466	.404
2 .379	.330	.413	.360	2 .579	.502	.442	.384
3 .341	.297	.349	.304	3 .513	.447	.327	.284
4 .429	.374	.253	.220	4 .625	.543	.280	.243
5 .381	.332	.247	.215	5 .457	.396	.258	.224
c .341	.297	.451	.392	c .490	.426	.587	.510
6 .191	.166	.392	.341	6 .350	.304	.548	.477
7 .192	.167	.287	.250	7 .303	.263	.427	.371
8 .125	.109	.305	.265	8 .205	.178	.385	.335
9 .140	.122	.322	.280	9 .216	.187	.408	.355
10 .122	.106	.293	.255	10 .165	.143	.400	.348



## CORRECTIONS TO STANDARD CONDITIONS

Test # 30

Test # 31

Lenth of pipe 14' 2"

Length of pipe 14' 2"

 $\frac{1}{2}$  Opening $\frac{5}{8}$  Opening

No Equalizer

No Equalizer

Top readings Side readings Top readings Side readings

Zero R.P.M. Zero R.P.M. Zero R.P.M. Zero R.P.M.

Cor. Cor. Cor. Cor. Cor. Cor. Cor. Cor.

1	.126	.103	.152	.240	1	.155	.129	.310	.258
2	.153	.125	.206	.169	2	.105	.087	.331	.274
3	.186	.152	.224	.184	3	.141	.117	.287	.238
4	.202	.166	.250	.205	4	.196	.163	.266	.221
5	.235	.193	.285	.234	5	.253	.210	.280	.232
c	.280	.230	.256	.210	c	.293	.243	.280	.232
6	.286	.234	.166	.136	6	.296	.246	.250	.208
7	.304	.250	.133	.109	7	.313	.260	.240	.199
8	.324	.266	.140	.115	8	.373	.310	.230	.191
9	.326	.268	.116	.095	9	.415	.344	.230	.191
10	.236	.194	.100	.082	10	.448	.372	.200	.166

CORRECTIONS TO STANDARD CONDITIONS

Test # 32

Test # 33

Length of pipe 14' 2"

Length of pipe 14' 2"

3/4 Opening

7/8 Opening

No Equalizer

No Equalizer

Top readings Side readings				Top readings Side readings					
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.		
Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.		
1	.195	.162	.381	.316	1	.215	.181	.490	.412
2	.141	.117	.366	.304	2	.216	.182	.504	.424
3	.169	.140	.286	.237	3	.235	.198	.446	.376
4	.220	.182	.267	.221	4	.272	.229	.380	.320
5	.311	.258	.313	.260	5	.386	.325	.404	.340
c	.410	.340	.363	.301	c	.486	.410	.448	.378
6	.399	.331	.408	.339	6	.496	.418	.506	.426
7	.411	.341	.387	.321	7	.536	.452	.458	.386
8	.466	.387	.357	.296	8	.624	.525	.374	.314
9	.541	.449	.316	.262	9	.649	.546	.345	.290
10	.561	.465	.271	.225	10	.510	.430	.208	.175

## CORRECTIONS TO STANDARD CONDITIONS

Test # 34

Test # 35b

Length of pipe 14' 2"

Length of pipe 14' 2"

1/2 Opening

5/8 Opening

One Equalizer 2' 3" out

One equalizer 2' 3" out

	Top readings		Side readings			Top readings		Side readings	
	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.		Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.
1	.071	.058	.196	.160	1	.140	.115	.116	.095
2	.082	.066	.233	.190	2	.176	.145	.136	.102
3	.073	.059	.243	.198	3	.169	.140	.168	.139
4	.061	.050	.213	.173	4	.188	.155	.188	.155
5	.052	.042	.173	.141	5	.206	.170	.188	.155
c	.106	.086	.132	.107	6	.276	.224	.286	.236
6	.203	.165	.077	.063	6	.256	.212	.265	.219
7	.263	.214	.103	.084	7	.256	.212	.258	.213
8	.285	.232	.153	.124	8	.266	.220	.268	.222
9	.282	.230	.193	.157	9	.310	.256	.295	.244
10	.243	.198	.175	.142	10	.300	.448	.286	.236

CORRECTIONS TO STANDARD CONDITIONS

Test # 35a

Length of pipe 14' 2"

5/8 Opening

One equalizer 2' 3" out 45

	Top readings		Side readings	
	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.
1	.065	.220	.114	.195
2	.273	.227	.148	.123
3	.269	.224	.163	.136
4	.283	.235	.166	.138
5	.271	.225	.195	.162
c	.233	.194	.275	.229
6	.203	.169	.265	.220
7	.153	.127	.285	.237
8	.151	.126	.265	.220
9	.163	.136	.295	.246
10	.121	.101	.285	.237

CORRECTIONS TO STANDARD CONDITIONS

Test # 36

Test # 37

Length of pipe 14' 2"

Length of pipe 14' 2"

3/4 Opening

7/8 Opening

One equalizer 2' 3" out

One equalizer 2' 3" out

Top readings		Side readings		Top Readings		Side readings	
Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.
1 .382	.320	.169	.142	1 .549	.465	.198	.168
2 .422	.363	.199	.165	2 .573	.486	.217	.184
3 .392	.328	.180	.151	3 .603	.512	.217	.184
4 .422	.353	.159	.133	4 .583	.495	.193	.164
5 .362	.303	.159	.133	5 .423	.360	.228	.193
c .332	.378	.263	.220	c .357	.303	.357	.303
6 .272	.228	.377	.316	6 .372	.316	.489	.415
7 .256	.214	.401	.336	7 .387	.328	.488	.414
8 .312	.262	.373	.312	8 .452	.384	.511	.434
9 .312	.262	.418	.350	9 .468	.398	.511	.434
10 .222	.186	.419	.351	10 .384	.326	.527	.447

CORRECTIONS TO STANDARD CONDITIONS

Test # 38

Test # 39

Length of pipe 14' 2"

Length of pipe 14' 2"

1/2 Opening

5/8 Opening

One equalizer 6' 7" out

One equalizer 6' 7" out

Top readings				Side readings				Top readings				Side readings			
Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.	Zero	R.P.M.		
Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.	Cor.		
1	.110	.094	.187	.154	1	.159	.134	.269	.227						
2	.118	.097	.240	.198	2	.190	.160	.269	.227						
3	.137	.113	.221	.182	3	.200	.169	.225	.190						
4	.155	.128	.219	.180	4	.207	.174	.181	.153						
5	.168	.138	.229	.189	5	.229	.183	.205	.173						
c	.267	.220	.219	.180	c	.215	.181	.205	.173						
6	.248	.204	.087	.072	6	.284	.239	.229	.193						
7	.328	.270	.071	.059	7	.308	.260	.177	.149						
8	.280	.231	.058	.048	8	.315	.265	.181	.152						
9	.329	.271	.058	.048	9	.355	.315	.170	.143						
10	.267	.220	.058	.048	10	.319	.268	.184	.155						

## CORRECTIONS TO STANDARD CONDITIONS

Test # 40

Test # 41

Length of pipe 14' 2"

Length of pipe 14' 2"

3/4 Opening

7/8 Opening

One equalizer 6' 7" out

One equalizer 6' 7" out

Top readings Side readings Top readings Side readings

	Zero Cor	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.		Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.
1	.168	.144	.380	.325	1	.202	.179	.548	.486
2	.198	.169	.350	.300	2	.258	.229	.529	.469
3	.205	.175	.311	.266	3	.240	.213	.423	.375
4	.217	.186	.236	.202	4	.248	.220	.277	.246
5	.303	.259	.229	.197	5	.316	.280	.263	.233
c	.265	.226	.279	.239	c	.285	.252	.299	.265
6	.278	.238	.341	.292	6	.401	.356	.356	.316
7	.368	.315	.312	.267	7	.445	.394	.424	.376
8	.378	.324	.350	.300	8	.441	.391	.459	.407
9	.498	.426	.309	.264	9	.551	.488	.437	.387
10	.458	.392	.356	.304	10	.485	.430	.469	.415

CORRECTIONS TO STANDARD CONDITIONS

Test # 42

Test # 43

Length of pipe 14' 2"

Length of pipe 14' 2"

1/2 Opening

5/8 Opening

Two equalizers 2' 3" & 6' 7" out

Top readings		Side readings		Top readings		Side readings	
Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.
1 .082	.068	.200	.166	1 .143	.122	.170	.145
2 .089	.074	.260	.216	2 .249	.212	.215	.183
3 .066	.055	.171	.142	3 .204	.178	.165	.141
4 .035	.029	.239	.198	4 .251	.214	.192	.164
5 .041	.034	.181	.150	5 .303	.268	.250	.213
c .132	.109	.130	.108	c .285	.243	.350	.298
6 .162	.134	.083	.069	6 .314	.268	.278	.236
7 .212	.176	.070	.058	7 .208	.178	.200	.171
8 .302	.250	.170	.141	8 .254	.266	.268	.228
9 .315	.261	.173	.143	9 .321	.274	.262	.224
10 .182	.151	.246	.204	10 .205	.175	.316	.270



CORRECTIONS TO STANDARD CONDITIONS

Test # 44

Test # 45

Length of pipe 14' 2"

Length of pipe 14' 2"

3/4 Opening

7/8 Opening

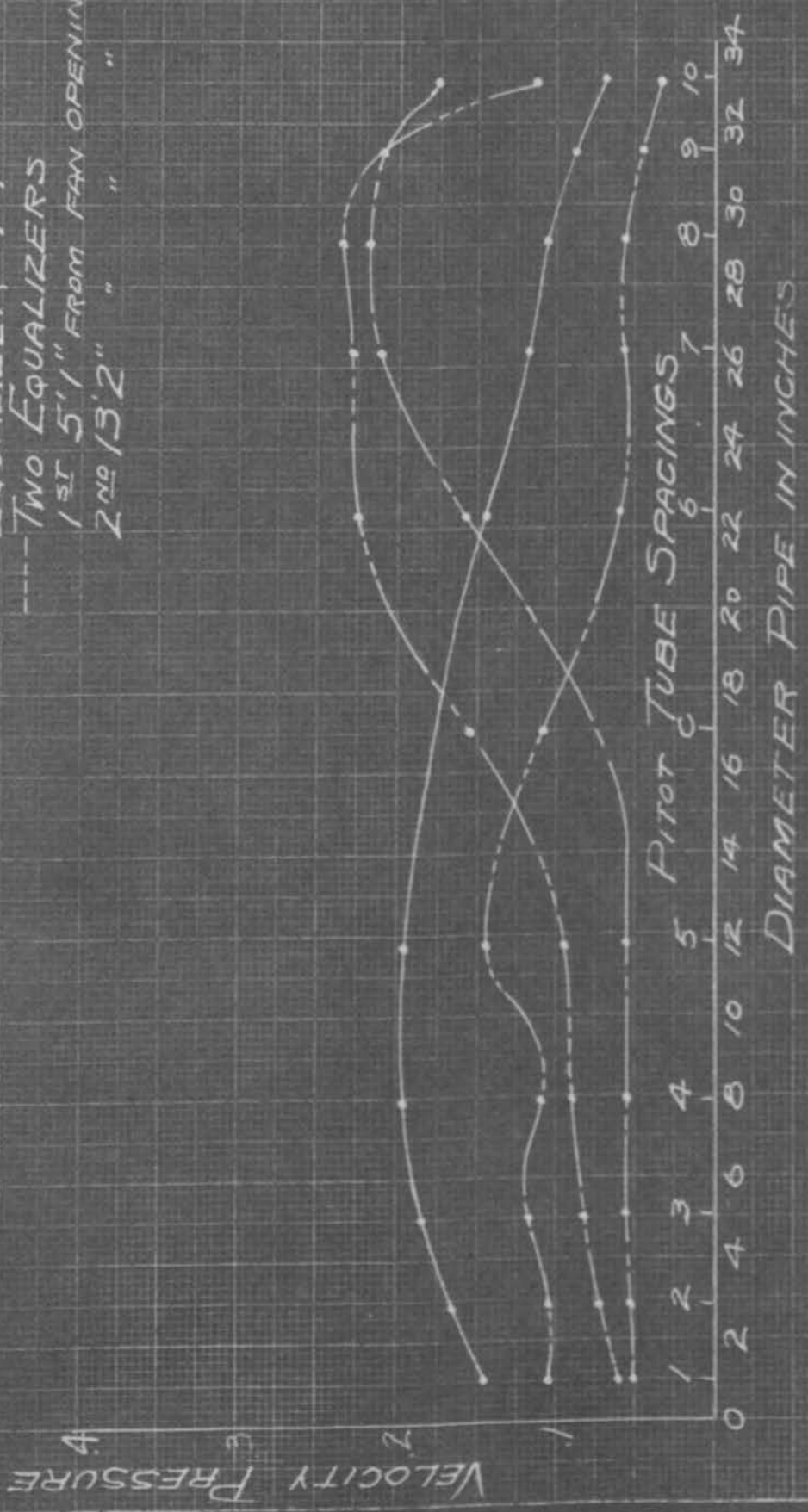
Two equalizers 2' 3" and 6' 7" from fan openings

Top readings Side readings Top readings Side readings

	Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.		Zero Cor.	R.P.M. Cor.	Zero Cor.	R.P.M. Cor.
1	.355	.300	.233	.197	1	.438	.380	.229	.198
2	.413	.349	.273	.231	2	.584	.505	.538	.206
3	.323	.273	.223	.188	3	.518	.450	.158	.234
4	.393	.332	.143	.121	4	.538	.467	.149	.129
5	.413	.249	.153	.129	5	.450	.390	.196	.170
c	.263	.220	.303	.256	c	.330	.286	.408	.354
6	.283	.239	.360	.304	6	.258	.224	.438	.380
7	.238	.201	.278	.334	7	.288	.250	.348	.302
8	.293	.248	.413	.349	8	.413	.358	.489	.424
9	.421	.356	.403	.340	9	.520	.451	.443	.384
10	.323	.273	.443	.374	10	.367	.318	.528	.458

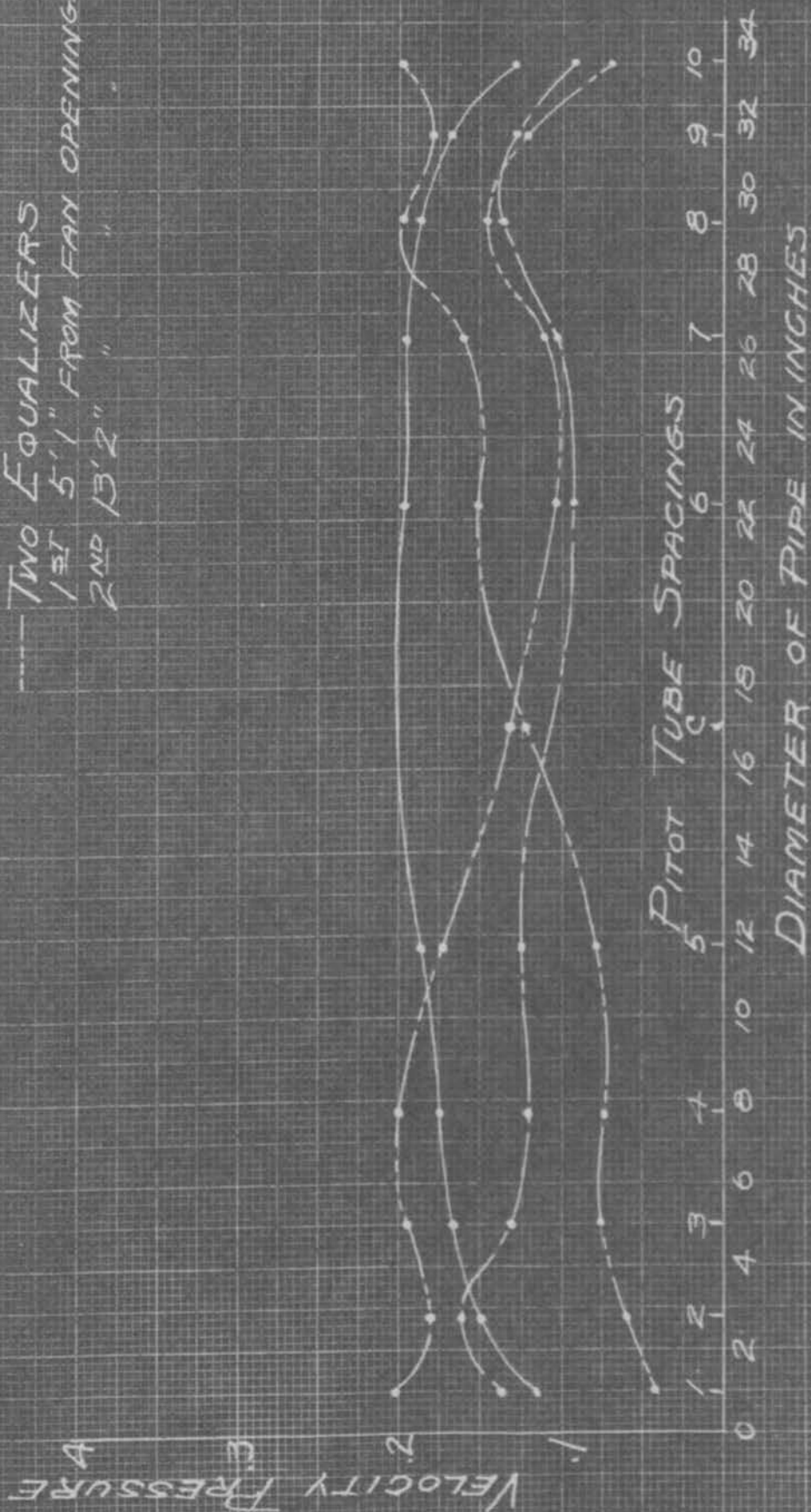
FULL LENGTH  
 1/2 OPENING.  
 TOP READINGS

— NO EQUALIZER  
 - - - EQUALIZER 5'1" OUT  
 - - - - - EQUALIZER 7'1" "  
 - - - - - TWO EQUALIZERS  
 1<sup>ST</sup> 5'1" FROM FAN OPENING  
 2<sup>ND</sup> 13'2" " "



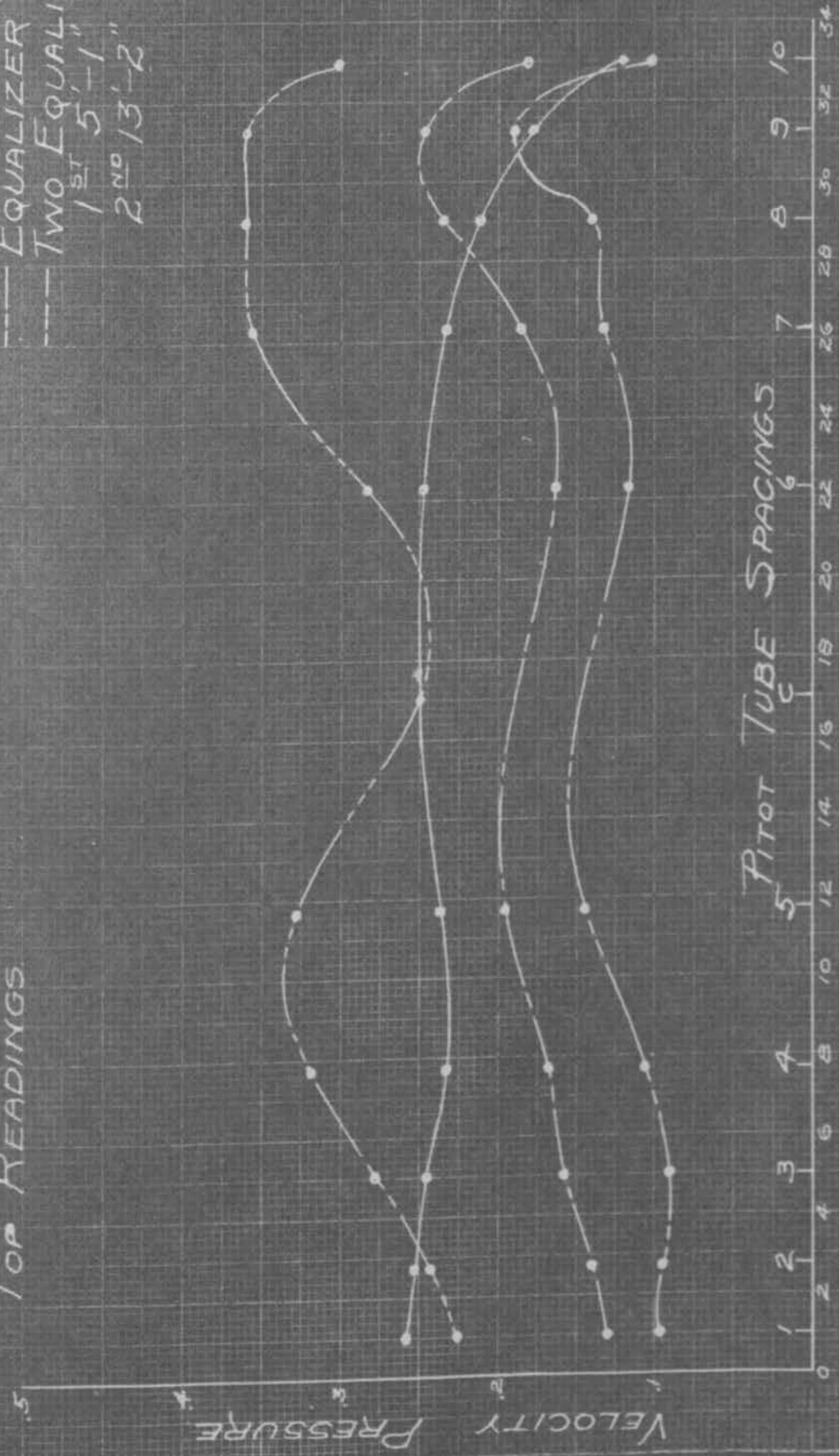
FULL LENGTH  
 1/2 OPENING  
 SIDE READINGS

— NO EQUALIZER  
 - - - EQUALIZER 5'1" OUT FROM FAN  
 - - - - - EQUALIZER 7'1" " "  
 - - - - - TWO EQUALIZERS  
 1ST 5'1" FROM FAN OPENING  
 2ND 13'2" "



——— NO EQUALIZER  
 - - - - - EQUALIZER 5'-1"  
 - - - - - EQUALIZER 7'-1"  
 - - - - - TWO EQUALIZERS  
           1<sup>ST</sup> 5'-1"  
           2<sup>ND</sup> 13'-2"

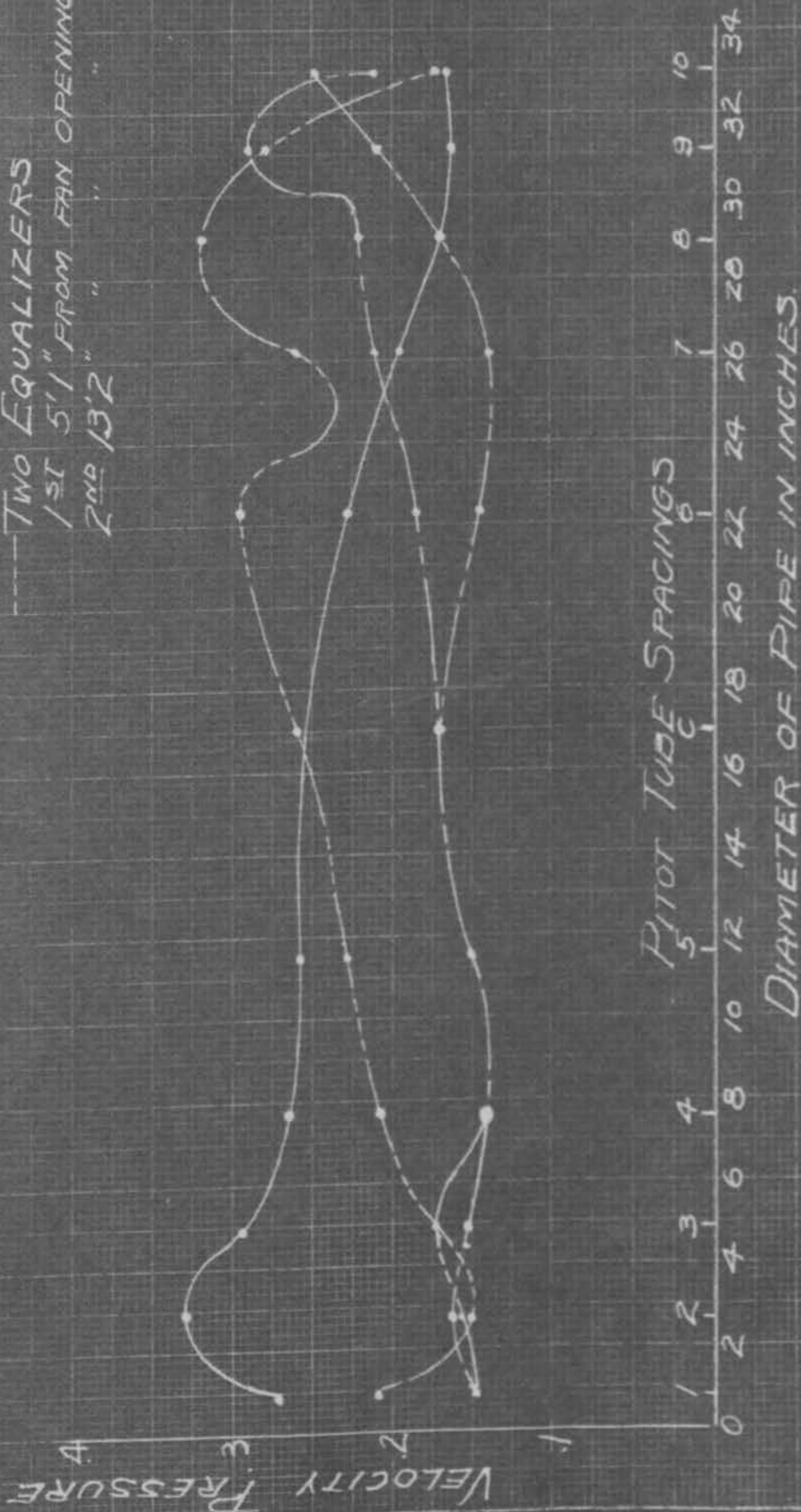
FULL LENGTH  
 5/8 OPENING  
 TOP READINGS



PITOT TUBE SPACINGS  
 5 6 7  
 DIAMETER OF PIPE IN INCHES

FULL LENGTH  
5/8 OPENING  
SIDE READINGS

— NO EQUALIZER  
 - - - EQUALIZER 5'1" OUT  
 - - - EQUALIZER 7'1" "  
 - - - TWO EQUALIZERS  
   1<sup>ST</sup> 5'1" FROM FAN OPENING  
   2<sup>ND</sup> 13'2" "



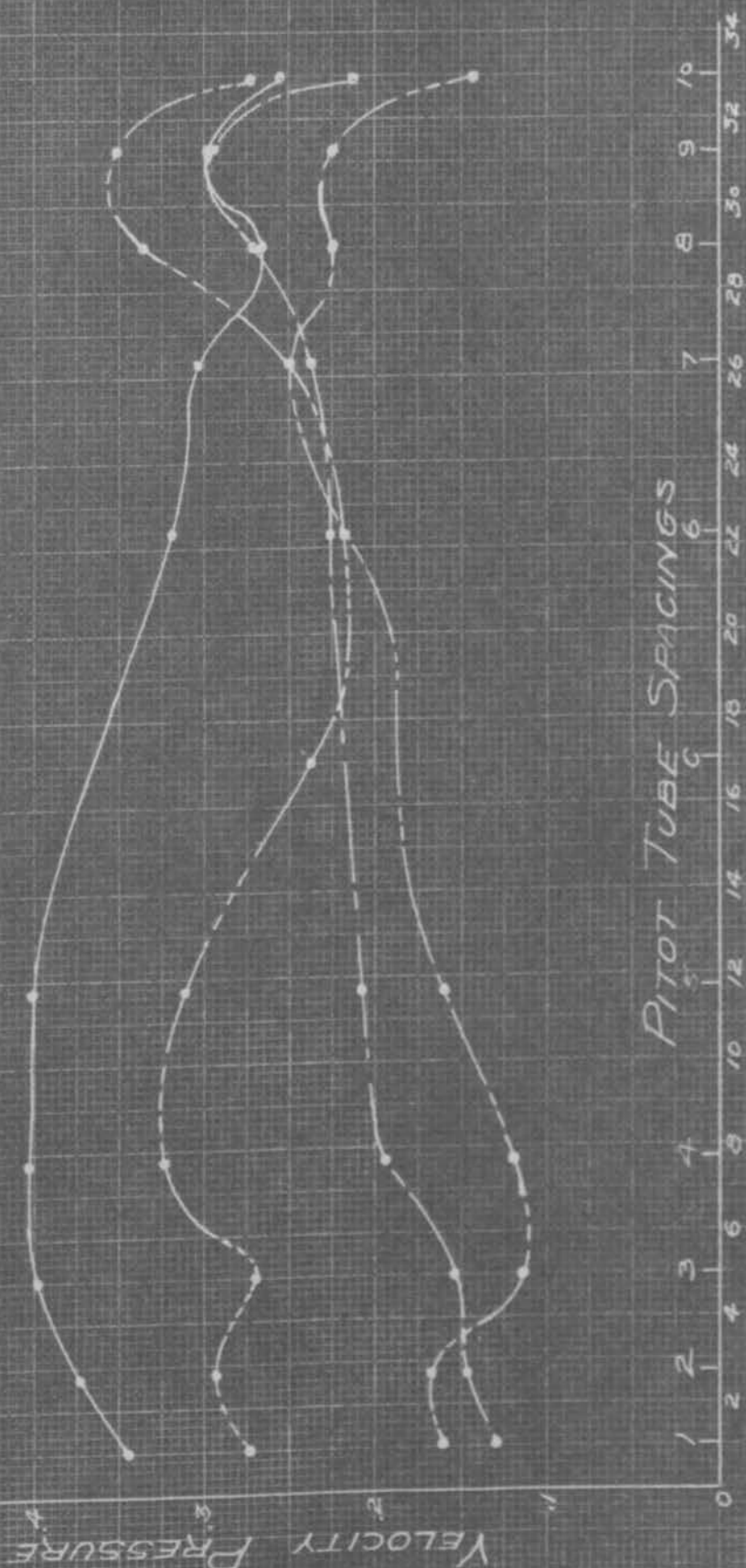
PITOT TUBE SPACINGS

0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34

DIAMETER OF PIPE IN INCHES.

——— NO EQUALIZER  
 - - - - - EQUALIZER 5'-1"  
 - - - - - EQUALIZER 7'-1"  
 - - - - - TWO EQUALIZERS  
           1<sup>ST</sup> 5'-1"  
           2<sup>ND</sup> 13'-2"

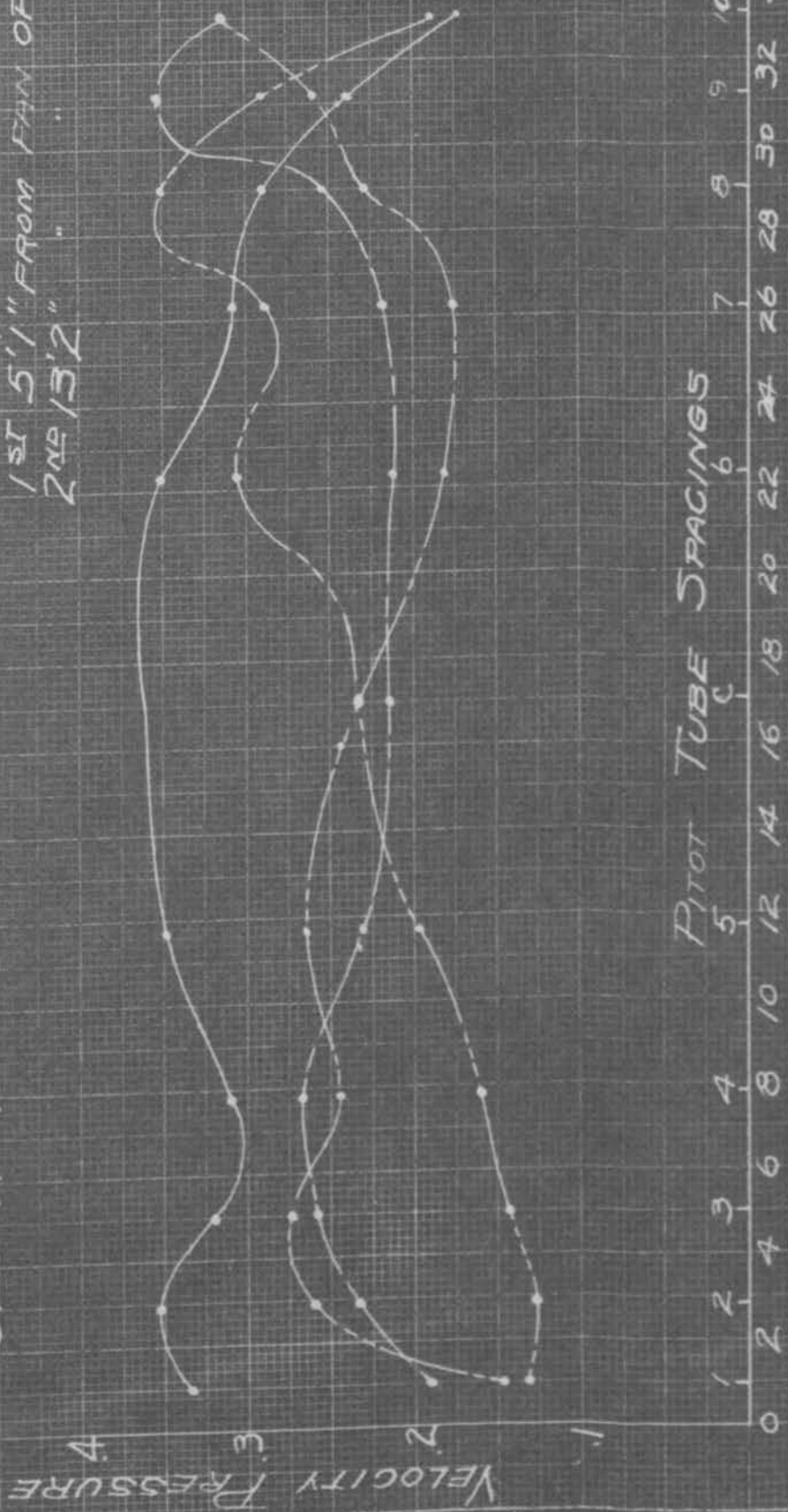
FULL LENGTH  
 3/4 OPENING  
 5 TOP READINGS



PITOT TUBE SPACINGS  
 DIAMETER OF PIPE IN INCHES

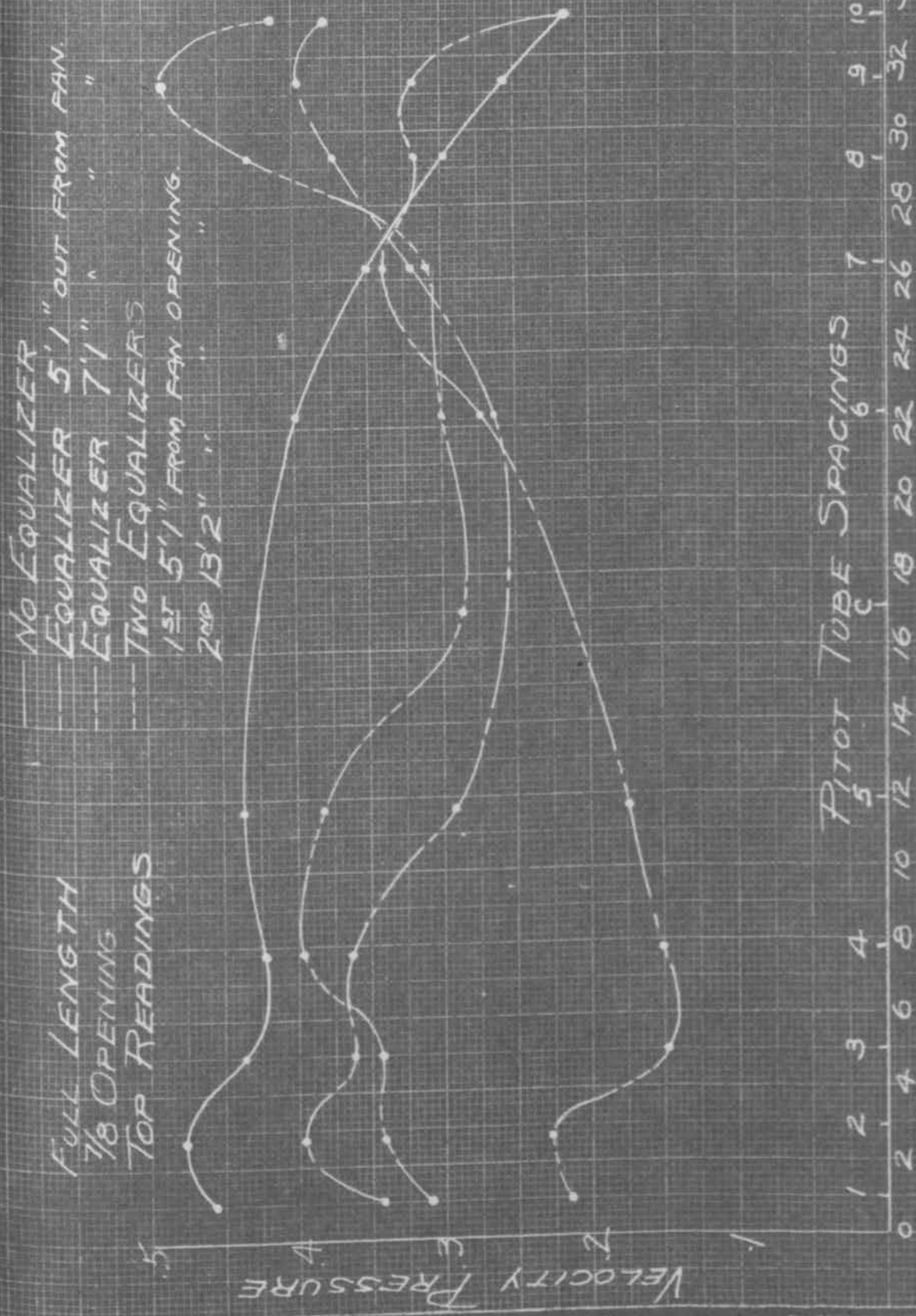
FULL LENGTH  
3/4 OPENING  
SIDE READINGS

--- NO EQUALIZER  
 --- EQUALIZER 5'1" OUT  
 --- EQUALIZER 7'1" "  
 --- TWO EQUALIZERS  
 1<sup>ST</sup> 5'1" FROM FAN OPENING  
 2<sup>ND</sup> 13'2"



PITOT TUBE SPACINGS

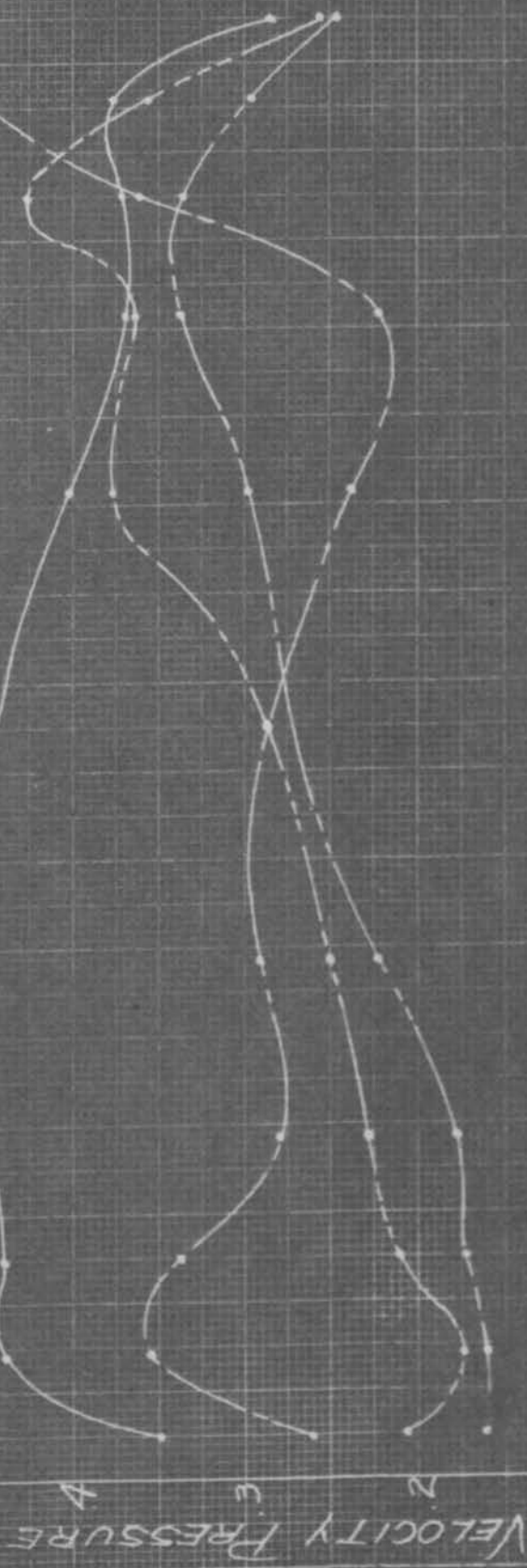
DIAMETER OF PIPE IN INCHES





- No EQUALIZER
- - - EQUALIZER 5'1" OUT FROM FAN
- EQUALIZER 7'1" " "
- Two EQUALIZERS
- 1st 5'1" FROM FAN OPENING
- 2nd 13'2" " "

FULL LENGTH  
1/8 OPENING  
5 SIDE READINGS



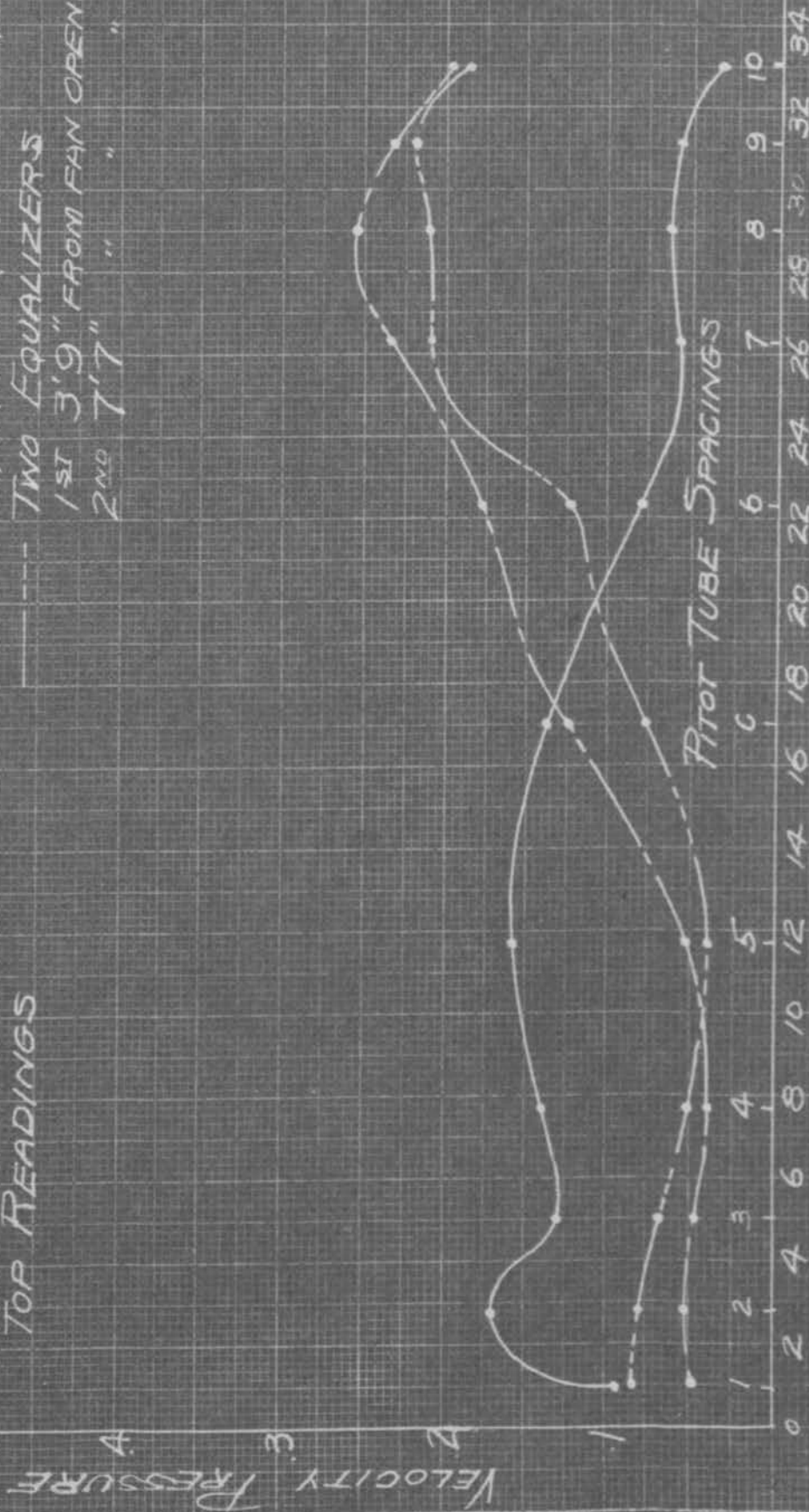
PITOT TUBE SPACINGS

1 2 3 4 5 6 7 8 9 10  
0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34

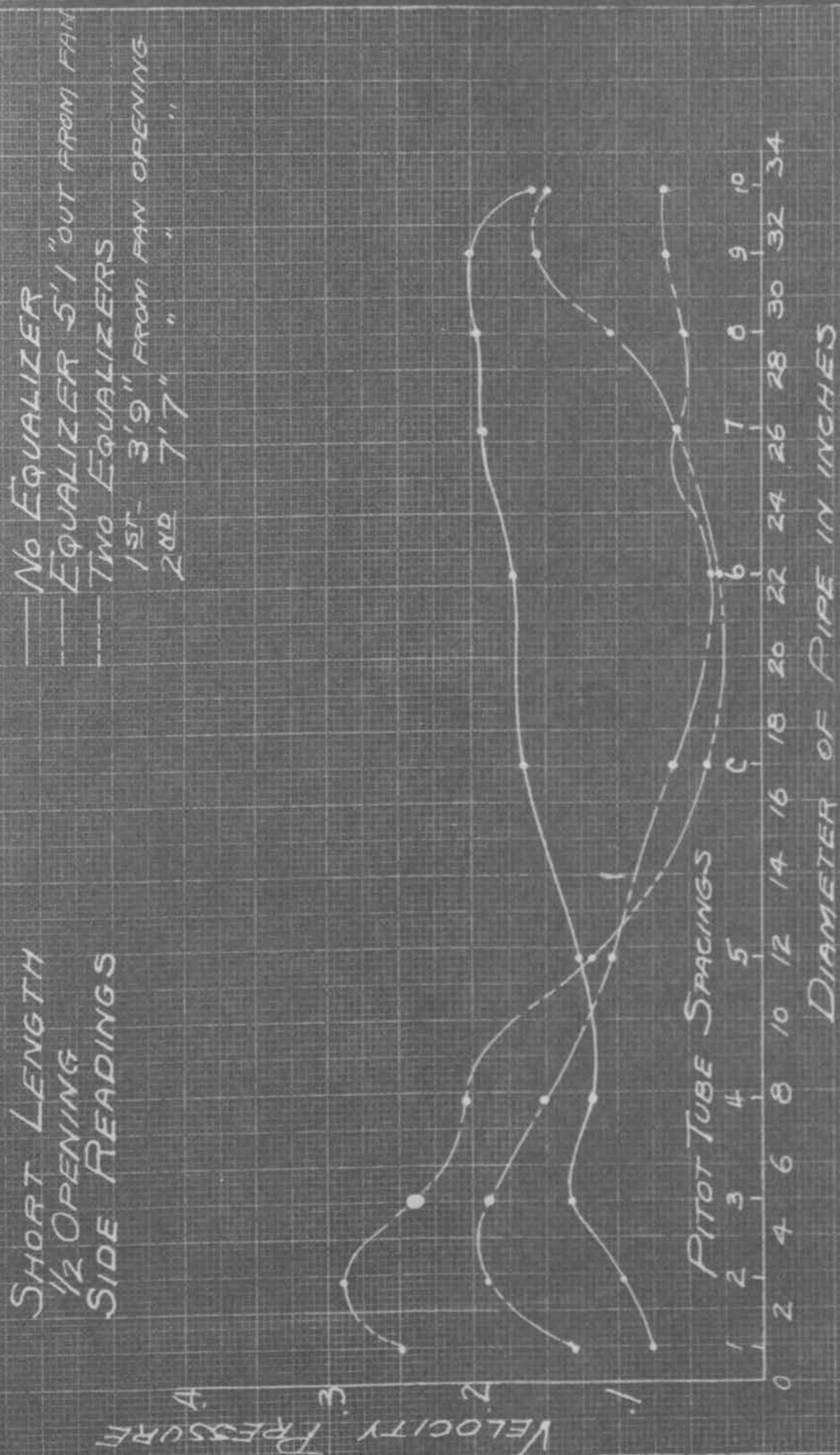
DIAMETER OF PIPE IN INCHES

--- NO EQUALIZER  
 --- EQUALIZER 5'1" OUT FROM FAN  
 --- TWO EQUALIZERS  
   1ST 3'9" FROM FAN OPENING  
   2ND 7'7" "

SHORT LENGTH  
 1/2 OPENING  
 TOP READINGS

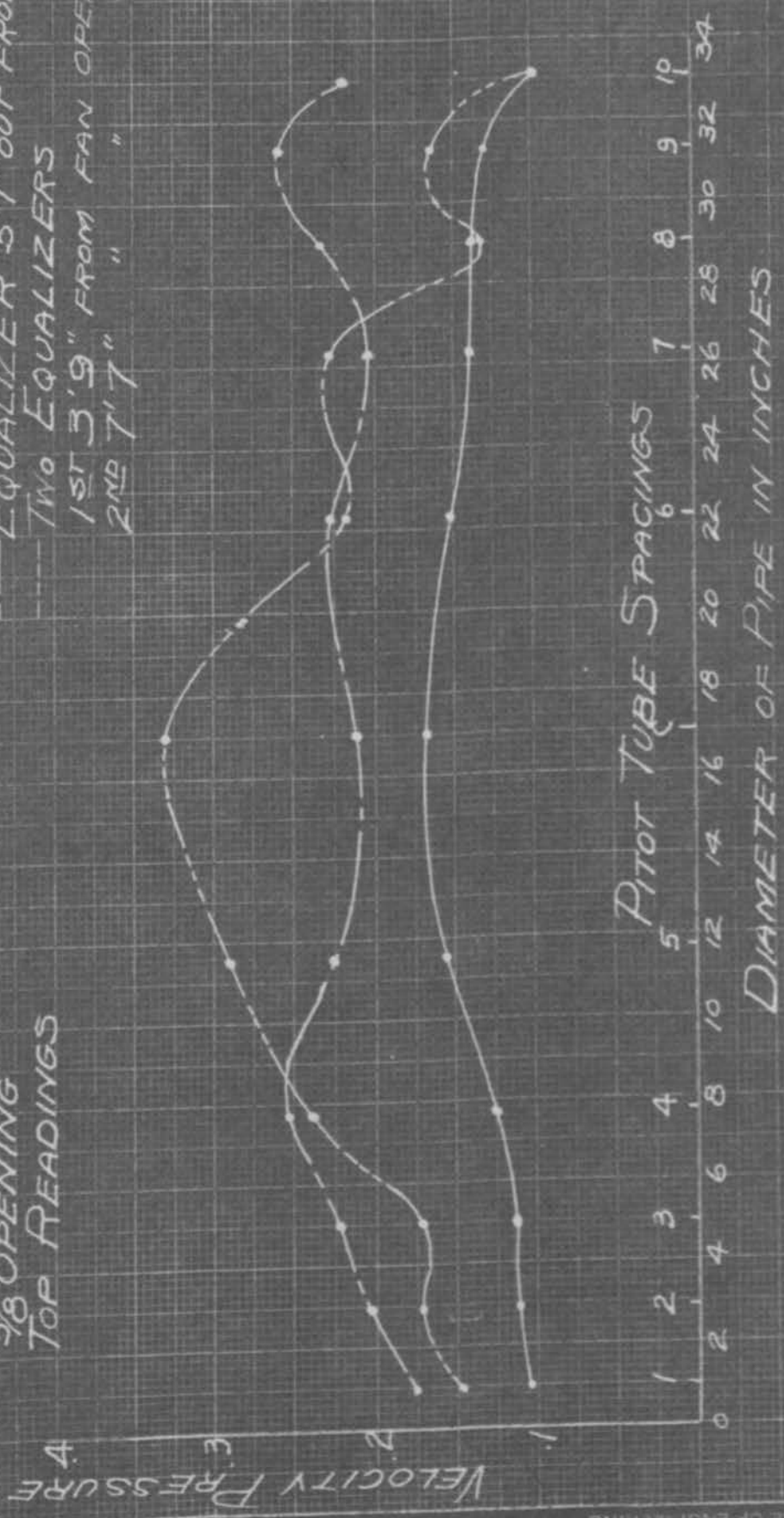


DIAMETER OF PIPE IN INCHES.



--- No EQUALIZER  
 --- EQUALIZER 5'1" OUT FROM FAN  
 --- Two EQUALIZERS  
 1st 3'9" FROM FAN OPENING  
 2nd 7'7" " "

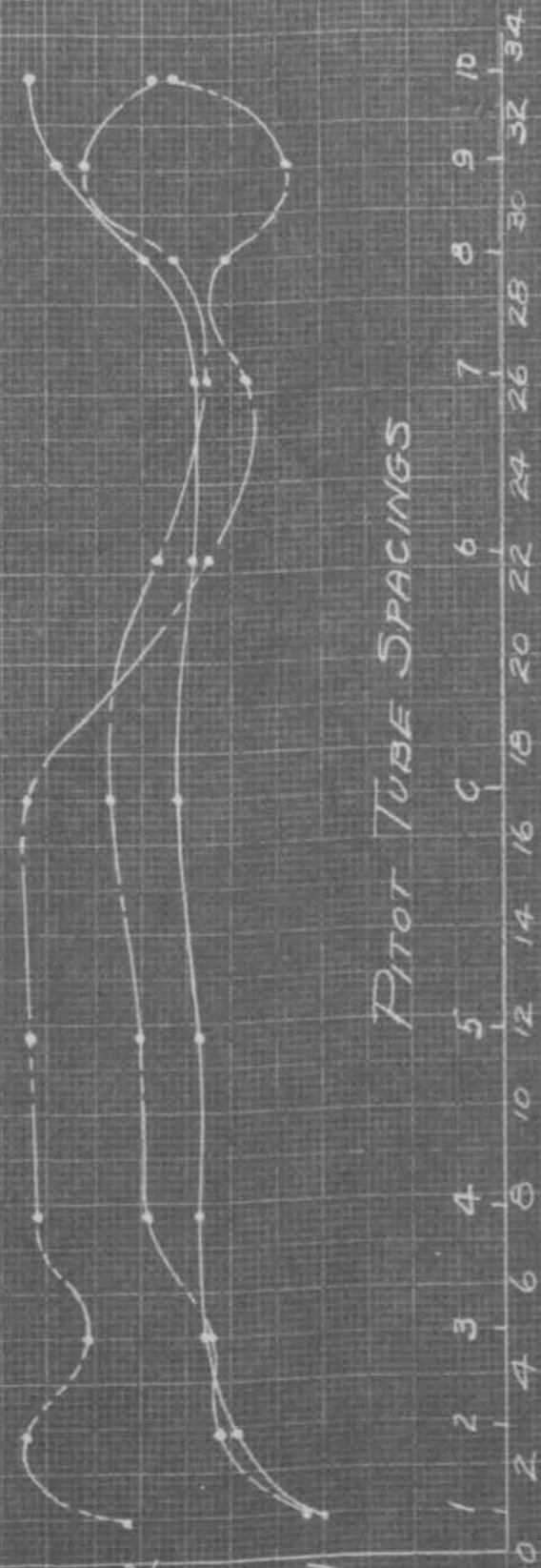
SHORT LENGTH  
 5/8 OPENING  
 TOP READINGS



SHORT LENGTH  
5/8 OPENING  
SIDE READINGS

— No EQUALIZER  
- - - EQUALIZER 5'1" OUT FROM FAN  
- · - · - Two EQUALIZERS  
1<sup>ST</sup> 3'9" FROM FAN OPENING  
2<sup>ND</sup> 7'7" "

VELOCITY PRESSURE

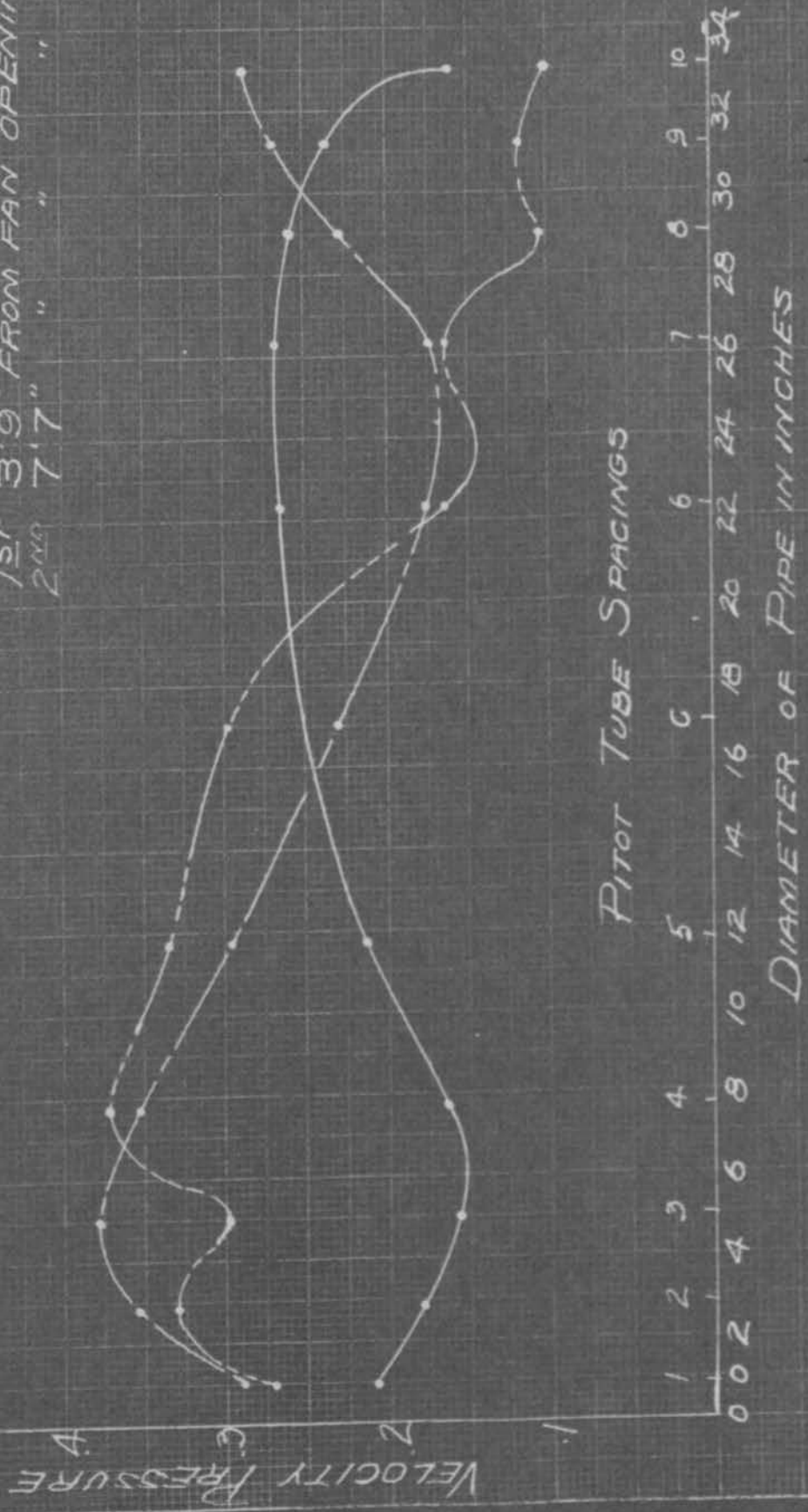


PITOT TUBE SPACINGS

DIAMETER OF PIPE IN INCHES

——— No EQUALIZER  
 - - - - - EQUALIZER 5'1" OUT FROM FAN  
 - - - - - TWO EQUALIZERS  
 1ST 3'9" FROM FAN OPENING  
 2ND 7'7" " "

SHORT LENGTH  
 3/4 OPENING  
 TOP READINGS

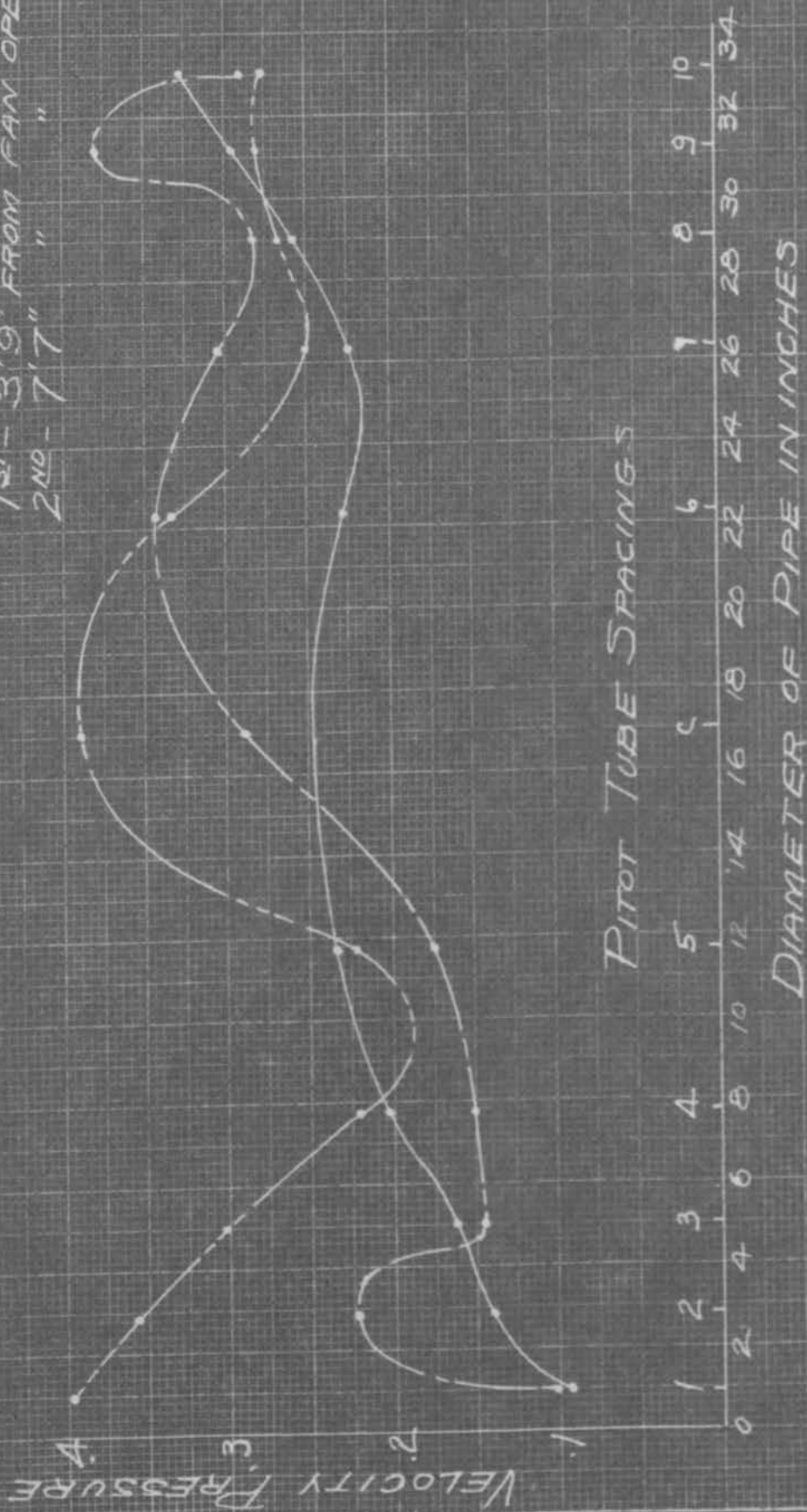


PITOT TUBE SPACINGS

DIAMETER OF PIPE IN INCHES

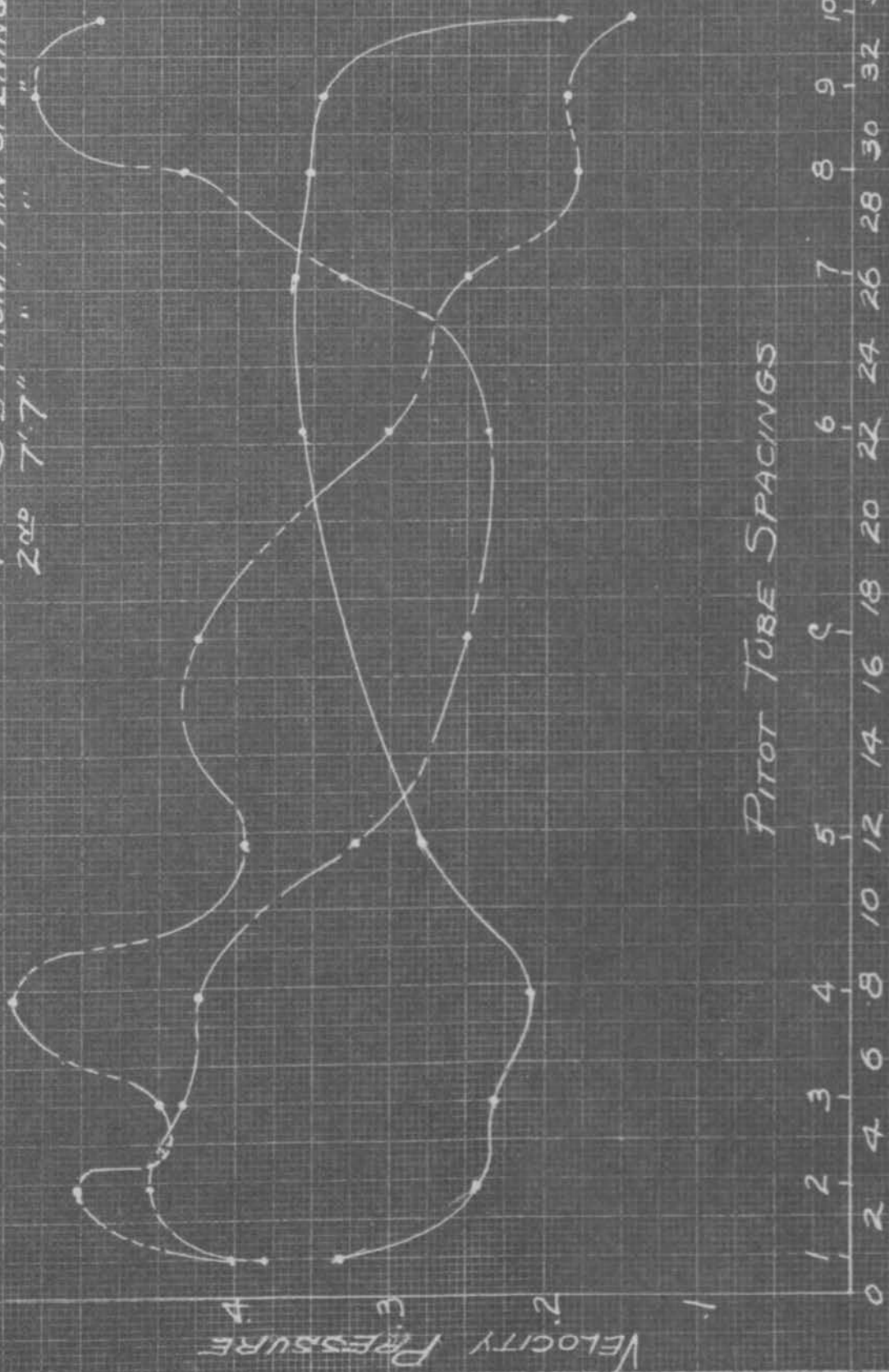
— No EQUALIZER  
 - - - EQUALIZER 5'1" OUT FROM FAN  
 - - - Two EQUALIZERS  
     1st - 3'9" FROM FAN OPENING  
     2nd - 7'7" " "

SHORT LENGTH  
 3/4 OPENING  
 SIDE READINGS



SHORT LENGTH  
 1/8 OPENING  
 TOP READINGS

— NO EQUALIZER  
 --- EQUALIZER 5'1" OUT FROM FAN  
 - - - - - TWO EQUALIZERS  
 1st - 3'9" FROM FAN OPENING  
 2nd - 7'7" "



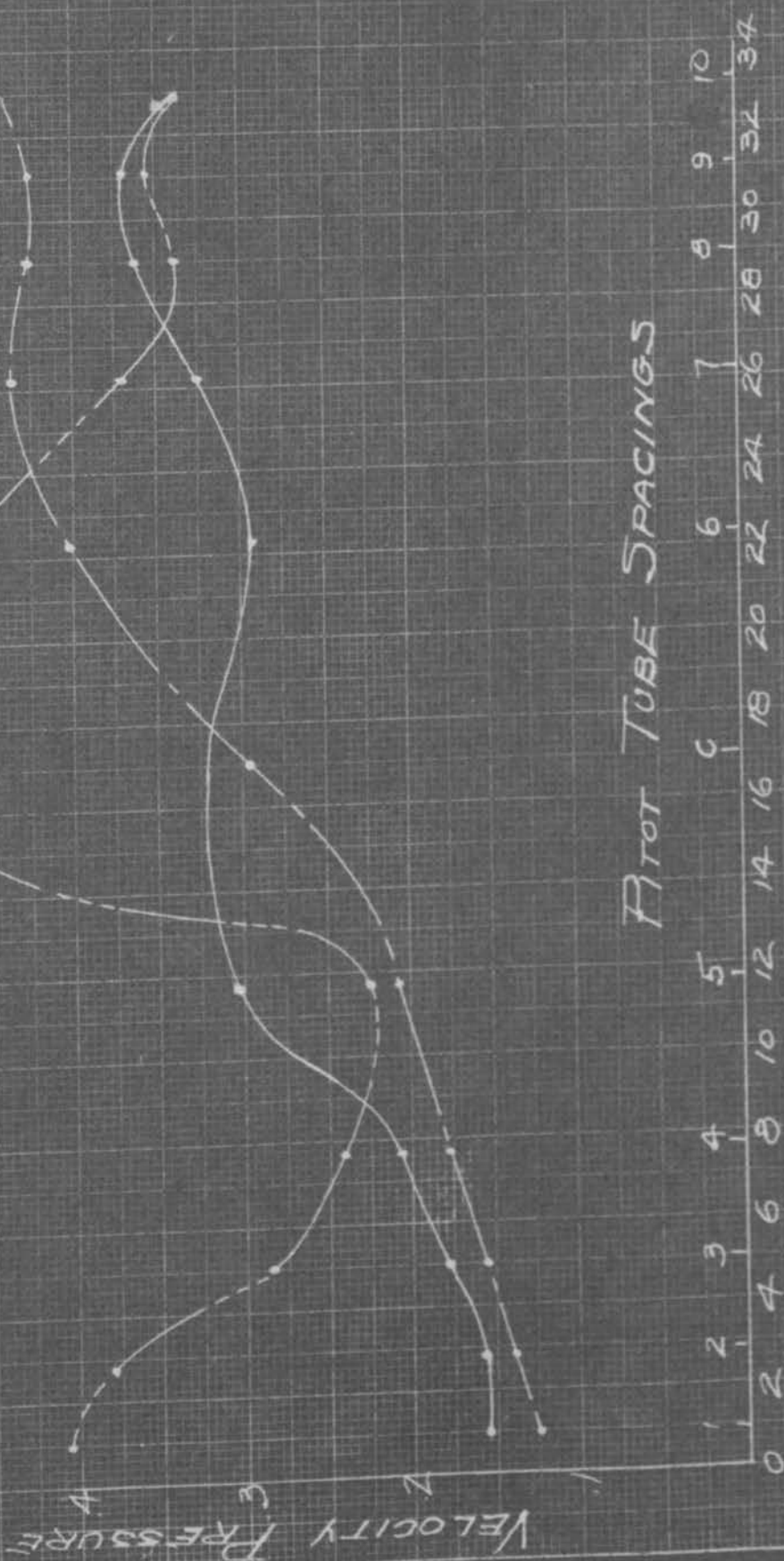
PITOT TUBE SPACINGS

DIAMETER OF PIPE IN INCHES



SHORT LENGTH  
 $\frac{7}{8}$  OPENING  
 SIDE READINGS

— NO EQUALIZER  
 - - - EQUALIZER 5'1" OUT FROM FAN  
 - - - - TWO EQUALIZERS  
 1ST 3'9" FROM FAN OPENING  
 2ND 7'7" " " "

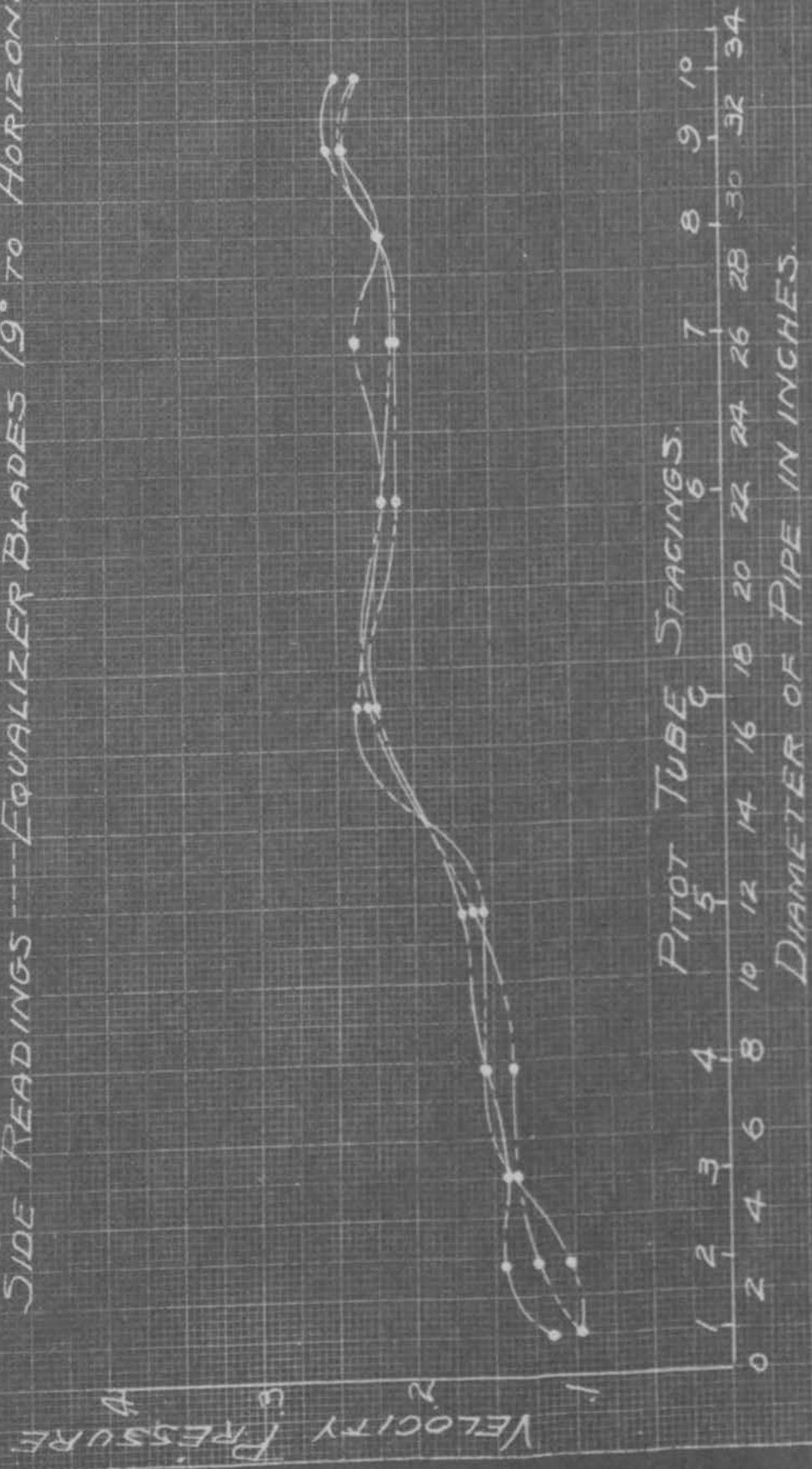


PITOT TUBE SPACINGS

DIAMETER OF PIPE IN INCHES

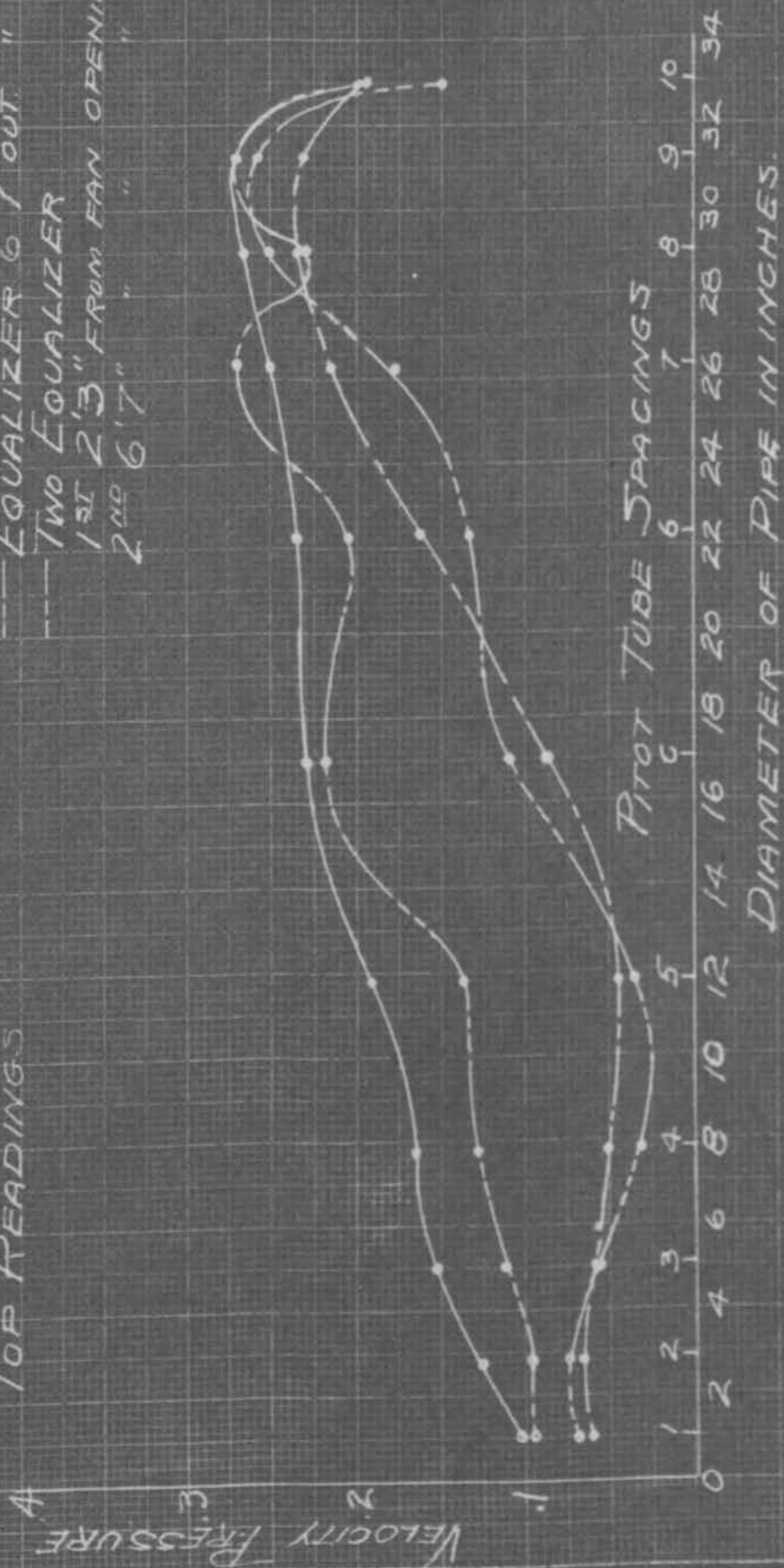
# EFFECT OF TURNING EQUALIZER IN PIPE

SHORT LENGTH --- EQUALIZER BLADES 45° TO HORIZONTAL  
 5/8 OPENING --- EQUALIZER BLADES PARALLEL TO FAN BLADE  
 SIDE READINGS --- EQUALIZER BLADES 19° TO HORIZONTAL.



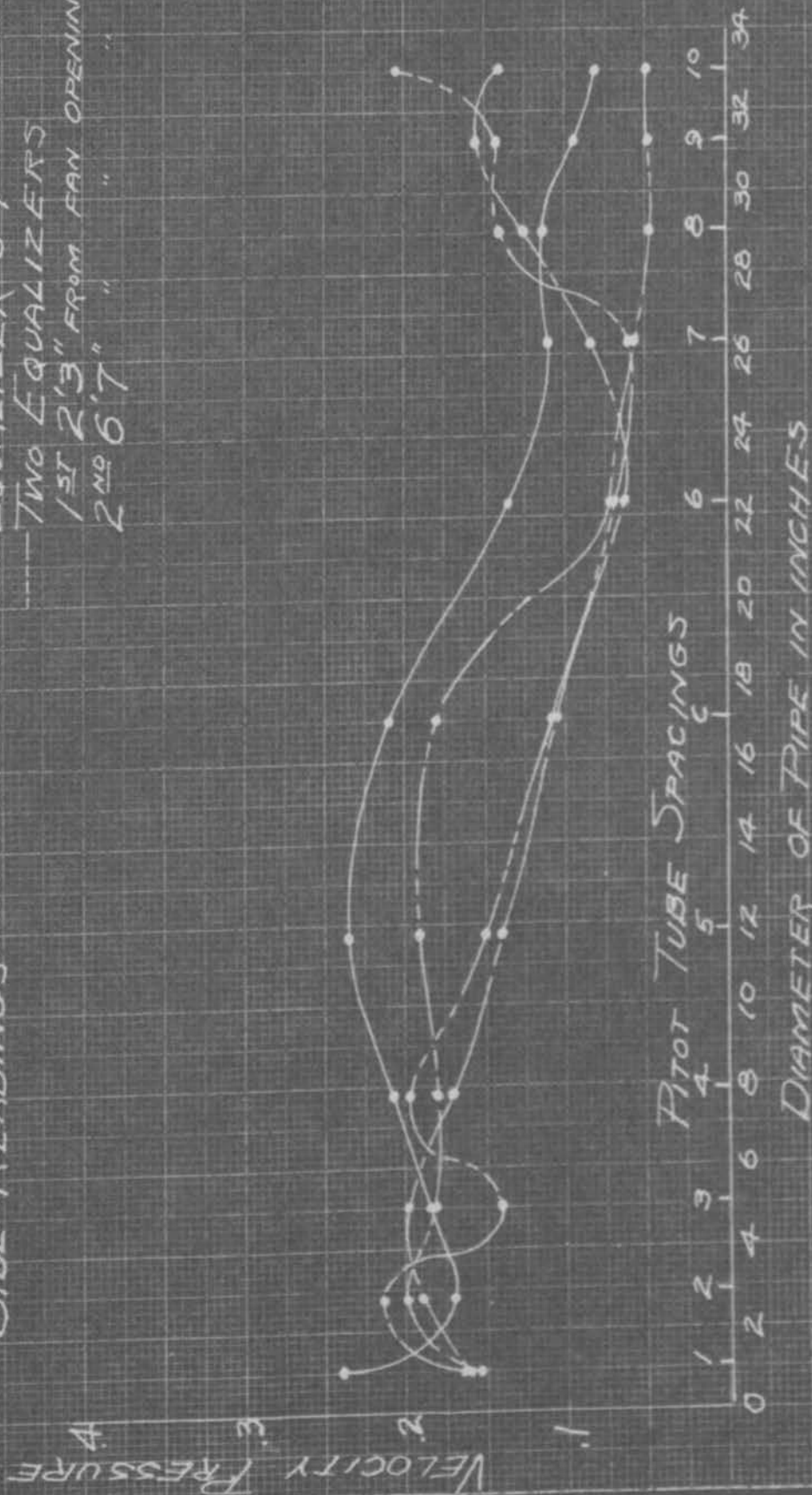
--- NO EQUALIZER  
 --- EQUALIZER 2'3" OUT FROM FAN  
 --- EQUALIZER 6'7" OUT "  
 --- TWO EQUALIZER  
 1<sup>ST</sup> 2'3" FROM FAN OPENING  
 2<sup>ND</sup> 6'7" "

SHORT LENGTH  
 1/2 OPENING  
 TOP READINGS



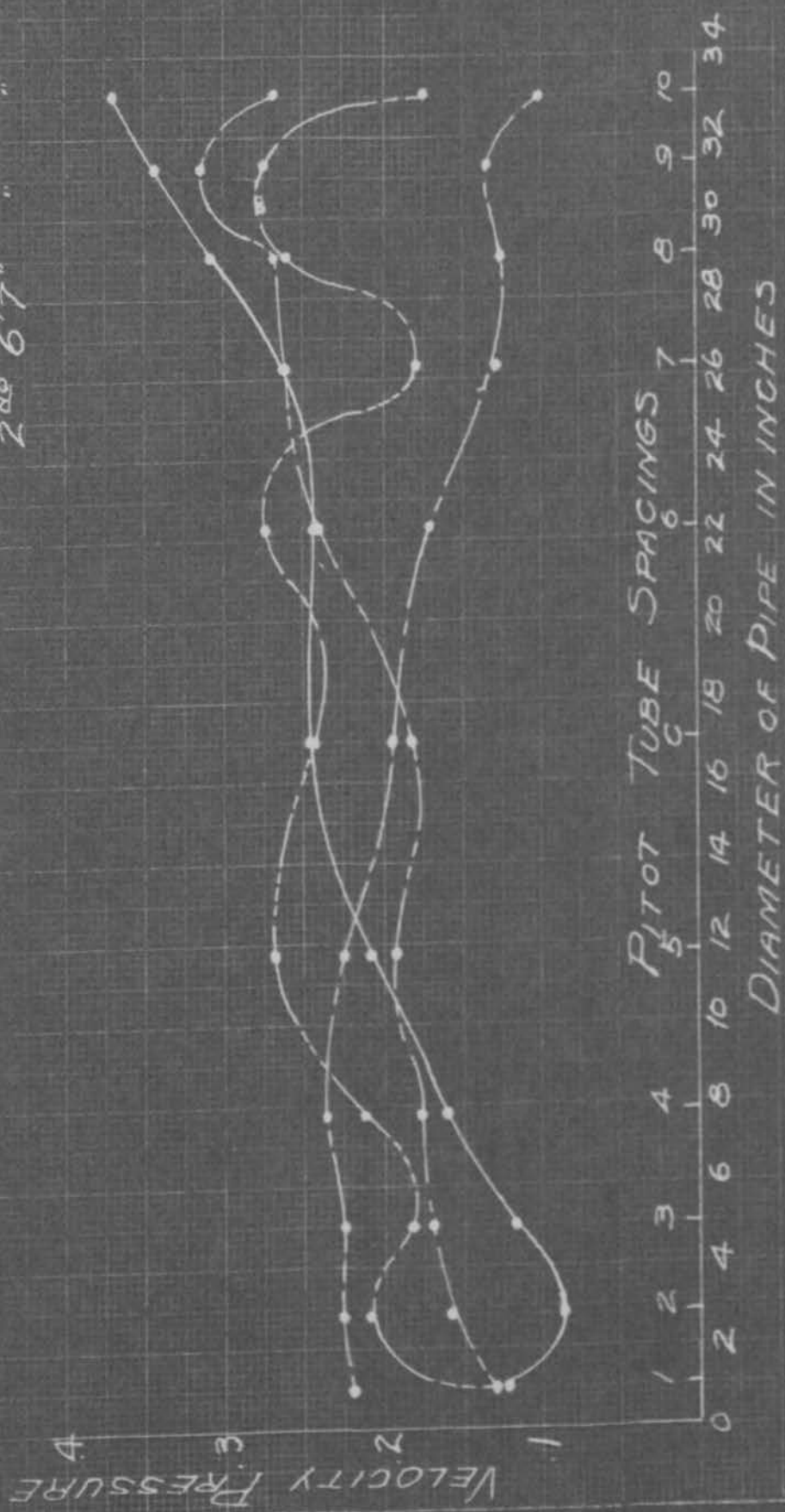
SHORT LENGTH  
 1/2 OPENING  
 SIDE READINGS

— No EQUALIZER  
 - - - EQUALIZER 2'3" OUT FROM FAN  
 - - - - - EQUALIZER 6'7" "  
 - - - - - TWO EQUALIZERS  
 1<sup>ST</sup> 2'3" FROM FAN OPENING  
 2<sup>ND</sup> 6'7" "



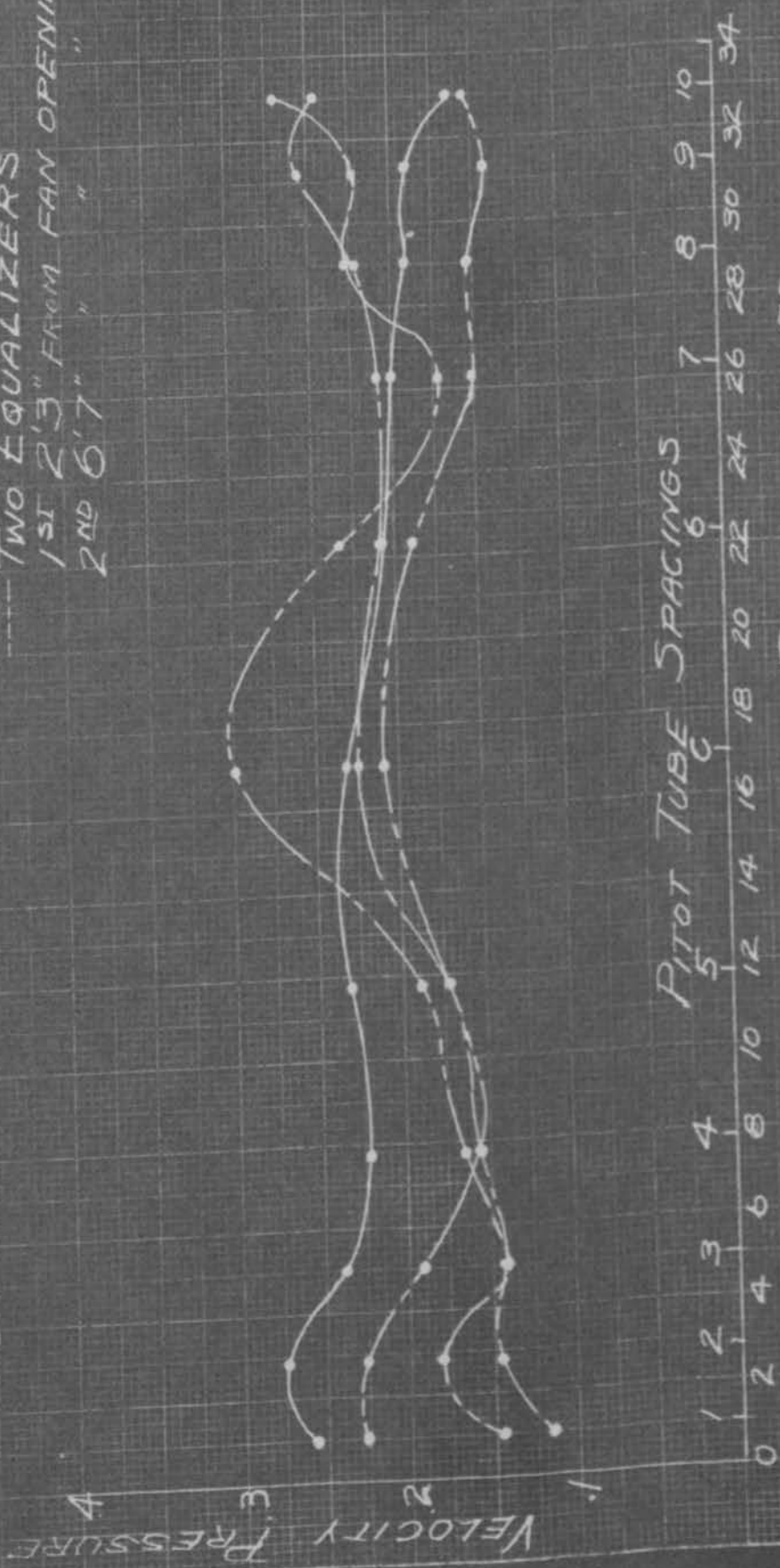
--- NO EQUALIZER  
 --- EQUALIZER 2'3" OUT FROM FAN  
 --- EQUALIZER 6'7" "  
 --- TWO EQUALIZERS  
     1<sup>ST</sup> 2'3" FROM FAN OPENING  
     2<sup>ND</sup> 6'7" "

SHORT LENGTH  
 5/8 OPENING  
 TOP READINGS



--- NO EQUALIZER  
 --- EQUALIZER 2'3" OUT FROM FAN  
 --- EQUALIZER 6'7" "  
 --- TWO EQUALIZERS  
 --- 1ST 2'3" FROM FAN OPENING  
 --- 2ND 6'7" "

SHORT LENGTH  
 5/8 OPENING  
 SIDE READINGS

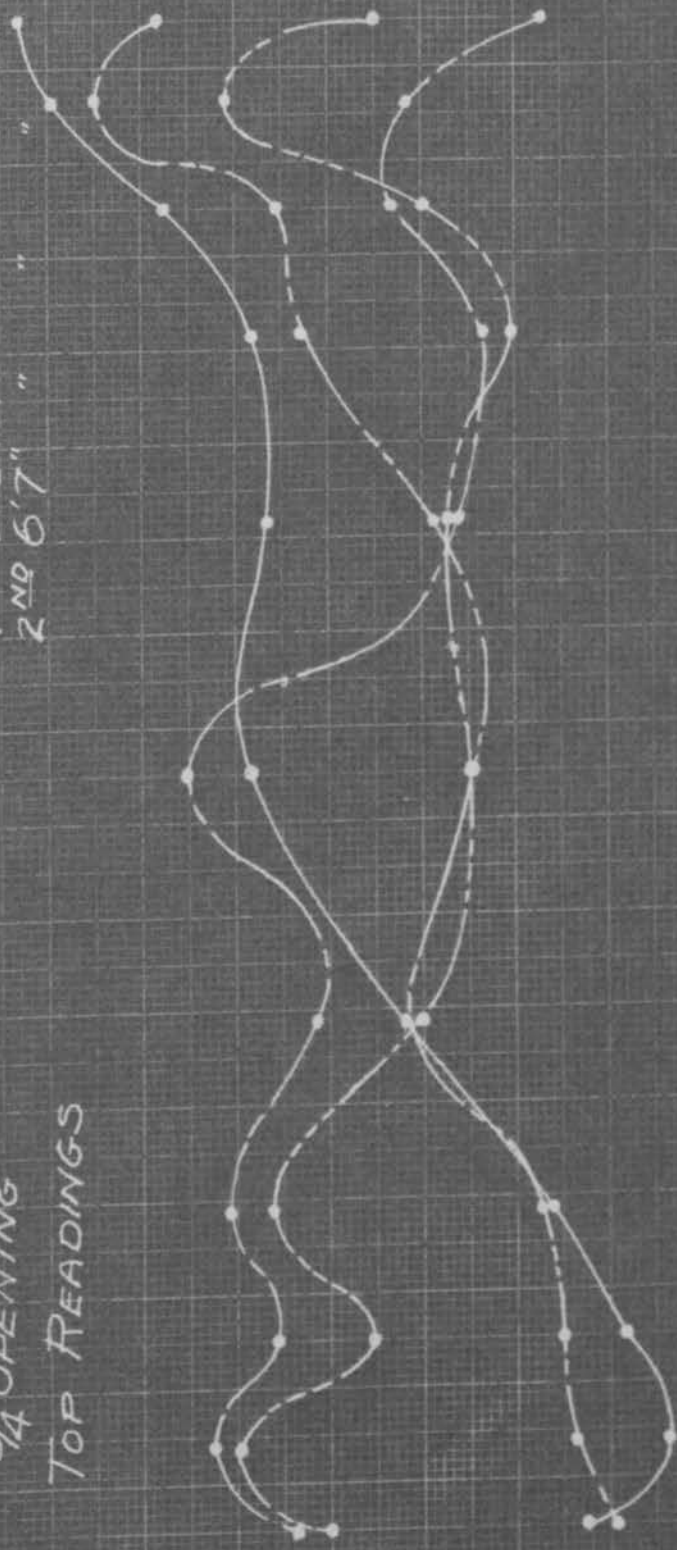


PITOT TUBE SPACINGS  
 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34  
 5 6 7 8 9 10  
 DIAMETER OF PIPE IN INCHES.

- NO EQUALIZER
- - - EQUALIZER 2'3" OUT FROM FAN
- · · · · EQUALIZER 6'7" "
- TWO EQUALIZERS
- 1ST 2'3" FROM FAN OPENING.
- 2ND 6'7" "

SHORT LENGTH  
3/4 OPENING  
TOP READINGS

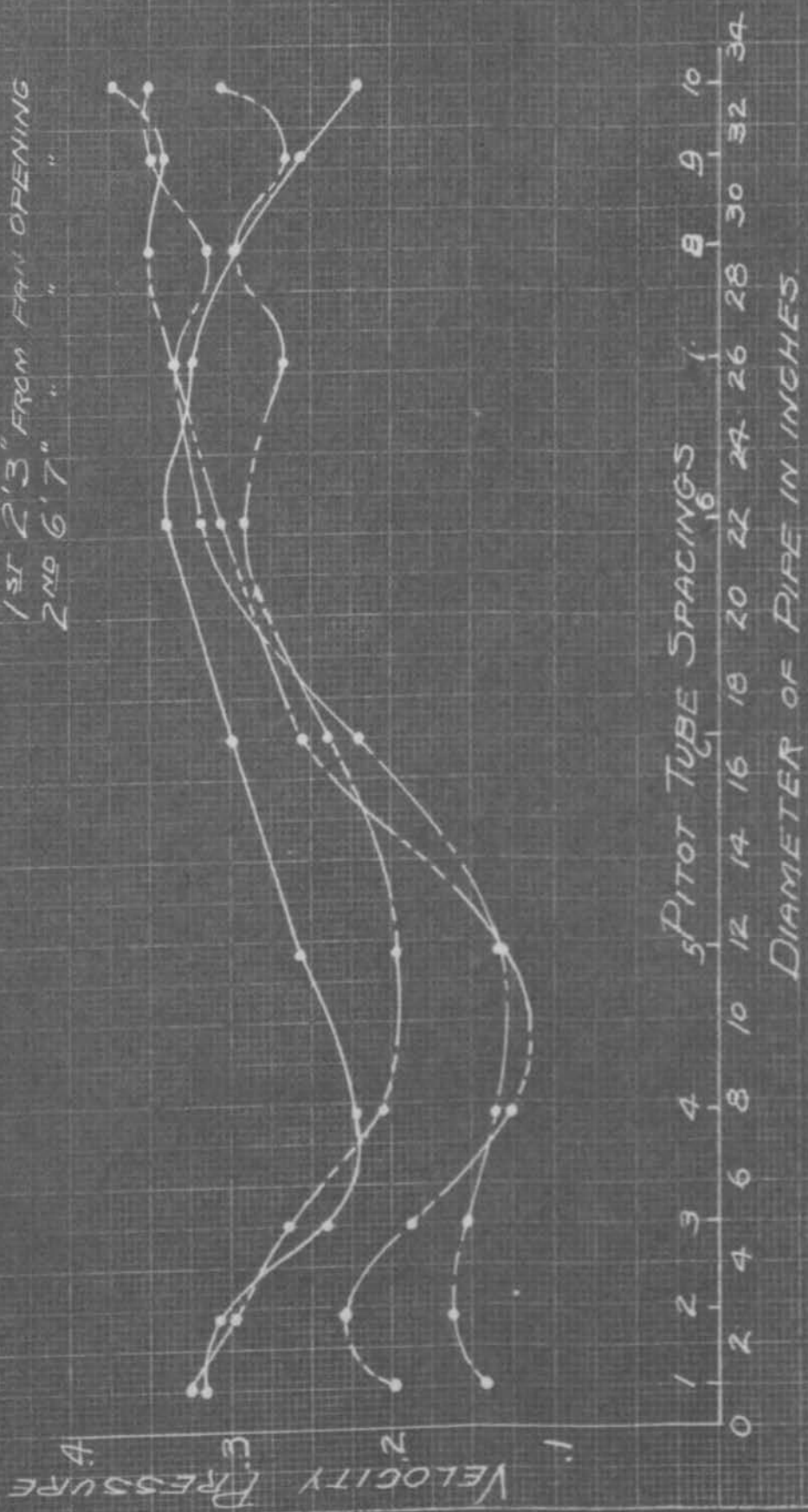
5  
4  
3  
2  
1  
VELOCITY PRESSURE



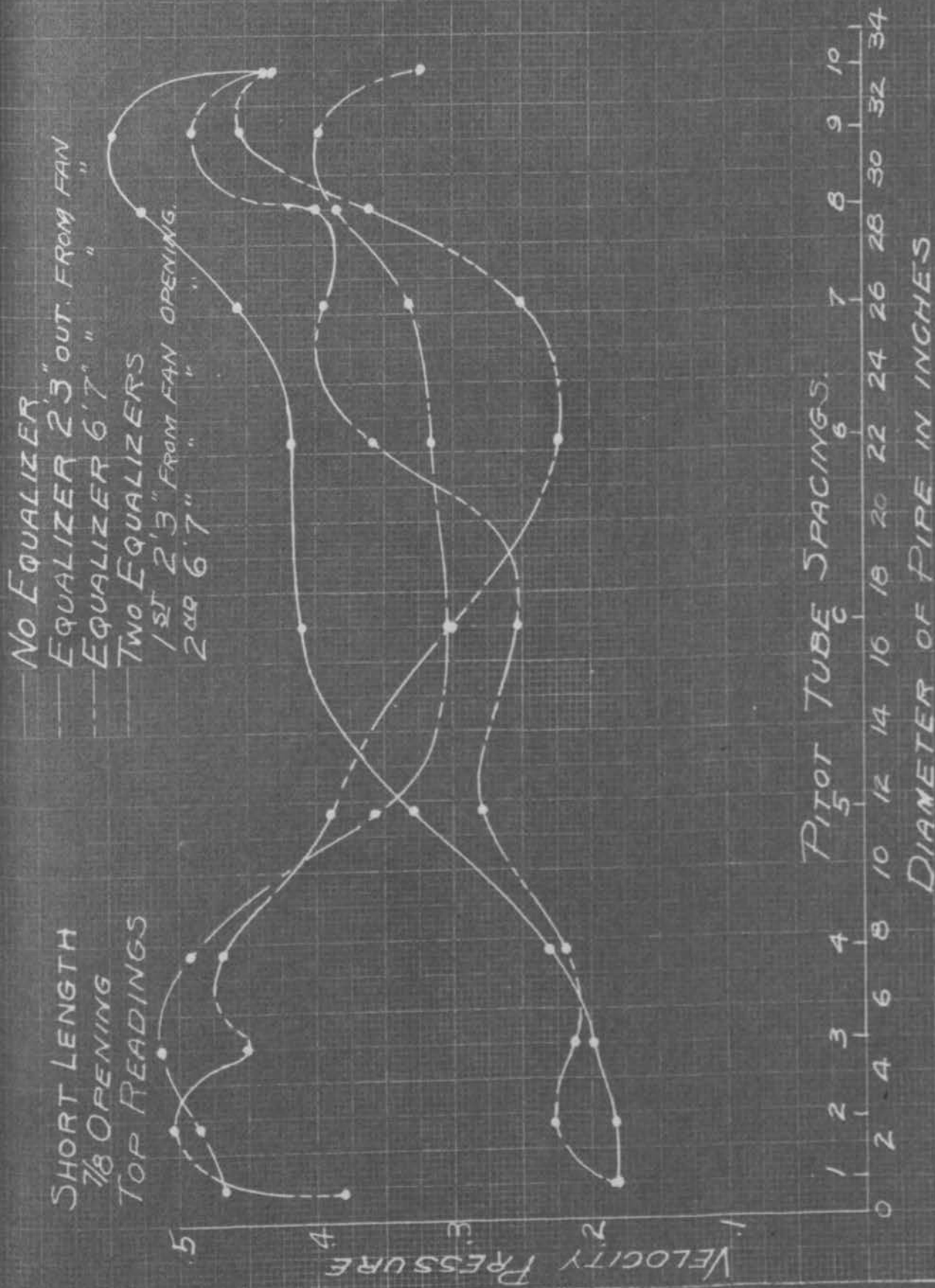
10  
9  
8  
7  
6  
5  
4  
3  
2  
1  
0  
PITOT TUBE SPACINGS 7 8 9 10  
DIAMETER OF PIPE IN INCHES

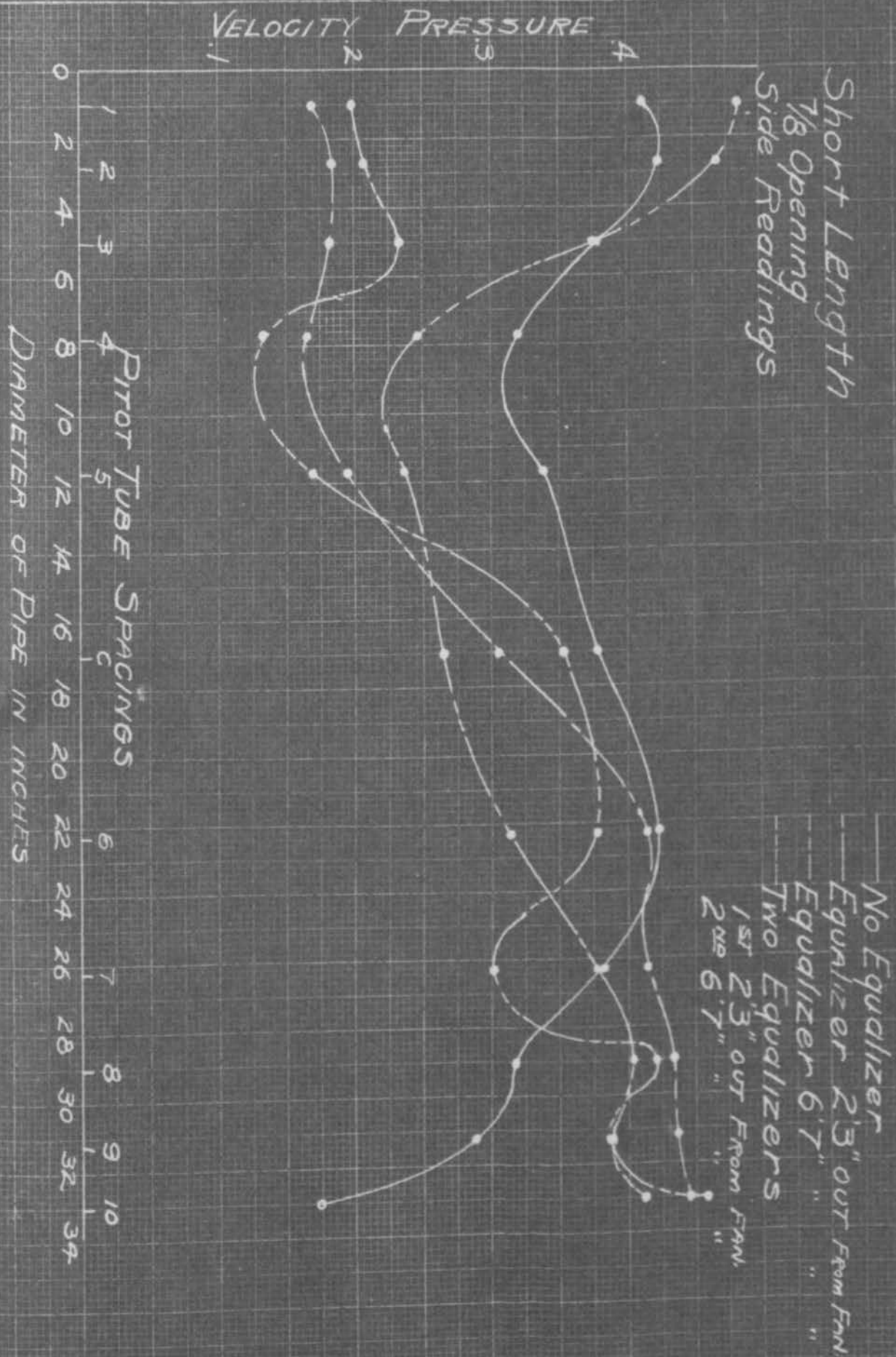
- NO EQUALIZER
- - - EQUALIZER 2'3" OUT FROM FAN "
- - - - EQUALIZER 6'7" "
- - - - - TWO EQUALIZERS
- 1<sup>ST</sup> 2'3" FROM FAN OPENING "
- 2<sup>ND</sup> 6'7" "

SHORT LENGTH  
3/4 OPENING  
SIDE READINGS









### CONCLUSION

When two equalizers were used it was difficult to obtain constant values of the velocity pressure at each point in the pipe because of the effect of the equalizers distributing the air in the pipe. The second equalizer was placed at an angle to the first equalizer (with reference to the side of the pipe). These readings show clearly that one or two equalizers do not give an even distribution of the air in the pipe using the short or long length of pipe. The curves given in Mr. T. S. Taylor's discussion for 50 diameters of pipe shows a very good distribution at that distance. Our tests, however, were made using only 8 diameters for the long length and 5 diameters for the short length.

The curves given show the effect of varying the distance of the equalizer from the mouth of the blower. An even distribution is not obtained but the velocity increases at one, two or three points in the pipe. A different curve was obtained (as might be ex-

pected) with the equalizer at a greater distance from the mouth of the blower because the air distributes itself with increasing distance from the mouth of the blower.

The curve given shows the effect of the angle of the blades of the equalizer to the blades of the fan. The velocity is practically the same throughout the pipe. The same general curve is obtained at all angles. This test to determine the effect of the angle that the equalizer is placed at, was run because of the effect of the equalizer in changing the velocity in the pipe to a maximum at a point where it was near a minimum before as is shown by a study of the curves.

A study of the curves will also show that the majority of the curves have a greater or equal average or mean velocity with no equalizer than with an equalizer placed in the fan. This is because of the effect of the equalizer in distributing the air and causing friction against the sides of the 4" squares of the equalizer.

It is impossible to obtain an even distribution

such as that obtained with a 40 diameter pipe as is shown by all these tests. The effect of the two equalizers at different spacings in the short and long length of pipe are clearly shown by the curves. The air passes through the equalizers and does not cause a distribution such as that desired. This may easily be seen by comparing the top and side readings. The top reading might be a maximum at one side of the pipe while the side reading might be a maximum at the 7th, 8th, 9th or 10th reading. The maximum velocity is around the outside of the pipe. The equalizers break up the air in the pipe and cause a maximum velocity at one, two, three, or more points as shown. This may be seen by comparing the equalizer curves with those of no equalizer.

It is therefore clearly seen by the above discussion that it is impossible to get an even distribution of the air in the pipe of this size by using equalizers. We therefore recommend that ~~N~~ (in any other tests to be carried on in the future) ~~that~~ in the first place, either a larger or smaller fan be used with similar equalizers or, in the second place, another kind

*The type shown*

of equalizer used such as a blade of some kind which could rotate, such as a propeller blade on an airplane. Still another method to be recommended is that of applying the Venturi principle in the construction of the delivery pipe.

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